



Phillips Lytle LLP

Federal Express and Email

March 15, 2018

Mr. Rick Geiger, Chair
Village of Trumansburg Planning Board
56 East Main Street
Trumansburg, NY 14886

Re: Ithaca Neighborhood Housing Services and Sundial Property Development, LLC/Claudia Brenner's Proposed Project at 46 South Street in the Village of Trumansburg, New York ("Village") - - **Supplemental Information - Response to Comments from MRB Group and Comments from Village Planning Board**

Dear Chairman Geiger and Members of the Village Planning Board:

As you know, we represent Ithaca Neighborhood Housing Services ("INHS") in connection with the proposed 46 South Street Project ("**Project**"), which involves the construction of a residential/mixed-use project on a nineteen (19) acre parcel of property located at 46 South Street in the Village of Trumansburg, New York ("**Site**"). INHS and Sundial Property Development LLC/Claudia Brenner ("**Applicant**") are working on the Project together.

On behalf of the Applicant, we hereby submit one (1) original, and five (5) copies of this supplemental submittal: (1) responding to MRB Group's written comments on the proposed Project by letter dated February 19, 2018; and (2) responding to a number of questions posed by the Planning Board in connection with the Project at the January 18 Planning Board meeting. For the convenience of the Planning Board, we have included the text of each comment that the Applicant is providing responses to with Applicant's response to same in italics.

We hereby submit the following exhibits, which are attached hereto, and made part of the Supplemental Submittal and which amend the pending applications:

- Exhibit A:** Cover Sheet
- Exhibit B:** Site Plan & Preliminary Plat
- Exhibit C:** Correspondence from Army Corps of Engineers
- Exhibit D:** Civil Engineering Plans
- Exhibit E:** Landscaping Plan

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- Exhibit F: Lighting Plan
- Exhibit G: Revised Drainage Report
- Exhibit H: Photographs of "No Mow" Lawn
- Exhibit I: Enlarged Road Plans

Applicant's Response to Comments From MRB Group

SEQRA

1. The Planning Board declared their "Intent to be Lead Agency" at the January 18, 2018 Planning Board meeting and began the Coordinated Review. Preliminary Applications materials were forwarded to all identified agencies (Involved and Interested) with a request for response. Please note not all identified Involved Agencies have responded to the Planning Boards request and it is suggested that the SEQR and the project application be continued to the March 22, 2018 Planning Board meeting to provide additional time for these agencies to respond.

Applicant's Response: Acknowledged.

General & Site Materials Plan

2. The Cover Sheet should be updated to identify the project as being a 'Preliminary Site Plan and Subdivision Plan'. A drawing index is also encouraged.

Applicant's Response: A cover sheet including drawing index has been added. See Exhibit A, Cover Sheet.

3. Please incorporate a Site Plan at the same scale as the utility and grading plans into the set. These plans should depict and label all site features including, but not limited to, parking areas, roadways, driveways, walkways, buildings, setbacks, road designations, road stationing, dumpsters, patios, easements and other typical site related



information. Site Data tables with zoning information such as setback requirements (proposed and required), parking requirements, green space, etc. should also be provided.

Applicant's Response: The Site Materials Plan has been updated to reflect the same scale as the Utility Plans (40 scale) – two sheets (L-101 & L-102) with match line. Unique and typical features have been labelled and zoning reference data table added. See Exhibit B, Site Plan & Preliminary Plat.

- 4. The proposed buildings should be placed as close to the front setback lines as possible to create a more uniform appearance and minimize impervious surface lengths for driveways and sidewalks.**

Applicant's Response: Alterations to proposed front yard setbacks to be reviewed with Planning Board for further direction.

- 5. All variances granted by the ZBA are to be detailed on the site plans.**

Applicant's Response: A note detailing the variance for the reduced width of the right-of-way to Pennsylvania Avenue has been added to the Preliminary Plat. See Exhibit B, Site Plan & Preliminary Plat (Note 6).

- 6. The public road and private drive should have a designation (such as A, B, C), or name on the plans, for discussion and review purposes. This should also be considered for buildings as well with some lots having multiple structures.**

Applicant's Response: Alphabetic designators have been assigned to all distinct road segments. See Exhibit B, Site Plan & Preliminary Plat.

- 7. All proposed garages and driveway locations should be labeled on the plans. Where garages are located, if shared parking spaces are being proposed, they should be depicted on the plans.**

Applicant's Response: All garages labelled with associated parking spaces have been identified both graphically, and with annotations. All typical driveway types have been identified. See Exhibit B, Site Plan & Preliminary Plat.



8. A typical parking space dimension and driveway dimensions are to be added to the plans. Where feasible, shared driveways should be considered.

Applicant's Response: Typical dimensions for all driveway types and parking areas have been included. See Exhibit B, Site Plan & Preliminary Plat.

9. Pedestrian access from the proposed driveway locations to the buildings should be provided on the plans.

Applicant's Response: Pedestrian access between driveways and buildings shown.

10. The site plans should demonstrate compliance with the ADA requirements including handicapped parking areas, accessibility, and sidewalk connections. Handicapped parking spaces should be located at locations with the shortest accessible route of travel to the building entrances.

Applicant's Response: ADA parking spaces shown proximate to building entrances. See Exhibit B, Site Plan & Preliminary Plat.

11. Method and assurance of perpetual maintenance of common areas, , internal sidewalks, parking areas, private roadways, stormwater mitigation measures including stormwater wetlands, bioretention filter, rain gardens and hydrodynamic separator is to be provided to the Village Attorney for review and approval as part of Final Plan submission.

Applicant's Response: This comment will be addressed at Final Site Plan Approval. Methods and responsibilities of maintenance will be outlined in the final SWPPP document.

12. Either the sideway or the dumpster locations associated with the Apartment Complex should be reconfigured to prevent crossing of the sidewalk by a disposal vehicle to access dumpsters. Also the eastern dumpster may need to be relocated due to its close proximity to an



outdoor gathering area/ patio. Also a dumpster enclosure detail is to be provided on the plans. Are individual totes anticipated for the remaining lots?

Applicant's Response: Dumpster enclosures have intentionally been pulled back from the edge of roadway. Specific to the western dumpster - the concrete sidewalk, which a service vehicle must traverse, shall be designed to support vehicular loads for the full width of the dumpster access drive. Direct sidewalk connection to the dumpsters facilitates safe and convenient access from the apartment building. Dumpster enclosure drawing to be provided. All other lots are to have individual totes.

- 13. All correspondences with Army Corps of Engineers (ACOE) regarding their review of the project plans and Wetland Delineation Report are to be forwarded to the Village and MRB.**

Applicant's Response: The requested information has been provided with this Supplemental submittal as Exhibit C, Correspondence form Army Corps of Engineers.

- 14. The Site Materials Plan identifies one of the wetlands as "Wetland E" which is labeled as "Wetland F" on the Boundary & Topographic Plan. Please ensure consistent labeling between plans.**

Applicant's Response: Correction completed. See Exhibit B, Site Plan & Preliminary Plat.

- 15. The Site Materials Plan is to be updated to identify that a bioretention area is also proposed within the Landscape Buffer Area.**

Applicant's Response: All bioretention areas have been identified. See Exhibit B, Site Plan & Preliminary Plat.

- 16. The right-of-way for both terminus points of the public road should be extended beyond the pavement area for maintenance purposes.**

Applicant's Response: Right-of-ways were extended 10' beyond the terminus points of both turn-arounds. See Exhibit B, Site Plan & Preliminary Plat; Exhibit D, Civil Engineering Plans; and Exhibit E, Landscaping Plan.



17. The Planning Board should determine if a future public road to the southern property is warranted. According to the plans a proposed "Optional Future Road Extension" is provided at the terminus point of the public road at Lot 11. If the Planning Board desires a future connection, then the public right-of-way should be extended to the property line.

Applicant's Response: Recommendation to be discussed with Planning Board for further direction.

18. The length of the proposed public road and sidewalk areas extending beyond Lot 11 should be shortened to provide only what is necessary to provide access to Lot 11.

Applicant's Response: Length of public road has been reduced. See Exhibit B, Site Plan & Preliminary Plat.

19. In order to provide legal means for the Village to be able to turnaround the vehicles, an easement is to be provided over a portion of the entrance drive to apartment complex by Lot 15.

Applicant's Response: An access easement was added to the plan set. See Exhibit B, Site Plan & Preliminary Plat.

20. An evaluation of vehicle turning movements demonstrating that there is adequate space available for emergency vehicles, disposal vehicles, vehicles with trailers, etc. to maneuver around onsite without obstructing the internal traffic flow and emergency access to the site should be provided.

Applicant's Response: Autoturn circulation analysis to be documented at Final Site Plan Approval.

21. The Village Fire Marshal and Code Enforcement Officer should be satisfied that emergency access is adequate and meets NYS Building



Code requirements. The marking of fire lanes and the installation of no parking signs should be identified on the plans.

Applicant's Response: Fire lane markings and no parking signs to be included in Final Site Plan Application.

- 22. Signature lines for the Planning Board Chairman, Engineer, and DPW Supervisor are to be added to the Preliminary Plans.**

Applicant's Response: Signatory lines have been added. See Exhibit A, Cover Sheet.

- 23. The South Street right-of-way line scales as 60' but is listed as 49.5' on the subdivision plan. Please clarify.**

Applicant's Response: The South Street right-of-way is 49.5' feet per the Preliminary Plat. Right-of-way lines were corrected on all drawings. See Exhibit B, Site Plan & Preliminary Plat.

PRELIMINARY PLAT & EXISTING CONDITIONS PLAN

- 24. All identified wetlands should be shown on the Plat Plan, as they are referenced in the notes. Please provide more information within the notes regarding the wetlands such as the report date, survey date, who surveyed them and the ACOE Determination (if one was provided).**

Applicant's Response: Wetlands and report and ACOE determination information requested has been added to the Preliminary Plat. See Exhibit B, Site Plan & Preliminary Plat. (See Note 6).

- 25. The Village Attorney should confirm whether the proposed private drive making connection to South Street can be placed on its own lot (Lot 13), which is a non-confirming lot. This lot may need to be divided between the two neighboring lots (Lot 8 & Lot 14) with a perpetual access easement over to the community.**

Applicant's Response: Applicant is awaiting Village Attorney determination.



26. The Site Data Table should be added to the Subdivision Plat.

Applicant's Response: Site Data Table was added to the Preliminary Plat. See Exhibit B, Site Plan & Preliminary Plat.

27. The proposed utility easement to the Village of Trumansburg should be widened the full width of the private drive for access.

Applicant's Response: The original Lot 13 that included the Private Drive was consolidated with Lot 12. The entire portion of Lot 12 east of the new public roadway is included as a utility easement. See Exhibit B, Site Plan & Preliminary Plat.

28. The right-of-ways for both Pennsylvania Ave and South Street are to be labeled on all Plans.

Applicant's Response: The right-of-ways have been labeled on the Preliminary Plat. See Exhibit B, Site Plan & Preliminary Plat.

29. The boundaries of the wetlands are difficult to read on the Existing Conditions Plans. A different line weight should be considered.

Applicant's Response: Wetland boundaries have been enhanced on the Existing Conditions Plan. See Exhibit D, Civil Engineering Plans.

DRAINAGE PLANS

30. All building down spouts and leaders are depicted on the plans and labeled. Size, material, and where connected, inverts are to be provided.

Applicant's Response: As building designs have not been advanced to a point where downspout locations can be determined a typical downspout design and arrangement has been shown and will apply to all market rate and townhouse buildings. Downspouts for the multi-family building have been added. See Exhibit D, Civil Engineering Plans.

31. Please remove the "Rim" and "In" or "Out" designations from the End Section labels. These are misleading as there is no rim and some of the in and out designations appear to be the opposite of the flow direction.



Applicant's Response: "Rim" and "In" or "Out" designations have been removed from the End Section labels. See Exhibit D, Civil Engineering Plans. (Sheets C103 and C104).

32. A numerical designation for each drainage structure should be provided for clarity.

Applicant's Response: Numerical designations have been provided. See Exhibit D, Civil Engineering Plans. (Sheets C103 and C104).

33. Proposed rain gardens do not appear to be in the primary flow path where they can provide the greatest water quality benefit by collecting runoff from both buildings and driveways. Examples of this include constructing the rain gardens next to, but not within, the swales between Lots 2, 3, 4 & 5.

Applicant's Response: Grading has been modified to maximize the areas captured by the rain gardens. See Exhibit D, Civil Engineering Plans. (Sheets C103 and C104).

34. The size and depth of the proposed rain gardens are to be added to the plans. Rain gardens should have an average ponding depth of 6" or less.

Applicant's Response: The surface areas of the rain gardens have been added to the drawings. The depth of the rain gardens has been modified to 6". See Exhibit D, Civil Engineering Plans. (Sheets C103, C104 and C202).

35. Some of the proposed piping configurations for the catch basins cannot be built as proposed. These include the structure at station 1+45.69 and inlets that receive piping from bioretention areas. The size of all proposed catch basins are to be added to the plans.

Applicant's Response: Piping/Structure configurations have been re-examined. All drainage inlets are 2'x2' unless otherwise noted. See drawings C103 and C104. The drainage inlet detail has been modified. See Exhibit D, Civil Engineering Plans.

36. The storm sewer system draining to the bioretention filter is confusing in its design. It appears as though some storm water is piped to the



bioretention filter and some is bypassed through Storm Manhole at 1+06.61 to the stormwater wetland. According to the drainage report all water quality volume related storm water from this area shall be conveyed to the bioretention filter prior to it entering the stormwater wetland. Clarification should be provided regarding this design.

Applicant's Response: The piping configuration is set up to take only the water quality storm event to the bioretention filter (per guidance in section 6.4.2 of the NYSDEC Design Guide). The larger storm events will bypass to the stormwater wetland. This information has been provided in updated drainage calculations narrative. A detail showing the sizing of the diversion structures has been added to Sheet C202. See Exhibit D, Civil Engineering Plans.

37. The end section invert elevation of the pipe entering the stormwater wetland from Lot #11 is listed with an elevation of 987.78 below the bottom of the stormwater wetland which is listed at 989.90.

Applicant's Response: The invert elevation has been adjusted. See Exhibit D, Civil Engineering Plans. (Sheet C103).

38. The 12" pipe exiting from the Storm Manhole at 1+06.61 does not have any cover or the top of the pipe is above grade along portions of its length. Also this pipe terminates at an end section identified as a "Null Structure". Please clarify.

Applicant's Response: Grading has been revised to provide proper cover and the null structure tag has been removed. See Exhibit D, Civil Engineering Plans. (Sheet C104).

39. The underdrain piping with inverts for the bioretention filter are to be depicted on the plans. Based on an approximate 4' depth to the invert shown on the detail sheet, please verify the pipes can exit to daylight. The bioretention filter should also have an overflow allowing a maximum of 6" ponding depth.

Applicant's Response: Underdrain piping with inverts has been shown, an overflow structure included and the pipe invert has been noted. See Exhibit D, Civil Engineering Plans. (Sheets C103 and C104).



40. Details of the outlet structures for the stormwater wetland are to be added to the plans. Also the inverts for the end sections are to be provided. Outlet structure inlets should have reverse pitch piping to the permanent pool.

Applicant's Response: Inverts for all end sections and detail for the outlet structures have been added. See Exhibit D, Civil Engineering Plans. (Sheets C104 and C202).

41. The applicant should clarify why the two outlet structures for the Lot #12 stormwater wetland are separated by the rip-rap spillway? It would seem practical to keep them closer to one another for inspection and maintenance purposes.

Applicant's Response: The southern outlet structure has been relocated north of the rip-rap spillway for ease of maintenance.

42. Outlet Structure #3 and the Drainage Inlet at 5+17.23 appear to be shallow. A detail of these structures are to be provided for review.

Applicant's Response: Structures have been modified to provide adequate depth. See Exhibit D, Civil Engineering Plans. (Sheets C104 and C202).

43. The plans should demonstrate how access to the stormwater management areas and outfall structures will be provided as per the NYS Stormwater Management Design Manual (SWDM).

Applicant's Response: Grading has been revised to allow vehicular access to the stormwater management practices. See Exhibit D, Civil Engineering Plans. (Sheets C105 and C106).

44. The dimensions and inverts for all emergency spillways are to be labeled on the plans.

Applicant's Response: Dimensions and inverts have been labeled on the plans. See Exhibit D, Civil Engineering Plans. (Sheets C103 and C104).



45. The storm piping located on Lot #6 and #7 is missing. Also all piping from the rain gardens to the catch basins are to be labeled with size, materials, and inverts.

Applicant's Response: Storm piping has been added to Lots #6 and #7. Piping from rain gardens to drainage inlets have been labeled. See Exhibit D, Civil Engineering Plans. (Sheets C103 and C104).

46. Along South Street the right-of-way lines, street name and edge of pavement labels are to be added. Also please clarify the two north-south dashed lines east of the South Street pavement.

Applicant's Response: Labels have been added, and the two dashed lines have been removed from all drawings.

47. More detail needs to be provided on the twin 30" underground storage pipes near South Street including, how the connection to the pipes is made, how the 30" pipes are connected, and how they are accessed for maintenance. A detail should be provided for this system on the plans.

Applicant's Response: This system may change depending on the Planning Board's determination on the South Street drive location. This comment will be addressed in the Final Site Plan Review submission.

48. The hydrodynamic separator should be moved outside the South Street public right-of-way as it is a privately owned device.

Applicant's Response: This may change depending on the Planning Board's determination on the South Street drive location. This comment will be addressed in the Final Site Plan Review submission.

49. A change in direction of storm piping along South Street needs to be accomplished with a cleanout or structure.

Applicant's Response: A cleanout has been added to the bend. See Exhibit D, Civil Engineering Plans. (Sheet C104).



50. Please confirm that an end section can be provided for the 10' x 1' box culvert.

Applicant's Response: The box culvert will be a Contech aluminum box culvert with pre-manufactured aluminum end sections.

51. A number of the proposed catch basins appear to conflict with the proposed watermain location. Proper separation is to be provided.

Applicant's Response: Water mains have been relocated to provide proper separation. See Exhibit D, Civil Engineering Plans. (Sheets C103, C104, C107 and C108).

GRADING PLANS & EROSION AND SEDIMENT CONTROL COMMENTS

52. An erosion and sediment control plan is required. Suggest using NYSDEC standard details for all erosion and sediment control items.

Applicant's Response: See Exhibit D, Civil Engineering Plans. (Sheets C102 and C202).

53. The boundaries of all identified wetlands are to be depicted on the Grading Plans.

Applicant's Response: Wetland areas have been properly delineated. See Exhibit D, Civil Engineering Plans.

54. A portion of 'Wetland A' is filled on Lot 2 but not identified as such on the plans. Adjust labels regarding filling jurisdictional and/or isolated wetlands to reflect the current status of review provided by the Army Corps of Engineers (ACOE).

Applicant's Response: Grading plans show acreage of all jurisdictional wetlands to be filled in. See Exhibit D, Civil Engineering Plans. (Sheets C105 and C106).



55. Based on the proposed project design and improvements, the existing 'Wetland A' watershed will likely be reduced. The applicant should confirm that this reduction in area will not adversely impact this wetland.

Applicant's Response: This comment will be addressed in detail in the Full SWPPP submitted with the Final Site Plan Review submission. Please note the HydroCAD reports show that we are maintaining the water elevations in the wetland during the 1-, 10- and 100-year storm events.

56. The proposed 993 contour on Lot 2 needs to be corrected as it shown to dead end and not connect to an existing contour. Also the proposed contours at the southeast end of the public road end abruptly without any connection to an existing contour. It appears as though the continuation of these contours will result in impact to 'Wetland F'. Additional grading appears to be required and any fill areas are to be properly identified.

Applicant's Response: Grading Plans has been updated and proposed retaining walls shown. See Exhibit D, Civil Engineering Plans. (Sheets C105 and C106).

57. Add end section invert, catch basin grate and manhole rim elevations to the grading plan.

Applicant's Response: Storm structure rims and pipe inverts have been added. See Exhibit D, Civil Engineering Plans. (Sheets C105 and C106).

58. The plans should demonstrate how the 6" maximum permitted ponding depth within the bioretention filter will be maintained.

Applicant's Response: An overflow structure has been added to the bioretention filter to maintain the 6" maximum ponding depth. See Exhibit D, Civil Engineering Plans. (Sheet C104).



59. The drainage swales on Lots #10 & #11 are near flat at 0.2% likely resulting in standing water. Drainage swales should be designed at a minimum of 1% slope.

Applicant's Response: Grading of all drainage swales has been updated to maintain a 1% minimum slope. See Exhibit D, Civil Engineering Plans. (Sheets C105 and C106).

60. The existing tree line should be shown more clearly along with impacts associated with the grading.

Applicant's Response: Existing tree lines and a limit of disturbance line have been added to the plans. See Exhibit E, Landscaping Plan.

61. Some existing contours around the fringe of the project need to be labeled.

Applicant's Response: Existing contours have been labeled. See Exhibit D, Civil Engineering Plans. (Sheets C105 and C106).

62. Provide additional spot elevations at critical locations such as ramps, building entrances, curbs and sidewalks.

Applicant's Response: This comment will be addressed at Final Site Plan Approval submission.

63. The grading plan should identify the proposed spillway locations and incorporate spot elevations as necessary.

Applicant's Response: Spillway spot elevations have been added. See Exhibit D, Civil Engineering Plans. (Sheets C105 and C106).

64. Please clarify the heavy line on Lot #8 above the 997 contour.

Applicant's Response: The dark line was a feature line from Civil 3D that has been turned off. See Exhibit B, Site Plan & Preliminary Plat.



65. All grading between lots should be designed to provide positive flow away from building foundations and neighboring properties. The grading around Lot #14 appears to direct drainage flow towards Lot #15.

Applicant's Response: Cut off swales have been added to all lots. See Exhibit D, Civil Engineering Plans. (Sheets C105 and C106).

66. All snow storage locations should be identified on the Site Plan and Grading Plan. The proposed locations should minimize offsite drainage to adjacent properties.

Applicant's Response: Snow storage locations have been identified on the grading plans. See Exhibit D, Civil Engineering Plans. (Sheets C105 and C106).

67. An Erosion and Sediment Control Plan detailing how the site will be maintained and protected during construction is to be provided.

Applicant's Response: See Exhibit D, Civil Engineering Plans. (Sheets C102 and C202).

68. All erosion and sediment control measures and details shall be in accordance with the NYS Standards and Specifications for Erosion and Sediment Control (Blue Book).

Applicant's Response: All practices shown on the ESC Plan are in accordance with NYS Standards.

69. Silt fence sections must be joined either with a full section of overlap, or wrapping two ends together. See NYSDEC Blue Book for typical silt fence details. Strongly recommend using NYS DEC Reinforced Silt Fence detail.

Applicant's Response: See Exhibit D, Civil Engineering Plans. (Sheet C201).

70. A construction staging area should be identified on the demolition plans to prevent storage of vehicles and equipment from impacting adjacent residential areas or properties.



Applicant's Response: Construction staging areas have been added. See Exhibit D, Civil Engineering Plans. (Sheet C102).

71. Topsoil stockpile locations are to be identified on the plans and shown to be properly protected.

Applicant's Response: Topsoil stockpile areas have been added. See Exhibit D, Civil Engineering Plans. (Sheet C102).

72. All slope areas of 1 on 3 to be stabilized with a rolled erosion stabilization fabric including the drainage swales. These areas are to be identified on the plans.

Applicant's Response: Areas requiring stabilization fabric have been added. See Exhibit D, Civil Engineering Plans. (Sheet C102).

73. A more site specific construction sequence is to be provided detailing when the stormwater management facilities will be installed, the construction of the bioretention area, the installation of utilities, sidewalks, landscaped areas, and construction of certain storm sewers and inlets, etc. Is this project to be constructed all in one phase?

Applicant's Response: All project site infrastructure work (including roads, utilities, mass grading and stormwater management systems) and certain buildings are planned to be completed in 1 Phase. See Exhibit B, Site Plan & Preliminary Plat (Sheet L101, for a table of anticipated building construction. The sequencing notes on the E&SC plan have been tailored to the project. See Exhibit D, Civil Engineering Plans. (Sheet C102).

74. If the project will be developed in phases, a phasing plan defining the phase boundaries and associated acreage of each phase should be included with the plans set.

Applicant's Response: All Project Site infrastructure work (including roads, utilities, mass grading and stormwater management systems) and certain buildings are planned to be completed in 1 Phase. See Exhibit B, Site Plan & Preliminary Plat (Sheet L101, for a table



of anticipated building construction. See Exhibit D, Civil Engineering Plans. (Sheets C102).

75. The proposed limits of disturbance should be clearly identified on the plans with a boundary line. This area is to include all improvements proposed including work within right-of-ways or offsite.

Applicant's Response: A limit of disturbance line has been added to the plans.

76. The total acreage of disturbance anticipated for this project at one time should be labeled on the plans. If the total acreage to be disturbed at one time is greater than 5-acres, then a 5-acre waiver from the NYSDEC will be required. All correspondences with NYSDEC will be required to be forwarded to the Village and MRB.

Applicant's Response: This comment will be addressed in the Final Site Plan Review submission. It is anticipated that more than five (5) acres will be disturbed at one time, and as a result a waiver will be required from the NYSDEC. This will be addressed in the Full SWPPP and on the Notice of Intent (NOI).

UTILITY PLANS AND UTILITY PROFILES

77. The Design Engineer shall coordinate with the associated utility companies regarding the proposed new locations and connections. All correspondences with these utility companies shall be forwarded to the Village of Trumansburg.

Applicant's Response: This is an ongoing process and such information will be presented with the Final Site Plan submission.

78. The proposed water and sewer improvements and connections are subject to the review and approval of the Village of Trumansburg Public Works Department. Also the proposed water system master meter and RPZ location will require an approval from the Village and DOH. The design engineer should forward copies of all correspondence from DOH to the Village Office and MRB.



Applicant's Response: The water and sewer are both being dedicated to the Village. As this is not a private system, there will be no master meter & RPZ.

79. Based on the New York State Fire Code, Chapter 5, a residential/subdivision road constitutes a fire apparatus access road and therefore the minimum approved surface width is 26' where a hydrant is present (20 feet on center of the hydrant). The plans should be updated accordingly.

Applicant's Response: The roads have been widened to 26' at hydrant locations. These areas have been dimensioned on the Utility Plans. See Exhibit D, Civil Engineering Plans. (Sheets C107 and C108).

80. On sheet C107, the sanitary sewer lateral extending from Lot #2 is shown crossing the watermain. If possible, the lateral should be connected closer to the manhole to prevent the crossing.

Applicant's Response: The lateral has been connected directly to the manhole. See Exhibit D, Civil Engineering Plans. (Sheets C107).

81. In multiple locations, the sanitary sewer and watermain are shown within less than 10 feet of each other and are not close to being perpendicularly aligned. There are many laterals and service connections shown in these areas as well. 10 foot separation needs to be maintained between the watermain and any sewers except at crossings. Crossings should be made at as close to 90 degree angles as possible.

Applicant's Response: Applicant has modified all mains to maintain 10' of separation and minimized the number of crossings. The locations and profiles have been adjusted. See Exhibit D, Civil Engineering Plans. (Sheets C107 and C108).

82. At least one section of parallel watermain and sanitary sewer did not meet the 10 foot separation requirement. Verify that separation requirements are met for all watermains on site.



Applicant's Response: Applicant has modified all mains to maintain 10' of separation. See Exhibit D, Civil Engineering Plans. (Sheets C107 and C108).

83. The size, materials, length of all watermains and sewers are to be added to the Utility Plan. Slopes should also be labeled for sewers.

Applicant's Response: This information has been added to the Utility Plans. See Exhibit D, Civil Engineering Plans. (Sheets C107 and C108).

84. All curb stops and clean out locations should be identified on the plans and shown at the right-of-way beyond the sidewalk. Proper separation is to be provided between the sidewalk and these locations.

Applicant's Response: The walks were relocated to allow for installation at the right-of-way lines. See Exhibit D, Civil Engineering Plans. (Sheets C107 and C108).

85. Water and sewer notes regarding installation requirements, materials, testing, and inspections are to be added to the plans.

Applicant's Response: This information will be provided with the Final Site Plan submission.

86. Water Profile - A: One 12" storm was found to have less than 18" separation at a crossing. Watermains must maintain 18" minimum separation from any type of sewer crossing.

Applicant's Response: Crossings were modified to provide 18" separation. See Exhibit D, Civil Engineering Plans.

87. Water Profile - A: The proposed box culvert at about 13+20 should be labeled with its size, does not appear to be drawn to the correct width and does not have the 18" separation from the watermain.

Applicant's Response: The correct box culvert dimensions and vertical placement was added to the profile. See Exhibit D, Civil Engineering Plans. (Sheets C301).



88. Water Profile - B: One 6" storm was found to have less than 18" separation at a crossing. Watermains must maintain 18" minimum separation from any type of sewer crossing.

Applicant's Response: Crossings were modified to provide 18" separation. See Exhibit D, Civil Engineering Plans.

89. Sanitary Profile - C: numerous 1" copper pipes are shown crossing at the same elevation as the sanitary main.

Applicant's Response: Notes were added to the Utility plans to maintain 18" separation between all copper laterals and sewer mains. See Exhibit D, Civil Engineering Plans. (Sheets C107 and C108).

ROAD PROFILES

90. Add intersecting roads and label on the profiles.

Applicant's Response: Labels were added. See Exhibit D, Civil Engineering Plans. (Sheets C601 and C602).

91. Label the ends of roads and add right-of-way lines to the profiles.

Applicant's Response: Labels were added. See Exhibit D, Civil Engineering Plans. (Sheets C601 and C602).

LANDSCAPING PLAN, SITE LIGHTING & SIGNAGE PLANS & MISCELLANEOUS

92. The Landscape Plant Lists should be updated to provide the quantity and size of plants and trees to be provided. The landscaping plan is to be updated to identify where these trees and plants are located.

Applicant's Response: Typical plant and tree sizes and tree quantities to be reflected in Final Site Plan Submission, as was coordinated with MRB.



93. The Site Lighting Plan should provide manufacturer cut sheets and photometric plan depicting the true foot-candle illumination level. The proposed light fixtures are to be IDA (International Dark-Sky Association) approved. A note is to be added to the plans stating that all site lighting will be dark sky compliant and any replacement of lighting will remain dark sky compliant.

Applicant's Response: Note added. Photometric Plan to be included with Final Site Plan Submission.

94. Proposed lighting is not very visible on the plans. Please increase the lineweight of any proposed work that is pertinent to this plan sheet.

Applicant's Response: Graphic lineweights have been adjusted. See Exhibit F, Lighting Plan.

95. The Lighting Schedule identifies a quantity of 21 for street lights, however, only 20 are depicted on the plan. Please update accordingly.

Applicant's Response: Light quantities updated. See Exhibit F, Lighting Plan.

96. An additional path lighting is encouraged for the path between the private and public road.

Applicant's Response: Light levels intentionally kept low in this area due to proximity of adjacent neighboring buildings. To be reviewed with Planning Board for direction.

97. Where ADA parking spots are designated, the ADA parking spot pavement markings should be shown on the plans. ADA aisles should show appropriate hatched pavement markings on the plans.

Applicant's Response: ADA parking space aisles are shown with appropriate hatches. Spot elevations to be shown in Final Site Plan Submission.



98. Suggest adding a sidewalk and marked pedestrian crossing for the ADA parking spots on the north side of the main building.

Applicant's Response: Pavement marking crossing extension of access aisle shown. Exhibit B, Site Plan & Preliminary Plat.

99. The applicant should consider relocating the ADA parking spaces closer to the building entrances and sidewalk locations.

Applicant's Response: ADA spaces located proximate to building entrances in all instances. Exhibit B, Site Plan & Preliminary Plat.

100. Coordinate with the Village regarding proposed speed limits within the site and access roads.

Applicant's Response: Speed Limit signage to be reviewed with Village Department of Public Works and provided at Final Site Plan Approval submission.

101. No parking signs should be placed at all dead ends on the public roads.

Applicant's Response: No parking signs are shown in these locations.

SWPPP/DRAINAGE REPORT

102. Calculations supporting the sizing of storm sewers are to be provided in the drainage report.

Applicant's Response: Calculations have been provided. See Exhibit G, Revised Drainage Report.

103. As part of Final Plan submission, a SWPPP and NOI are to be provided for review and ultimately will require the approval from NYSDEC.

Applicant's Response: This comment will be addressed in the Final Site Plan Review submission.



104. The calculations show an increase in the peak rate of runoff to South Street at the north end of the project. If this condition is to remain, an analysis of the existing Village system receiving the runoff will be required to be provided.

Applicant's Response: Calculations on the capacity of the existing storm piping have been provided. See Exhibit G, Revised Drainage Report.

105. The drainage report is to be updated to include the off-site contributing impervious areas in the WQv calculations.

Applicant's Response: The Required WQv was calculated based on the on-site development. The WQv being provided in the stormwater wetlands includes off-site areas, as well as on-site. This has been quantified in the revised drainage report. See Exhibit G, Revised Drainage Report.

106. Regarding rooftop disconnection the location of the downspouts, and whether they discharge to grade or are connected, should be provided on the plans so the disconnections can be confirmed as meeting standards for WQv area reduction. In Soil Groups A & B disconnection of downspouts is encouraged to promote infiltration. In the area of the site with Soil Group D the disconnection benefit is minimized due to the impermeable nature of the soil which becomes exacerbated due to the compaction associated with construction. To support the credit associated with disconnection within the Soil Group D area we request a supporting letter from a geotechnical engineer determining whether soil enhancement is necessary to promote infiltration in these areas.

Applicant's Response: As part of the SWPPP for the Project, soil restoration will be required. Per the requirements outlined on page 5-65 of the NYSDEC Design Guide, this is an acceptable method for C/D soils. This will be covered in more detail in the Full SWPPP as part of the Final Site Plan Review submission.

107. WQv area reduction credit for tree planting should be limited to those potential large trees that are within 10' of an impervious surface. It does not appear as though the trees noted in the drainage report meet that



requirement. The landscaping plan shall be updated to identify the trees that meet this requirement.

Applicant's Response: Calculations have been provided. See Exhibit G, Revised Drainage Report.

108. Any alterations in impervious cover, rooftop disconnect, and/or tree planting numbers, will impact the RRV calculations. The drainage report may need to be updated accordingly.

Applicant's Response: Calculations have been provided. See Exhibit G, Revised Drainage Report.

109. The proposed bioretention filter is an effective method of obtaining WQv treatment. In this project it's designed to meet the minimum RRV required. Rain gardens are also proposed throughout the project site and should be included within the drainage report as they provide additional WQv treatment. The rain gardens should be designed and located to intercept as much impervious runoff as possible and sized to treat this runoff. The WQv provided by the rain gardens can then be added to the drainage calculations.

Applicant's Response: Calculations have been provided. See Exhibit G, Revised Drainage Report.

110. Please included sizing calculations for the hydrodynamic separator per Appendix B of the NYS SWDM.

Applicant's Response: Calculations have been provided. See Exhibit G, Revised Drainage Report.

111. Design related information should also be included in the WQv calculations for the proposed stormwater wetlands as they appear to provide the remainder of the WQv not provided by the bioretention filter and rain gardens.



Applicant's Response: Calculations have been provided. See Exhibit G, Revised Drainage Report.

112. The bioretention area soil specifications should be provided on the plans to ensure the soil meets the requirements of the NYS SWDM. The bioretention area shall be design in accordance with the NYS SWDM.

Applicant's Response: See Exhibit D, Civil Engineering Plans. (Sheet C202).

113. Stormwater wetland design shall be in accordance with the NYS SWDM. Stormwater wetlands must meet all requirements of stormwater ponds as well. A forebay must be constructed at each inflow point unless the inflow point provides less than 10% of the total design storm flow. A micropool must be provided at the outlet. Please see sections 6.1 and 6.2 of the NYS SWDM for more information.

Applicant's Response: Forebays and micropools have been added to the Grading Plans. See Exhibit D, Civil Engineering Plans. (Sheet C105 and C106).

114. Watershed maps should show soil hydrologic soil group overlays, label off site contours, clearly depict the features to which the CN factors are contributed and provide directional arrows for time of concentration paths. Please update the reports accordingly.

Applicant's Response: Overlays have been provided. See Exhibit G, Revised Drainage Report.

115. Please include the link path of flow from Watershed #1A through Watershed #1B on the Existing Watershed Boundaries Map.

Applicant's Response: Link path has been provided. See Exhibit G, Revised Drainage Report.

116. On the Proposed Watershed Boundaries Map one time of concentration node appears to be missing from Watershed #1A and the Watershed



#2A area and curve number information does not match the information within the report.

Applicant's Response: Added node and updated curve numbers. See Exhibit G, Revised Drainage Report.

117. If possible, provide a summary sheet printout from Hydrocad for the existing and proposed watershed with all subcatchments, reaches and links.

Applicant's Response: Summary sheets have been provided. See Exhibit G, Revised Drainage Report.

118. In Hydrocad, the Summary for Pond 3P sheet should include the surface area and storage at elevation 992.0 since this is the elevation of the overflow grate. Also, this summary appears to reflect that four (4) overflow grates are proposed when the plans identify only two (2).

Applicant's Response: The requested information will be provided. The number of grates have been updated to reflect the correct quantities. See Exhibit G, Revised Drainage Report.

119. In Hydrocad, the Summary for Ponds 3P and 4P show overflow spillways much longer than shown on the plan. The applicant should verify these spillways can be constructed at the invert elevation shown since the inverts are at the top contour elevation of the banks of the ponds.

Applicant's Response: More detail has been added to the drawings to show the top of embankment elevations. Likewise the spillways have been updated in HydroCAD.

120. Rating tables for outlet flows at critical stages should be developed for the various existing and proposed ponds incorporated into the drainage calculations.

Applicant's Response: Stage-Discharge rating tables have been provided. See Exhibit G, Revised Drainage Report.



121. In Hydrocad the method used to combine watershed subcatchments and pond outflows is a Reach. The Reaches should show the inflow hydrograph information listed and graphically.

Applicant's Response: A reach was added to combine the flows of watersheds #2A, 2B, and 2C. See Exhibit G, Revised Drainage Report.

122. In Table 3, Hydrograph Modeling Results the Pre-Developed WS #1A 100-yr runoff rate is different from on the Hydrocad calculation pages.

Applicant's Response: The discrepancy has been fixed. See Exhibit G, Revised Drainage Report.

TRAFFIC IMPACT STUDY

123. Erdman and Anthony will be providing comments regarding their review of the submitted Traffic Study prepared by SRF on a separate cover once completed.

Applicant's Response: Acknowledged. Since MRB issued its comment letter on February 19th, we have received Erdman Anthony's evaluation of the Traffic Study. Erdman Anthony's report concludes: "It does not appear that the proposed development will make significant adverse traffic impacts to the study intersections and the recommendation for no mitigation seems appropriate based on the results of the analysis."

Applicant's Response to Comments From Planning Board

1. Provide a count of parking spaces, including handicapped parking spaces.

Applicant's Response: Village Code requires 2 parking spaces for every dwelling unit. There are 146 parking spaces for residential use, and an additional 8 parking spaces for the Trumansburg Community Nursery School, totaling 154 parking spaces. Included in that total



are 5 ADA compliant parking spaces for residential use and 2 ADA compliant parking spaces for the Trumansburg Community Nursery School.

2. Are all buildings slab on grade?

Applicant's Response: All INHS buildings will be slab-on-grade, as will the Trumansburg Community Nursery School. It is possible that the purchasers of the market rate lots may choose to commission a home with a basement from Claudia Brenner.

3. Describe the stub driveways in the plan.

Applicant's Response: All driveways in the revised site plan submission connect to the buildings via sidewalks. It is possible that a purchaser of a market rate lot may choose not to install a sidewalk to connect their driveway to their home, but it has been shown on the plan regardless in order to conservatively calculate the amount of impervious surface across the entire site.

4. Provide a balance sheet of trees before and after.

Applicant's Response: Applicant has utilized the site survey as compared against the proposed on-site grading. This allowed the applicant to determine the number and location of all trees with a caliper of 8" or greater as identified on the survey to see which trees might be affected. The current site plan was developed in part to preserve as many mature trees as possible that mostly occur around the perimeter of the site. The count of the current canopy trees that exist on the site, are as follows: 47 deciduous canopy trees and 17 evergreen trees, a total of 64. Due to construction and required associated grading, 33 deciduous canopy trees and 8 evergreen trees will be preserved. To mitigate the tree removals, 180 new deciduous canopy trees and 96 evergreen trees are proposed. This would bring the final after construction tree count to 213 deciduous canopy trees and 104 evergreen trees, a total of 317. Factoring in the current tree count, the total tree count on site would increase by 253 trees.

5. Describe "no mow" lawn seed mix.

Applicant's Response: "No Mow" lawn seed mix is an eco-friendly, low maintenance and drought tolerant blend of fine fescue grasses. The fine fescue seed mix establishes quickly to minimize soil erosion. It inhibits invasive plants and weeds. It does not require fertilization or



irrigation once established. It accommodates foot traffic well while growing only to 6" to 8" and then stops, allowing for a variety of uses. While this seed mix can be mowed, it does not require any maintenance to create the appearance of a well-managed landscape. Photographs depicting "No Mow" lawn have been included as **Exhibit H, Photographs of "No Mow" Lawn**.

6. Reexamine the entrance/exit to the nursery school.

Applicant's Response: This comment has been addressed in the revised submittal.

7. Is there any designated public green space?

Applicant's Response: Applicants have opted to allow public access to any green space on Site that is owned by the Applicant. Nearly a mile of walking trails are proposed. There is no green space deeded to the Village, which means that the Village will not be responsible for any maintenance or improvements to the green space.

8. Are electric lines underground?

Applicant's Response: Electric lines will be buried for aesthetic reasons.

9. On the building elevations, some show windows with sills flush with the porch roof surface. Snow will collect against the windows.

Applicant's Response: This comment will be addressed when architecture drawings next advance, but we understand the concern and will ensure it is addressed.

10. For both access roads, provide the distances from the lot lines and the road to the adjoining buildings; the width of pavement, curb to side yard, and other applicable measurements.

Applicant's Response: Distances from lot lines to adjoining buildings, width of pavement and curb width have been delineated on enlarged road plans. Applicant will ensure, through continued consultation with the Department of Public Works, that the road layout and design is compliant with subdivision regulations and is appropriately sized to facilitate traffic and access needs. See **Exhibit I, Enlarged Road Plans**.



Rick Geiger, Chair
Page 31

March 15, 2018

11. In connection with the proposed access roads, show setbacks for neighboring properties and discuss whether either road will result in adjoining lots being turned into corner lots.

Applicant's Response: Setback distances for neighboring properties have been delineated on the enlarged road plans. It would appear that the installation of a new public road to Pennsylvania Avenue will create a corner lot for both adjoining lots, which front on Pennsylvania, although we note that such determination would have to be made by the Zoning Officer. That said, Section 707 of the Village Zoning Code provides that setbacks on side yards for corner lots are $\frac{1}{2}$ the front yard setback, which is 50 feet. There are no structures on the lot north of the new road within this setback. There is one structure, a garage, on the lot to the south within this setback but it would simply become a non-conforming structure under Article II of the Village Zoning Code. Nothing in Section 707 suggests that a private road such as the one proposed to connect to South Street would make adjoining lots into corner lots, but again, such a determination would be up to the Zoning Officer. **See Exhibit I, Enlarged Road Plans.**

The Applicant is committed to working with the Planning Board to design and develop a Project that will benefit the Village. If you have any questions with the information contained herein, please do not hesitate to contact the undersigned.

Very truly yours,

Phillips Lytle LLP

By 

Adam S. Walters

Enclosure(s)

cc: Matt Johnston, Zoning Officer and Planner
Lance Brabant, CPESC, Director of Planning Services, MRB Group
Joseph L. Bowes, Director of Real Estate Development, INHS
Alena Fast, Real Estate Developer, INHS
Claudia Brenner, Architect

Exhibit A

ITHACA NEIGHBORHOOD HOUSING SERVICES & SUNDIAL PROPERTY DEVELOPMENT, LLC

46 SOUTH STREET TRUMANSBURG, NEW YORK
PRELIMINARY SITE PLAN AND SUBDIVISION PLAN

DATE: MARCH 16, 2018

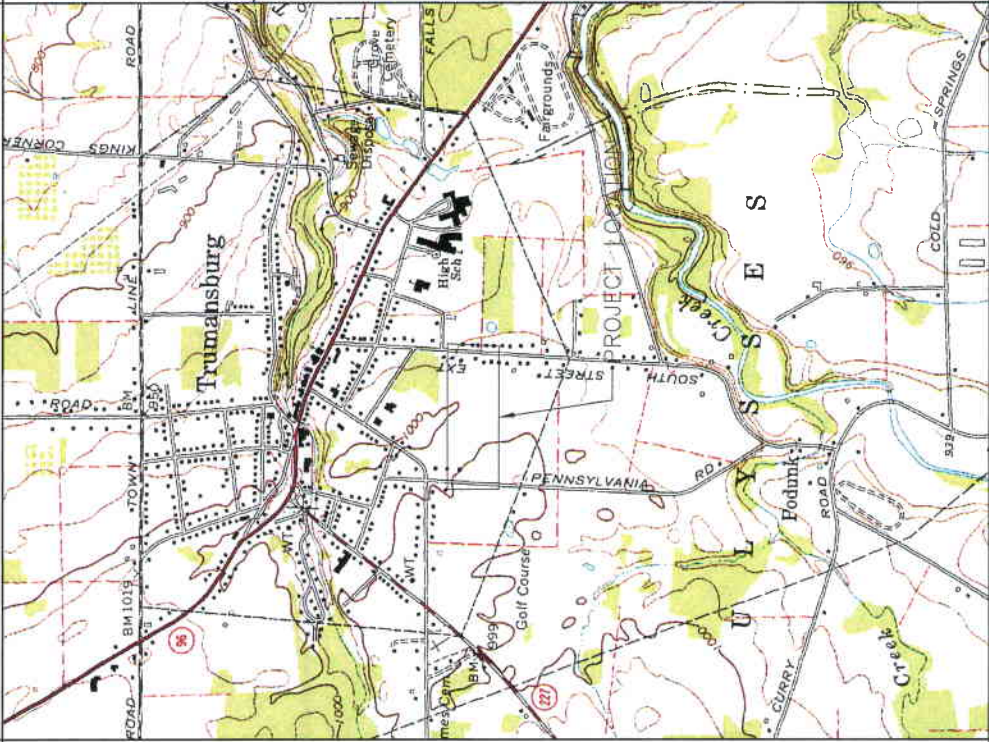
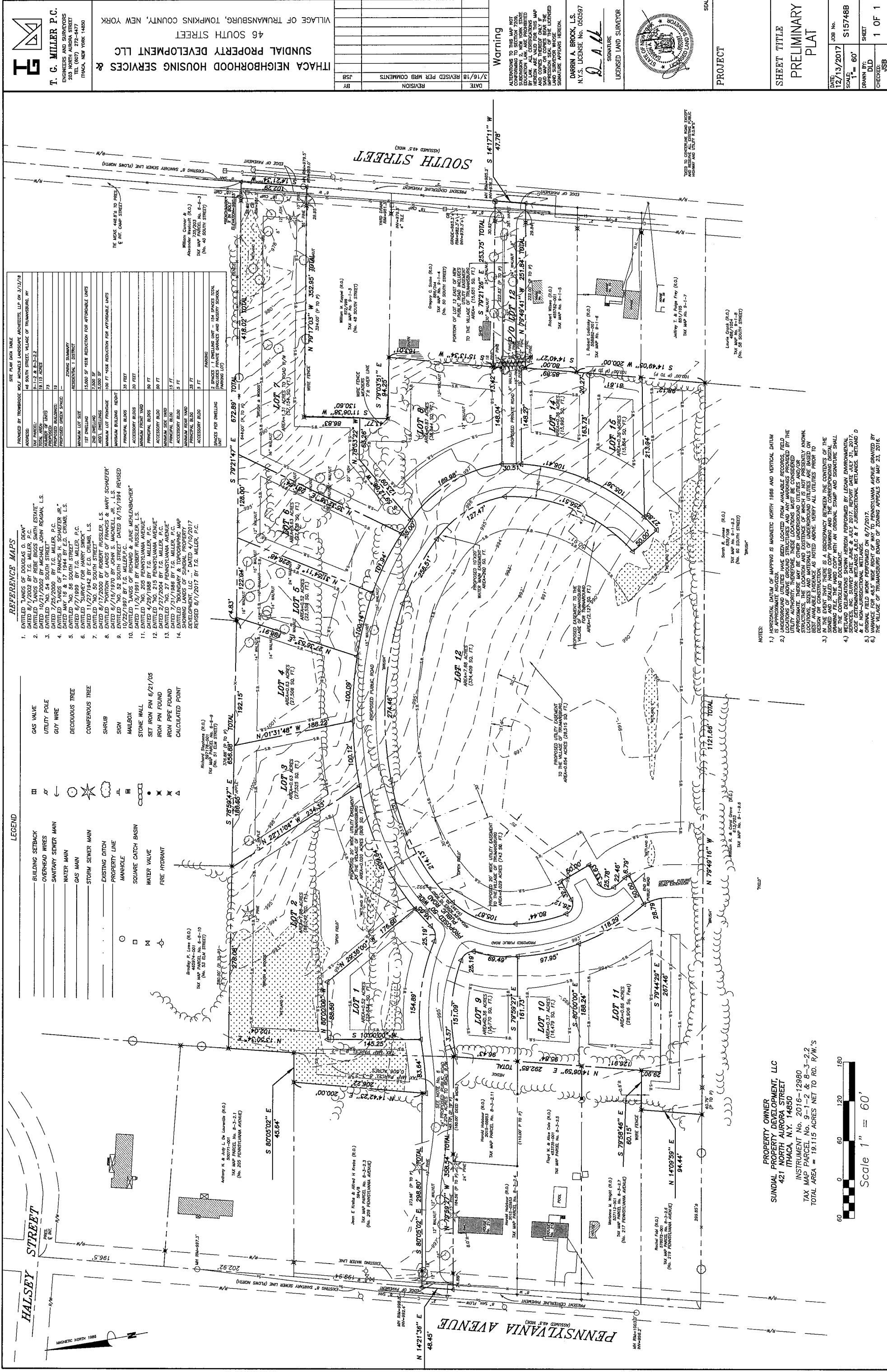
DRAWING INDEX	GENERAL NOTES	VICINITY MAP	SIGNATURES
<div>10F1 10F1</div> <div>BOUNDARY & TOPOGRAPHIC MAP PRELIMINARY PLAN</div> <div>C101 C102 C103 C104 C105 C106 C107 C108 C201 C301 C302 C303 C401 C402 C501 C501 C601 C602</div> <div>L101 L102 L103 L104 L105 L106</div> <div>AP102 AP103 AP104 AP109 AP110</div> <div>EXISTING CONDITIONS PLAN EROSION AND SEDIMENT CONTROL PLAN DRAINAGE PLAN DRAINAGE PLAN GRADING PLAN GRADING PLAN UTILITY PLAN UTILITY PLAN DETAILS WATER PROFILES WATER PROFILES WATER PROFILES SANITARY PROFILES SANITARY PROFILES STORM PROFILES ROAD PROFILES ROAD PROFILES</div> <div>SITE MATERIALS PLAN-WEST SITE MATERIALS PLAN-EAST SITE LIGHTING & SIGNAGE PLAN LANDSCAPE PLAN LANDSCAPE PLANT LIST SITE DETAILS</div> <div>MULTI-FAMILY BUILDING PERSPECTIVES MULTI-FAMILY BUILDING PERSPECTIVES MULTI-FAMILY BUILDING PERSPECTIVES TOWNHOUSE BUILDING 'C1' EXTERIOR ELEVATIONS TOWNHOUSE BUILDING 'C2' EXTERIOR ELEVATIONS</div>	<div>- TOPOGRAPHIC INFORMATION SHOWN IS BASED ON MAP TITLED "BOUNDARY & TOPOGRAPHIC MAP" SHOWING LANDS OF SUNDIAL PROPERTY DEVELOPMENT, LLC, PREPARED BY T. G. MILLER, P.C. IN 1999. ALL INFORMATION COLLECTED IN FIELD BY T. G. MILLER, P.C. AS WELL AS ADDITIONAL INFORMATION COLLECTED IN FIELD FOLLOWING ISSUANCE OF MAP.</div> <div>- EXISTING UTILITIES SHOWN ARE IN APPROXIMATE LOCATION ONLY. VERIFY EXACT LOCATION OF ALL UTILITIES BEFORE BEGINNING CONSTRUCTION. NOTIFY DIG SAFELY NEW YORK (D.S.N.Y. 1-800-992-7962) A MINIMUM 3 WORKING DAYS PRIOR TO BEGINNING CONSTRUCTION.</div> <div>- ALL DIMENSIONS TO BUILDINGS OR CURBS ARE TO EXTERIOR FACE OF BUILDING UNLESS OTHERWISE NOTED. ALL DIMENSIONS TO UTILITIES ARE TO CENTERLINE OR PARALLEL TO THE LINES FROM WHICH THEY ARE DRAWN UNLESS OTHERWISE NOTED.</div> <div>- DATUM OF ELEVATIONS IS APPROXIMATE U.S.G.S.</div> <div>- POSITIVE ELEVATIONS OF FINISHES AT BUILDING ENTRANCES WITH ARCHITECTURAL DRAWINGS OF BUILDING.</div> <div>- CONFORM TO CONVENTIONS BETWEEN EXISTING UTILITIES AND PROPOSED SANITARY AND STORM SEWERS PRIOR TO LAYING PIPE OR INSTALLING STRUCTURES.</div>		<div>APPROVED BY: PLANNING BOARD CHAIRMAN _____ VILLAGE ENGINEER _____ DPW SUPERVISOR _____</div> <div><div><div>THOMAS WOLF MICHAELS</div><div>TWMA</div><div>LANDSCAPE ARCHITECTS</div><div>1001 W. Seneca St., 3rd Fl. ITHACA, NY 14850 507.273.1200</div></div><div><div>HOLTARCHITECTS</div><div>Architecture Planning Interior Design</div><div>615 W. Seneca St., 3rd Fl. ITHACA, NY 14850 p 507.273.7500 f 507.273.0475</div></div><div><div>IG</div><div>T. G. MILLER P.C.</div><div>ENGINEERS AND SURVEYORS</div><div>203 NORTH AURORA STREET P.O. BOX 777 ITHACA, NEW YORK 14851</div></div></div>

Exhibit B



T. C. MILLER P.C.
ENGINEERS AND SURVEYORS
203 NORTH AURORA STREET
ITHACA, NEW YORK 14850

ITHACA NEIGHBORHOOD HOUSING SERVICES & SUNDIAL PROPERTY DEVELOPMENT LLC
46 SOUTH STREET
VILLAGE OF TRUMANSBURG, TOMPKINS COUNTY, NEW YORK

REVISION	DATE	BY
3/16/18	REVISED PER MRB COMMENTS	JSB

Warning
ATTENTION: THIS MAP NOT BEING USED FOR ANY PURPOSES OTHER THAN THAT FOR WHICH IT WAS DESIGNED. THE USER OF THIS MAP ASSUMES ALL LIABILITY FOR ANY DAMAGE OR INJURY RESULTING FROM THE USE OF THIS MAP. THE USER OF THIS MAP ASSUMES ALL LIABILITY FOR ANY DAMAGE OR INJURY RESULTING FROM THE USE OF THIS MAP.

DARRIN A. BROCK, L.S.
N.Y.S. LICENSE NO. 055597
D.A.B.
SIGNATURE
LICENSED LAND SURVEYOR



PROJECT

SHEET TITLE
PRELIMINARY
PLAT

DATE: 12/13/2017
JOB NO.: S15748B
SCALE: 1" = 60'
DRAWN BY: DLD
CHECKED: JSB
SHEET: 1 OF 1

T.G. MILLER, P.C.
ENGINEERS AND SURVEYORS
203 NORTH AURORA STREET
ITWACA, NEW YORK 14850
www.tgmillerpc.com
807-272-8477 fax
807-273-8322 fax

DATE	REVISION	BY
1/16/10	PER VILLAGE COMMENTS	RK

1000

IT IS A VIOLATION OF LAW FOR ANY PERSON, UNLESS ACTING UNDER THE DIRECTION OF A LICENSED LANDSCAPE ARCHITECT, TO ALTER ANY ITEM ON THIS DOCUMENT WHO ALTERS THIS DOCUMENT WITHOUT AFFIXING HIS OR HER SEAL AND THE NOTATION "ALTERED BY" FOLLOWED BY HIS OR HER SIGNATURE AND A SPECIFIC DESCRIPTION OF ALTERATIONS.

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46 South Street
Sundial Property Development LLC
Trumansburg, New York

DATE:	12/13/2017
PROJECT:	17003
DRAWN BY:	RK
CHECKED:	

SITE MATERIALS
PLAN - EAST

L-102



Exhibit C



DEPARTMENT OF THE ARMY
BUFFALO DISTRICT, CORPS OF ENGINEERS
1776 NIAGARA STREET
BUFFALO, NEW YORK 14207-3199

RECEIVED
JAN 29 2018

REPLY TO

January 25, 2018

Regulatory Branch

SUBJECT: Preliminary and Approved Jurisdictional Determination Transmittal Letter, File No. 2017-00927

Ithaca Neighborhood Housing Services
115 West Clinton Street
Ithaca, New York 14850
Attn: Joseph Bowes

Dear Mr. Bowes:

I am writing in regard to a request, made on your behalf by Mr. Ron LeCain, for a Jurisdictional Determination (JD) associated with aquatic resources delineated on property located adjacent to the South Street Extension, Village of Trumansburg, Tompkins County, New York.

Preliminary JD: Preliminary JDs are non-binding written indications that there may be WOUS on your parcel and approximate locations of those waters. Preliminary JDs are advisory in nature and may not be appealed.

I have evaluated the wetland delineation map and report and determined that the wetland and water boundaries identified in Review Area 2 accurately represent on-site conditions pertaining to Wetlands A, B, C, and F.

Pursuant to Regulatory Guidance Letter 16-01, any permit application made in reliance on this Preliminary JD will be evaluated as though all wetlands or waters on the site are regulated by the Corps. Further, all waters, including wetlands will be used for purposes of assessing the area of project related impacts and compensatory mitigation. If you require a definitive response regarding Department of the Army jurisdiction for any or all of the waters identified on the submitted drawings, you may request an approved jurisdictional determination from this office. If an approved jurisdictional determination is requested, please be aware that this is often a lengthy process and we may require the submittal of additional information.

I have enclosed the signed Preliminary JD Form dated January 25, 2018, with this letter. The form and attached table identify the extent of waters on the site and specific terms and conditions of the Preliminary JD.

In accordance with Regulatory Guidance Letter 05-02, "Preliminary jurisdictional determinations are not definitive determinations of areas within regulatory jurisdiction and do not have expiration dates." However, I strongly recommend that the boundaries of waters of the United States be re-evaluated by a qualified wetland biologist after five years of the date of this letter. This will ensure that any changes are appropriately identified and you do not inadvertently incur a violation of Federal law while constructing your project or working on your project site.

Regulatory Branch

SUBJECT: Preliminary and Approved Jurisdictional Determination Transmittal Letter, File No. 2017-00927

Approved JD: Based on the information provided, I have determined that there is no clear surface water connection or ecological continuum between Wetlands D and E (Review Area 1) on the parcel and a surface tributary system to a navigable water of the United States.

These wetlands are outside Department of the Army jurisdiction as they do not meet the criteria for a jurisdictional WOUS according to 33 CFR Part 328.3(a)(1-7) as follows:

1. does not/has not supported interstate or foreign commerce;
2. is not an interstate water/wetland;
3. the degradation or destruction of which would not affect interstate or foreign commerce and does not include such waters:
 - (i) which are or could be used by interstate or foreign travelers for recreational or other purposes; or
 - (ii) from which fish or shellfish are or could be taken and sold in interstate or foreign commerce; or
 - (iii) which are used or could be used for industrial purpose by industries in interstate commerce
4. is not an impoundment of water otherwise defined as WOUS under the definition;
5. is not a tributary of waters identified in paragraphs (a)(1)-(4) of this section;
6. is not a territorial sea;
7. is not wetland adjacent to waters (other than waters that are themselves wetlands) identified in paragraphs (a)(1)-(6) of this section.

Therefore, these waters are considered isolated, non-navigable, intrastate waters and not regulated under Section 404 of the CWA. Accordingly, Department of the Army authorization is not required to commence work in these areas.

Attached is an Approved JD, dated January 25, 2018 for Wetlands D and E (Review Area 1). If you object to this determination, you may request an administrative appeal under USACE regulations at 33 CFR Part 331. Enclosed you will find a Notification of Appeal Process (NAP) fact sheet and Request for Appeal (RFA) form. If you request to appeal the above determination, you must submit a completed RFA form within 60 days of the date on this letter to the Great Lakes/Ohio River Division Office at the following address:

Review Officer
Great Lakes and Ohio River Division
CELRD-PDS-O
550 Main Street, Room 10524
Cincinnati, OH 45202-3222
Phone: 513-684-6212

In order for an RFA to be accepted, the USACE must determine that it is complete, that it meets the criteria for appeal under 33 CFR Part 331.5, and that it has been received by the Division Office within 60 days of the date of the NAP. Should you decide to submit an RFA form, it must be received at the above address by **March 26, 2018**. It is not necessary to submit an RFA to the Division office if you do not object to the determination in this letter.

Regulatory Branch

SUBJECT: Preliminary and Approved Jurisdictional Determination Transmittal Letter, File No. 2017-00927

Note that this delineation/determination may not be valid for the wetland conservation provisions of the Food Security Act of 1985, as amended. If you or your tenant are USDA program participants, or anticipate participation in USDA programs, you should request a certified wetland determination from the local office of the Natural Resource Conservation Service (NRCS) prior to starting work.

A copy of this correspondence has been sent to Ron LeCain, LeCain Environmental Services, Inc.

Questions pertaining to this matter should be directed to me at 716-879-6330, by writing to the following address: U.S. Army Corps of Engineers, 7413 County House Road, Auburn, New York 13021, or by e-mail at: judy.a.robinson@usace.army.mil.

Sincerely,



Judy Robinson, Biologist
Project Manager

Enclosures

APPROVED JURISDICTIONAL DETERMINATION FORM
U.S. Army Corps of Engineers

This form should be completed by following the instructions provided in Section IV of the JD Form Instructional Guidebook.

SECTION I: BACKGROUND INFORMATION

A. REPORT COMPLETION DATE FOR APPROVED JURISDICTIONAL DETERMINATION (JD): January 25, 2018

B. DISTRICT OFFICE, FILE NAME, AND NUMBER: Buffalo District; Auburn Field Office; Ithaca Housing Services (South Street Extension); File No. 2017-00927

C. PROJECT LOCATION AND BACKGROUND INFORMATION:

State: New York County: Tompkins City: Ithaca
Center coordinates of site (lat/long in degree decimal format): Lat: 42.53553°N Long: -76.66151°W
Name of nearest waterbody: Trumansburg Creek
Name of nearest Traditional Navigable Water (TNW) into which the aquatic resource flows: N/A
Name of watershed or Hydrologic Unit Code (HUC): 4140201

- ☒ Check if map/diagram of review area and/or potential jurisdictional areas is/are available upon request.
☐ Check if other sites (e.g., offsite mitigation sites, disposal sites, etc...) are associated with this action and are recorded on a different JD form.

D. REVIEW PERFORMED FOR SITE EVALUATION (CHECK ALL THAT APPLY):

- ☒ Office (Desk) Determination. Date: January 11, 2018
☐ Field Determination. Date(s):

SECTION II: SUMMARY OF FINDINGS

A. RHA SECTION 10 DETERMINATION OF JURISDICTION.

There **ARE NO** "navigable waters of the U.S." within Rivers and Harbors Act (RHA) jurisdiction (as defined by 33 CFR part 329) in the review area. [Required]

- ☐ Waters subject to the ebb and flow of the tide.
☒ Waters are presently used, or have been used in the past, or may be susceptible for use to transport interstate or foreign commerce.
Explain:

B. CWA SECTION 404 DETERMINATION OF JURISDICTION.

There **ARE NO** "waters of the U.S." within Clean Water Act (CWA) jurisdiction (as defined by 33 CFR part 328) in the review area. [Required]

1. Waters of the U.S.

a. Indicate presence of waters of U.S. in review area (check all that apply):¹

- ☐ TNWs, including territorial seas
☐ Wetlands adjacent to TNWs
☐ Relatively permanent waters² (RPWs) that flow directly or indirectly into TNWs
☐ Non-RPWs that flow directly or indirectly into TNWs
☒ Wetlands directly abutting RPWs that flow directly or indirectly into TNWs
☐ Wetlands adjacent to but not directly abutting RPWs that flow directly or indirectly into TNWs
☐ Wetlands adjacent to non-RPWs that flow directly or indirectly into TNWs
☐ Impoundments of jurisdictional waters
☐ Isolated (interstate or intrastate) waters, including isolated wetlands

b. Identify (estimate) size of waters of the U.S. in the review area:

Non-wetland waters: linear feet: width (ft) and/or acres.
Wetlands: acres.

c. Limits (boundaries) of jurisdiction based on: ~~Pick List~~

Elevation of established OHWM (if known):

2. Non-regulated waters/wetlands (check if applicable):³

- ☒ Potentially jurisdictional waters and/or wetlands were assessed within the review area and determined to be not jurisdictional.
Explain: Wetland D Emergent 0.01 acre
Wetland E Emergent 0.05 acre

¹ Boxes checked below shall be supported by completing the appropriate sections in Section III below.

² For purposes of this form, an RPW is defined as a tributary that is not a TNW and that typically flows year-round or has continuous flow at least "seasonally" (e.g., typically 3 months).

³ Supporting documentation is presented in Section III.F.

Emergent Wetlands D and E are outside Department of the Army jurisdiction as they not meet the criteria for a jurisdictional water of the United States according to 33 CFR Part 328.3(a)(1-7) as follows:

1. does not/has not supported interstate or foreign commerce;
2. is not an interstate water/wetland;
3. the degradation or destruction of which would not affect interstate or foreign commerce and does not include such waters:
 - (i) which are or could be used by interstate or foreign travelers for recreational or other purposes; or
 - (ii) from which fish or shellfish are or could be taken and sold in interstate or foreign commerce; or
 - (iii) which are used or could be used for industrial purpose by industries in interstate commerce
4. is not an impoundment of water otherwise defined as WOUS under the definition;
5. is not a tributary of waters identified in paragraphs (a)(1)-(4) of this section;
6. is not a territorial sea;
7. is not wetland adjacent to waters (other than waters that are themselves wetlands) identified in paragraphs (a)(1)-(6) of this section;

In addition these wetlands are both depressional, emergent wetlands within a former agricultural field within an area having a hydric soil rating of 10. Wetland D is approximately 500 feet from the nearest conveyance and Wetland E is approximately 250 feet from the same conveyance, which is an unnamed tributary to Trumansburg Creek, which carries flow from Wetland F. (Note that Wetland F is not within the Approved JD Review Area 1 boundary, and along with Wetlands A, B, and C, is under review as a Preliminary JD). Further, due to topography and distance to the nearest tributary, the presence of a shallow subsurface flow connection is very unlikely.

SECTION III: CWA ANALYSIS

A. TNWs AND WETLANDS ADJACENT TO TNWs

The agencies will assert jurisdiction over TNWs and wetlands adjacent to TNWs. If the aquatic resource is a TNW, complete Section III.A.1 and Section III.D.1. only; if the aquatic resource is a wetland adjacent to a TNW, complete Sections III.A.1 and 2 and Section III.D.1.; otherwise, see Section III.B below.

1. **TNW**
Identify TNW:
Summarize rationale supporting determination:
2. **Wetland adjacent to TNW**
Summarize rationale supporting conclusion that wetland is "adjacent":

B. CHARACTERISTICS OF TRIBUTARY (THAT IS NOT A TNW) AND ITS ADJACENT WETLANDS (IF ANY):

This section summarizes information regarding characteristics of the tributary and its adjacent wetlands, if any, and it helps determine whether or not the standards for jurisdiction established under *Rapanos* have been met.

The agencies will assert jurisdiction over non-navigable tributaries of TNWs where the tributaries are "relatively permanent waters" (RPWs), i.e. tributaries that typically flow year-round or have continuous flow at least seasonally (e.g., typically 3 months). A wetland that directly abuts an RPW is also jurisdictional. If the aquatic resource is not a TNW, but has year-round (perennial) flow, skip to Section III.D.2. If the aquatic resource is a wetland directly abutting a tributary with perennial flow, skip to Section III.D.4.

A wetland that is adjacent to but that does not directly abut an RPW requires a significant nexus evaluation. Corps districts and EPA regions will include in the record any available information that documents the existence of a significant nexus between a relatively permanent tributary that is not perennial (and its adjacent wetlands if any) and a traditional navigable water, even though a significant nexus finding is not required as a matter of law.

If the waterbody⁴ is not an RPW, or a wetland directly abutting an RPW, a JD will require additional data to determine if the waterbody has a significant nexus with a TNW. If the tributary has adjacent wetlands, the significant nexus evaluation must consider the tributary in combination with all of its adjacent wetlands. This significant nexus evaluation that combines, for analytical purposes, the tributary and all of its adjacent wetlands is used whether the review area identified in the JD request is the tributary, or its adjacent wetlands, or both. If the JD covers a tributary with adjacent wetlands, complete Section III.B.1 for the tributary, Section III.B.2 for any onsite wetlands, and Section III.B.3 for all wetlands adjacent to that tributary, both onsite and offsite. The determination whether a significant nexus exists is determined in Section III.C below.

⁴ Note that the Instructional Guidebook contains additional information regarding swales, ditches, washes, and erosional features generally and in the arid West.

1. Characteristics of non-TNWs that flow directly or indirectly into TNW

(i) General Area Conditions:

Watershed size: Pick List
 Drainage area: Pick List
 Average annual rainfall: _____ inches

(ii) Physical Characteristics:

(a) Relationship with TNW:

- ☐ Tributary flows directly into TNW.
☐ Tributary flows through Pick List tributaries before entering TNW
 Project waters are Pick List river miles from TNW
 Project waters are Pick List river miles from RPW
 Project waters are Pick List aerial (straight) miles from TNW
 Project waters are Pick List aerial (straight) miles from RPW
 Project waters cross or serve as state boundaries. Explain:
 Identify flow route to TNW⁵:
 Tributary stream order, if known:

(b) General Tributary Characteristics (check all that apply):

Tributary is: ☐ Natural
☐ Artificial (man-made). Explain:
☐ Manipulated (man-altered). Explain:

Tributary properties with respect to top of bank (estimate):

Average width: _____ feet
 Average depth: _____ feet
 Average side slopes: Pick List

Primary tributary substrate composition (check all that apply):

- | | | |
|--|--|-----------------------------------|
| <input type="checkbox"/> Silts | <input type="checkbox"/> Sands | <input type="checkbox"/> Concrete |
| <input type="checkbox"/> Cobbles | <input type="checkbox"/> Gravel | <input type="checkbox"/> Muck |
| <input type="checkbox"/> Bedrock | <input type="checkbox"/> Vegetation. Type/% cover: | |
| <input type="checkbox"/> Other. Explain: | | |

Tributary condition/stability [e.g., highly eroding, sloughing banks]. Explain:

Presence of run/riffle/pool complexes. Explain:

Tributary geometry: Pick List

Tributary gradient (approximate average slope): _____ %

(c) Flow:

Tributary provides for: Pick List

Estimate average number of flow events in review area/year: Pick List

Describe flow regime:

Other information on duration and volume:

Surface flow is: Pick List. Characteristics:

Subsurface flow: Pick List. Explain findings:

☐ Dye (or other) test performed:

Tributary has (check all that apply):

☐ Bed and banks

☐ OHWM⁶ (check all indicators that apply):

- | | |
|--|---|
| <input type="checkbox"/> clear, natural line impressed on the bank | <input type="checkbox"/> the presence of litter and debris |
| <input type="checkbox"/> changes in the character of soil | <input type="checkbox"/> destruction of terrestrial vegetation |
| <input type="checkbox"/> shelving | <input type="checkbox"/> the presence of wrack line |
| <input type="checkbox"/> vegetation matted down, bent, or absent | <input type="checkbox"/> sediment sorting |
| <input type="checkbox"/> leaf litter disturbed or washed away | <input type="checkbox"/> scour |
| <input type="checkbox"/> sediment deposition | <input type="checkbox"/> multiple observed or predicted flow events |
| <input type="checkbox"/> water staining | <input type="checkbox"/> abrupt change in plant community |
| <input type="checkbox"/> other (list): | |

☐ Discontinuous OHWM.⁷ Explain:

⁵ Flow route can be described by identifying, e.g., tributary a, which flows through the review area, to flow into tributary b, which then flows into TNW.

⁶ A natural or man-made discontinuity in the OHWM does not necessarily sever jurisdiction (e.g., where the stream temporarily flows underground, or where the OHWM has been removed by development or agricultural practices). Where there is a break in the OHWM that is unrelated to the waterbody's flow regime (e.g., flow over a rock outcrop or through a culvert), the agencies will look for indicators of flow above and below the break.

⁷ Ibid.

If factors other than the OHWM were used to determine lateral extent of CWA jurisdiction (check all that apply):

- | | |
|--|--|
| <input checked="" type="checkbox"/> High Tide Line indicated by: | <input type="checkbox"/> Mean High Water Mark indicated by: |
| <input type="checkbox"/> oil or scum line along shore objects | <input type="checkbox"/> survey to available datum; |
| <input type="checkbox"/> fine shell or debris deposits (foreshore) | <input type="checkbox"/> physical markings; |
| <input type="checkbox"/> physical markings/characteristics | <input type="checkbox"/> vegetation lines/changes in vegetation types. |
| <input type="checkbox"/> tidal gauges | |
| <input type="checkbox"/> other (list): | |

(iii) **Chemical Characteristics:**

Characterize tributary (e.g., water color is clear, discolored, oily film; water quality; general watershed characteristics, etc.).

Explain:

Identify specific pollutants, if known:

(iv) **Biological Characteristics. Channel supports (check all that apply):**

- ☐ Riparian corridor. Characteristics (type, average width):
- ☐ Wetland fringe. Characteristics:
- ☐ Habitat for:
 - ☐ Federally Listed species. Explain findings:
 - ☐ Fish/spawn areas. Explain findings:
 - ☐ Other environmentally-sensitive species. Explain findings:
 - ☐ Aquatic/wildlife diversity. Explain findings:

2. **Characteristics of wetlands adjacent to non-TNW that flow directly or indirectly into TNW**

(i) **Physical Characteristics:**

(a) General Wetland Characteristics:

Properties:

Wetland size: acres

Wetland type. Explain:

Wetland quality. Explain:

Project wetlands cross or serve as state boundaries. Explain:

(b) General Flow Relationship with Non-TNW:

Flow is: ~~Pick List~~. Explain:

Surface flow is: ~~Pick List~~

Characteristics:

Subsurface flow: ~~Pick List~~. Explain findings:

☐ Dye (or other) test performed:

(c) Wetland Adjacency Determination with Non-TNW:

- ☐ Directly abutting
- ☐ Not directly abutting
 - ☐ Discrete wetland hydrologic connection. Explain:
 - ☐ Ecological connection. Explain:
 - ☐ Separated by berm/barrier. Explain:

(d) Proximity (Relationship) to TNW

Project wetlands are ~~Pick List~~ river miles from TNW.

Project waters are ~~Pick List~~ aerial (straight) miles from TNW.

Flow is from: ~~Pick List~~.

Estimate approximate location of wetland as within the ~~Pick List~~ floodplain.

(ii) **Chemical Characteristics:**

Characterize wetland system (e.g., water color is clear, brown, oil film on surface; water quality; general watershed characteristics; etc.). Explain:

Identify specific pollutants, if known:

(iii) **Biological Characteristics. Wetland supports (check all that apply):**

- ☐ Riparian buffer. Characteristics (type, average width):
- ☐ Vegetation type/percent cover. Explain:
- ☐ Habitat for:
 - ☐ Federally Listed species. Explain findings:
 - ☐ Fish/spawn areas. Explain findings:
 - ☐ Other environmentally-sensitive species. Explain findings:

☐ Aquatic/wildlife diversity. Explain findings:

3. Characteristics of all wetlands adjacent to the tributary (if any)

All wetland(s) being considered in the cumulative analysis: Pick List

Approximately () acres in total are being considered in the cumulative analysis.

For each wetland, specify the following:

Directly abuts? (Y/N)

Size (in acres)

Directly abuts? (Y/N)

Size (in acres)

Summarize overall biological, chemical and physical functions being performed:

C. SIGNIFICANT NEXUS DETERMINATION

A significant nexus analysis will assess the flow characteristics and functions of the tributary itself and the functions performed by any wetlands adjacent to the tributary to determine if they significantly affect the chemical, physical, and biological integrity of a TNW. For each of the following situations, a significant nexus exists if the tributary, in combination with all of its adjacent wetlands, has more than a speculative or insubstantial effect on the chemical, physical and/or biological integrity of a TNW. Considerations when evaluating significant nexus include, but are not limited to the volume, duration, and frequency of the flow of water in the tributary and its proximity to a TNW, and the functions performed by the tributary and all its adjacent wetlands. It is not appropriate to determine significant nexus based solely on any specific threshold of distance (e.g. between a tributary and its adjacent wetland or between a tributary and the TNW). Similarly, the fact an adjacent wetland lies within or outside of a floodplain is not solely determinative of significant nexus.

Draw connections between the features documented and the effects on the TNW, as identified in the *Rapanos* Guidance and discussed in the Instructional Guidebook. Factors to consider include, for example:

- Does the tributary, in combination with its adjacent wetlands (if any), have the capacity to carry pollutants or flood waters to TNWs, or to reduce the amount of pollutants or flood waters reaching a TNW?
- Does the tributary, in combination with its adjacent wetlands (if any), provide habitat and lifecycle support functions for fish and other species, such as feeding, nesting, spawning, or rearing young for species that are present in the TNW?
- Does the tributary, in combination with its adjacent wetlands (if any), have the capacity to transfer nutrients and organic carbon that support downstream foodwebs?
- Does the tributary, in combination with its adjacent wetlands (if any), have other relationships to the physical, chemical, or biological integrity of the TNW?

Note: the above list of considerations is not inclusive and other functions observed or known to occur should be documented below:

1. Significant nexus findings for non-RPW that has no adjacent wetlands and flows directly or indirectly into TNWs. Explain findings of presence or absence of significant nexus below, based on the tributary itself, then go to Section III.D:
2. Significant nexus findings for non-RPW and its adjacent wetlands, where the non-RPW flows directly or indirectly into TNWs. Explain findings of presence or absence of significant nexus below, based on the tributary in combination with all of its adjacent wetlands, then go to Section III.D:
3. Significant nexus findings for wetlands adjacent to an RPW but that do not directly abut the RPW. Explain findings of presence or absence of significant nexus below, based on the tributary in combination with all of its adjacent wetlands, then go to Section III.D:

D. DETERMINATIONS OF JURISDICTIONAL FINDINGS. THE SUBJECT WATERS/WETLANDS ARE (CHECK ALL THAT APPLY):

1. TNWs and Adjacent Wetlands. Check all that apply and provide size estimates in review area:

☒ TNWs: linear feet width (ft), Or, acres.

☒ Wetlands adjacent to TNWs: acres.

2. RPWs that flow directly or indirectly into TNWs.

☒ Tributaries of TNWs where tributaries typically flow year-round are jurisdictional. Provide data and rationale indicating that tributary is perennial:

☒ Tributaries of TNW where tributaries have continuous flow "seasonally" (e.g., typically three months each year) are jurisdictional. Data supporting this conclusion is provided at Section III.B. Provide rationale indicating that tributary flows seasonally:

Provide estimates for jurisdictional waters in the review area (check all that apply):

☒ Tributary waters: linear feet width (ft).

☒ Other non-wetland waters: acres.

Identify type(s) of waters:

3. **Non-RPWs⁸ that flow directly or indirectly into TNWs.**

- ☐ Waterbody that is not a TNW or an RPW, but flows directly or indirectly into a TNW, and it has a significant nexus with a TNW is jurisdictional. Data supporting this conclusion is provided at Section III.C.

Provide estimates for jurisdictional waters within the review area (check all that apply):

- ☐ Tributary waters: linear feet width (ft).
☐ Other non-wetland waters: acres.

Identify type(s) of waters:

4. **Wetlands directly abutting an RPW that flow directly or indirectly into TNWs.**

- ☒ Wetlands directly abut RPW and thus are jurisdictional as adjacent wetlands.
☐ Wetlands directly abutting an RPW where tributaries typically flow year-round. Provide data and rationale indicating that tributary is perennial in Section III.D.2, above. Provide rationale indicating that wetland is directly abutting an RPW:
☒ Wetlands directly abutting an RPW where tributaries typically flow "seasonally." Provide data indicating that tributary is seasonal in Section III.B and rationale in Section III.D.2, above. Provide rationale indicating that wetland is directly abutting an RPW:

Provide acreage estimates for jurisdictional wetlands in the review area: acres.

5. **Wetlands adjacent to but not directly abutting an RPW that flow directly or indirectly into TNWs.**

- ☐ Wetlands that do not directly abut an RPW, but when considered in combination with the tributary to which they are adjacent and with similarly situated adjacent wetlands, have a significant nexus with a TNW are jurisdictional. Data supporting this conclusion is provided at Section III.C.

Provide acreage estimates for jurisdictional wetlands in the review area: acres.

6. **Wetlands adjacent to non-RPWs that flow directly or indirectly into TNWs.**

- ☐ Wetlands adjacent to such waters, and have when considered in combination with the tributary to which they are adjacent and with similarly situated adjacent wetlands, have a significant nexus with a TNW are jurisdictional. Data supporting this conclusion is provided at Section III.C.

Provide estimates for jurisdictional wetlands in the review area: acres.

7. **Impoundments of jurisdictional waters.⁹**

As a general rule, the impoundment of a jurisdictional tributary remains jurisdictional.

- ☐ Demonstrate that impoundment was created from "waters of the U.S.," or
☒ Demonstrate that water meets the criteria for one of the categories presented above (1-6), or
☐ Demonstrate that water is isolated with a nexus to commerce (see E below).

E. **ISOLATED [INTERSTATE OR INTRA-STATE] WATERS, INCLUDING ISOLATED WETLANDS, THE USE, DEGRADATION OR DESTRUCTION OF WHICH COULD AFFECT INTERSTATE COMMERCE, INCLUDING ANY SUCH WATERS (CHECK ALL THAT APPLY):¹⁰**

- ☐ which are or could be used by interstate or foreign travelers for recreational or other purposes.
☒ from which fish or shellfish are or could be taken and sold in interstate or foreign commerce.
☒ which are or could be used for industrial purposes by industries in interstate commerce.
☒ Interstate isolated waters. Explain:
☒ Other factors. Explain:

Identify water body and summarize rationale supporting determination:

Provide estimates for jurisdictional waters in the review area (check all that apply):

- ☐ Tributary waters: linear feet width (ft).
☐ Other non-wetland waters: acres.

Identify type(s) of waters:

- ☐ Wetlands: acres.

⁸See Footnote # 3.

⁹To complete the analysis refer to the key in Section III.D.6 of the Instructional Guidebook.

¹⁰Prior to asserting or declining CWA jurisdiction based solely on this category, Corps Districts will elevate the action to Corps and EPA HQ for review consistent with the process described in the Corps/EPA Memorandum Regarding CWA Act Jurisdiction Following Rapanos.

F. NON-JURISDICTIONAL WATERS, INCLUDING WETLANDS (CHECK ALL THAT APPLY):

- ☐ If potential wetlands were assessed within the review area, these areas did not meet the criteria in the 1987 Corps of Engineers Wetland Delineation Manual and/or appropriate Regional Supplements.
- ☒ Review area included isolated waters with no substantial nexus to interstate (or foreign) commerce.
- ☒ Prior to the Jan 2001 Supreme Court decision in "SWANCC," the review area would have been regulated based solely on the "Migratory Bird Rule" (MBR).
- ☒ Waters do not meet the "Significant Nexus" standard, where such a finding is required for jurisdiction. Explain:
- ☒ Other: (explain, if not covered above):

Provide acreage estimates for non-jurisdictional waters in the review area, where the sole potential basis of jurisdiction is the MBR factors (i.e., presence of migratory birds, presence of endangered species, use of water for irrigated agriculture), using best professional judgment (check all that apply):

- ☒ Non-wetland waters (i.e., rivers, streams): linear feet width (ft).
- ☒ Lakes/ponds: acres.
- ☒ Other non-wetland waters: acres. List type of aquatic resource:
- ☒ Wetlands: **Wetland D** **Emergent** **0.01 acre**
- Wetland E** **Emergent** **0.05 acre**

Provide acreage estimates for non-jurisdictional waters in the review area that do not meet the "Significant Nexus" standard, where such a finding is required for jurisdiction (check all that apply):

- ☐ Non-wetland waters (i.e., rivers, streams): linear feet, width (ft).
- ☐ Lakes/ponds: acres.
- ☐ Other non-wetland waters: acres. List type of aquatic resource:
- ☐ Wetlands: acres.

SECTION IV: DATA SOURCES.**A. SUPPORTING DATA. Data reviewed for JD (check all that apply - checked items shall be included in case file and, where checked and requested, appropriately reference sources below):**

- ☒ Maps, plans, plots or plat submitted by or on behalf of the applicant/consultant: **Ron LeCain**
- ☒ Data sheets prepared/submitted by or on behalf of the applicant/consultant.
- ☒ Office concurs with data sheets/delineation report.
- ☐ Office does not concur with data sheets/delineation report.
- ☒ Data sheets prepared by the Corps:
- ☒ Corps navigable waters' study:
- ☒ U.S. Geological Survey Hydrologic Atlas:
- ☐ USGS NHD data.
- ☐ USGS 8 and 12 digit HUC maps.
- ☒ U.S. Geological Survey map(s). Cite scale & quad name: **Scale: 24000; Trumansburg, New York Quad**
- ☒ USDA Natural Resources Conservation Service Soil Survey. Citation: **on-line websoil survey**
- The following soils were identified within the review area Hydric Soil Rating**

RkA Rhinebeck silt loam, 0 to 2 percent slopes 10

- ☒ National wetlands inventory map(s). Cite name: **Trumansburg, New York**
- ☒ State/Local wetland inventory map(s): **Trumansburg, New York**
- ☒ FEMA/FIRM maps:
- ☒ 100-year Floodplain Elevation is: (National Geodetic Vertical Datum of 1929)
- ☒ Photographs: ☒ Aerial (Name & Date): **Google Earth 1994 and 2007; NYS Orthos On-Line 2002 and 2007**
- or ☒ Other (Name & Date): **Submitted with delineation report; photos taken June 5, 2017**
- ☐ Previous determination(s). File no. and date of response letter:
- ☐ Applicable/supporting case law:
- ☐ Applicable/supporting scientific literature:
- ☐ Other information (please specify):

B. ADDITIONAL COMMENTS TO SUPPORT JD:

Applicant: Ithaca Neighborhood Housing Services		File Number: 2017-00927	Date: 01/25/18
Attached is:			See Section below
	INITIAL PROFFERED PERMIT (Standard Permit or Letter of Permission)	A	
	PROFFERED PERMIT (Standard Permit or Letter of Permission)	B	
	PERMIT DENIAL	C	
X	APPROVED JURISDICTIONAL DETERMINATION (for wetlands shown in Area 1)	D	
	PRELIMINARY JURISDICTIONAL DETERMINATION	E	

SECTION I - The following identifies your rights and options regarding an administrative appeal of the above decision. Additional information may be found at <http://www.usace.army.mil/CECW/Pages/reg-materials.aspx> or Corps regulations at 33 CFR Part 3.14.

A: INITIAL PROFFERED PERMIT: You may accept or object to the permit.

- **ACCEPT:** If you received a Standard Permit, you may sign the permit document and return it to the district engineer for final authorization. If you received a Letter of Permission (LOP), you may accept the LOP and your work is authorized. Your signature on the Standard Permit or acceptance of the LOP means that you accept the permit in its entirety, and waive all rights to appeal the permit, including its terms and conditions, and approved jurisdictional determinations associated with the permit.
- **OBJECT:** If you object to the permit (Standard or LOP) because of certain terms and conditions therein, you may request that the permit be modified accordingly. You must complete Section II of this form and return the form to the district engineer. Your objections must be received by the district engineer within 60 days of the date of this notice, or you will forfeit your right to appeal the permit in the future. Upon receipt of your letter, the district engineer will evaluate your objections and may: (a) modify the permit to address all of your concerns, (b) modify the permit to address some of your objections, or (c) not modify the permit having determined that the permit should be issued as previously written. After evaluating your objections, the district engineer will send you a proffered permit for your reconsideration, as indicated in Section B below.

B: PROFFERED PERMIT: You may accept or appeal the permit

- **ACCEPT:** If you received a Standard Permit, you may sign the permit document and return it to the district engineer for final authorization. If you received a Letter of Permission (LOP), you may accept the LOP and your work is authorized. Your signature on the Standard Permit or acceptance of the LOP means that you accept the permit in its entirety, and waive all rights to appeal the permit, including its terms and conditions, and approved jurisdictional determinations associated with the permit.
- **APPEAL:** If you choose to decline the proffered permit (Standard or LOP) because of certain terms and conditions therein, you may appeal the declined permit under the Corps of Engineers Administrative Appeal Process by completing Section II of this form and sending the form to the division engineer. This form must be received by the division engineer within 60 days of the date of this notice.

C: PERMIT DENIAL: You may appeal the denial of a permit under the Corps of Engineers Administrative Appeal Process by completing Section II of this form and sending the form to the division engineer. This form must be received by the division engineer within 60 days of the date of this notice.

D: APPROVED JURISDICTIONAL DETERMINATION: You may accept or appeal the approved JD or provide new information.

- **ACCEPT:** You do not need to notify the Corps to accept an approved JD. Failure to notify the Corps within 60 days of the date of this notice, means that you accept the approved JD in its entirety, and waive all rights to appeal the approved JD.
- **APPEAL:** If you disagree with the approved JD, you may appeal the approved JD under the Corps of Engineers Administrative Appeal Process by completing Section II of this form and sending the form to the division engineer. This form must be received by the division engineer within 60 days of the date of this notice.

E: PRELIMINARY JURISDICTIONAL DETERMINATION: You do not need to respond to the Corps regarding the preliminary JD. The Preliminary JD is not appealable. If you wish, you may request an approved JD (which may be appealed), by contacting the Corps district for further instruction. Also you may provide new information for further consideration by the Corps to reevaluate the JD.

SECTION II - REQUEST FOR APPEAL or OBJECTIONS TO AN INITIAL PROFFERED PERMIT

REASONS FOR APPEAL OR OBJECTIONS: (Describe your reasons for appealing the decision or your objections to an initial proffered permit in clear concise statements. You may attach additional information to this form to clarify where your reasons or objections are addressed in the administrative record.)

ADDITIONAL INFORMATION: The appeal is limited to a review of the administrative record, the Corps memorandum for the record of the appeal conference or meeting, and any supplemental information that the review officer has determined is needed to clarify the administrative record. Neither the appellant nor the Corps may add new information or analyses to the record. However, you may provide additional information to clarify the location of information that is already in the administrative record.

POINT OF CONTACT FOR QUESTIONS OR INFORMATION:

If you have questions regarding this decision and/or the appeal process you may contact:

Judy A. Robinson
U.S. Army Corps of Engineers
New York Regulatory Branch
Auburn Field Office
7413 County House Road
Auburn, New York 13021
716-879-6330
Judy.a.robinson@usace.army.mil

If you only have questions regarding the appeal process you may also contact:

Review Officer
Great Lakes and Ohio River Division
CELRD-PDS-O
550 Main Street, Room 10524
Cincinnati, OH 45202-3222
Phone: 513-684-6212 Fax: 513-684-2460

RIGHT OF ENTRY: Your signature below grants the right of entry to Corps of Engineers personnel, and any government consultants, to conduct investigations of the project site during the course of the appeal process. You will be provided a 15 day notice of any site investigation, and will have the opportunity to participate in all site investigations.

<hr/> Signature of Appellant or Agent	Date	Telephone Number
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Appendix 2 - PRELIMINARY JURISDICTIONAL DETERMINATION (PJD) FORM

BACKGROUND INFORMATION

A. REPORT COMPLETION DATE FOR PJD: January 25, 2018

B. NAME AND ADDRESS OF PERSON REQUESTING PJD:

Ithaca Neighborhood Housing Services
115 West Clinton Street
Ithaca, New York 14850
Attn: Joseph Bowes

C. DISTRICT OFFICE, FILE NAME, AND NUMBER: Buffalo District, Auburn Field Office, Ithaca
Neighborhood Housing Services (South Street); File No. 2017-00927

D. PROJECT LOCATION(S) AND BACKGROUND INFORMATION:

Property adjacent to the South Street Extension

State: New York

County: Tompkins

Village: Trumansburg

Center coordinates of site (lat/long in degree decimal format):

Lat: 42.53553°N **Long:** -76.66151°W

Name of nearest waterbody: unnamed tributary to Trumansburg Creek

E. REVIEW PERFORMED FOR SITE EVALUATION (CHECK ALL THAT APPLY):

☒ Office (Desk) Determination. Date: January 10, 2018

☐ Field Determination. Date(s):

**TABLE OF AQUATIC RESOURCES IN REVIEW AREA WHICH "MAY BE" SUBJECT TO
REGULATORY JURISDICTION**

Site number	Latitude (decimal degrees)	Longitude (decimal degrees)	Estimated amount of aquatic resource in review area (acreage and linear feet, if applicable)	Type of aquatic resource (i.e., wetland vs. non- wetland waters)	Geographic authority to which the aquatic resource "may be" subject (i.e., Section 404 or Section 10/404)
Wetland A	42.53611	-76.6626	0.88 ac	Scrub-Shrub (PSS)	404
Wetland B	42.53611	-76.6626	0.05 ac	Scrub-Shrub (PSS)	404
Wetland C	42.53678	-76.65905	0.11 ac	Scrub-Shrub (PSS)	404
Wetland F	42.53495	-76.66026	0.24 ac	Scrub-Shrub (PSS)	404

1) The Corps of Engineers believes that there may be jurisdictional aquatic resources in the review area, and the requestor of this PJD is hereby advised of his or her option to request and obtain an approved JD (AJD) for that review area based on an informed decision after having discussed the various types of JDs and their characteristics and circumstances when they may be appropriate.

2) In any circumstance where a permit applicant obtains an individual permit, or a Nationwide General Permit (NWP) or other general permit verification requiring "pre-construction notification" (PCN), or requests verification for a non-reporting NWP or other general permit, and the permit applicant has not requested an AJD for the activity, the permit applicant is hereby made aware that:

(1) the permit applicant has elected to seek a permit authorization based on a PJD, which does not make an official determination of jurisdictional aquatic resources;

(2) the applicant has the option to request an AJD before accepting the terms and conditions of the permit authorization, and that basing a permit authorization on an AJD could possibly result in less compensatory mitigation being required or different special conditions;

(3) the applicant has the right to request an individual permit rather than accepting the terms and conditions of the NWP or other general permit authorization;

(4) the applicant can accept a permit authorization and thereby agree to comply with all the terms and conditions of that permit, including whatever mitigation requirements the Corps has determined to be necessary;

(5) undertaking any activity in reliance upon the subject permit authorization without requesting an AJD constitutes the applicant's acceptance of the use of the PJD;

(6) accepting a permit authorization (e.g., signing a proffered individual permit) or undertaking any activity in reliance on any form of Corps permit authorization based on a PJD constitutes agreement that all aquatic resources in the review area affected in any way by that activity will be treated as jurisdictional, and waives any challenge to such jurisdiction in any administrative or judicial compliance or enforcement action, or in any administrative appeal or in any Federal court; and

(7) whether the applicant elects to use either an AJD or a PJD, the JD will be processed as soon as practicable. Further, an AJD, a proffered individual permit (and all terms and conditions contained therein), or individual permit denial can be administratively appealed pursuant to 33 C.F.R. Part 331.

If, during an administrative appeal, it becomes appropriate to make an official determination whether geographic jurisdiction exists over aquatic resources in the review area, or to provide an official delineation of jurisdictional aquatic resources in the review area, the Corps will provide an AJD to accomplish that result, as soon as is practicable.

This PJD finds that there "may be" waters of the U.S. and/or that there "may be" navigable waters of the U.S. on the subject review area, and identifies all aquatic features in the review area that could be affected by the proposed activity, based on the following information:

SUPPORTING DATA. Data reviewed for PJD (check all that apply)

Checked items should be included in subject file. Appropriately reference sources below where indicated for all checked items:

- ☒ Maps, plans, plots or plat submitted by or on behalf of the PJD requestor:
LeCain Environmental Services

Map: NWI, NYSDEC FWW, Soil

- ☒ Data sheets prepared/submitted by or on behalf of the PJD requestor.
☒ Office concurs with revised data sheets/delineation report.
☐ Office does not concur with data sheets/delineation report. Rationale:
☐ Data sheets prepared by the Corps:
☐ Corps navigable waters' study: _
☐ U.S. Geological Survey Hydrologic Atlas:
☐ USGS NHD data.
☐ USGS 8 and 12 digit HUC maps.
☒ U.S. Geological Survey map(s). Cite scale & quad name: 24000k; Trumansburg, NY
☒ Natural Resources Conservation Service Soil Survey. Citation: **Web Soil Survey**

The following soils were identified on the parcel

Hydric Rating

HdC	Howard gravelly loam, 5 to 15 percent simple slopes	0
LbB	Iansing gravelly silt loam, 3 to 8 percent slopes	0
OaA	oid silt loam, 0 to 8 percent slopes	10
RkA	Rhinebeck silt loam, 0 to 2 percent slopes	10

- ☒ National wetlands inventory map: Cite name: Trumansburg, NY
☒ State/local wetland inventory map: Trumansburg, NY
☐ FEMA/FIRM maps:
☐ 100-year Floodplain Elevation is: _____. (National Geodetic Vertical Datum of 1929)
☒ Photographs:
☒ Aerial (Name & Date): **Google Earth 1994 and 2007; NYS Orthos On-Line 2002 and 2007**
☒ Other (Name & Date): **Submitted with delineation report; photos taken June 5, 2017**
☐ Previous determination(s). File no. and date of response letter:
☐ Other information (please specify):

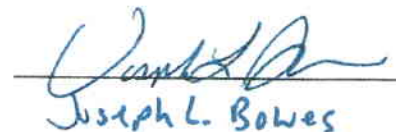
IMPORTANT NOTE: The information recorded on this form has not necessarily been verified by the Corps and should not be relied upon for later jurisdictional determinations.

ROBINSONJUD

Y A 1284100103
Judy Robinson

Digitally signed by
ROBINSONJUDY.A.1284100103
DN: c=US, o=U.S. Government, ou=DoD,
ou=PKI, ou=USA,
cn=ROBINSONJUDY.A.1284100103
Date: 2018.01.25 12:39:32 -05'00'

Signature and date of Regulatory
Project Manager


Joseph L. Bowes

Signature and date of person requesting PJD
(REQUIRED, unless obtaining the signature
is impracticable)¹

¹ Districts may establish timeframes for requestor to return signed PJD forms. If the requestor does not respond within the established time frame, the district may presume concurrence and no additional follow up is necessary prior to finalizing an action.

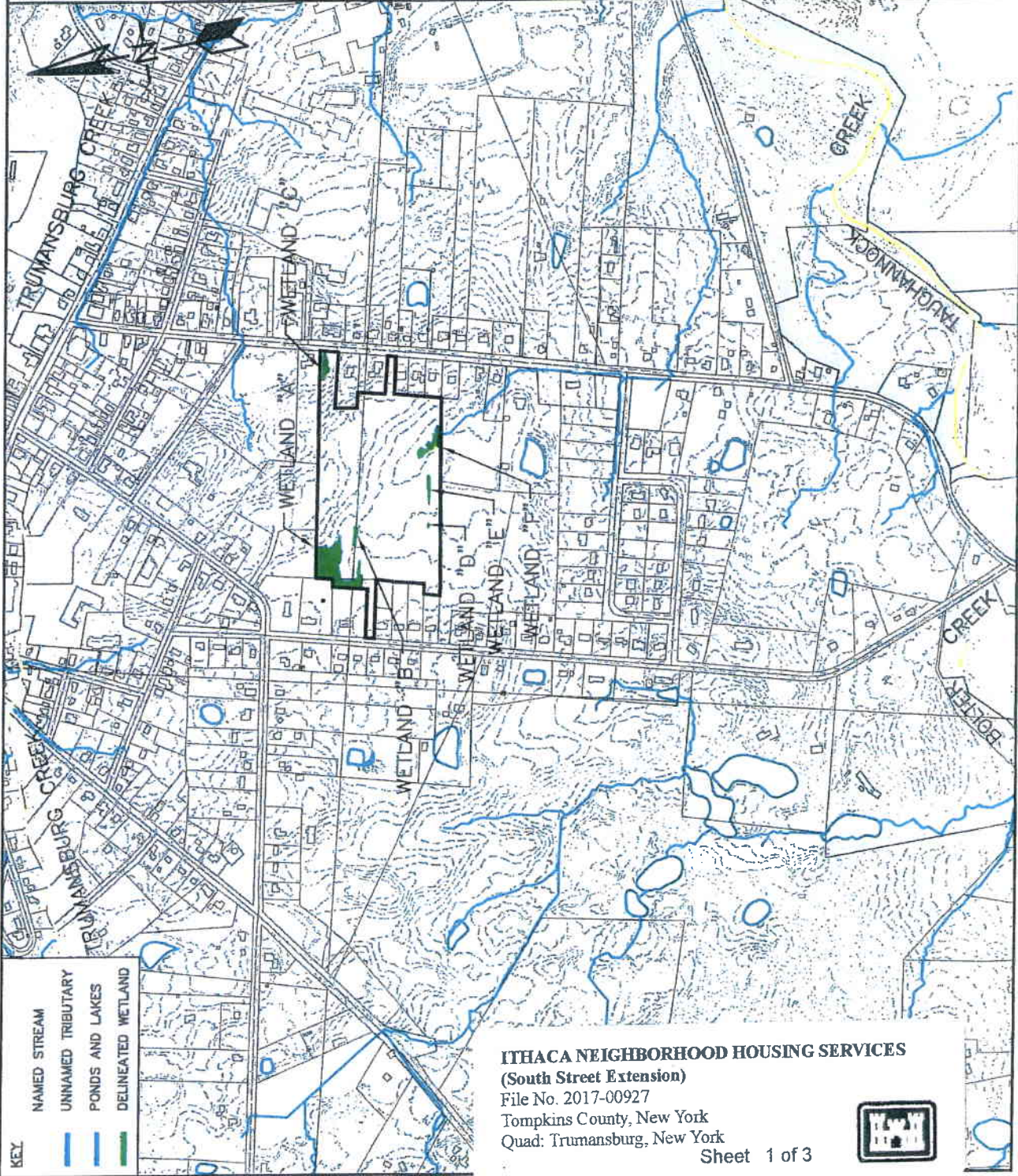


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607-272-6477

ITHACA NEIGHBORHOOD HOUSING SERVICES
46 SOUTH STREET DEVELOPMENT
VILLAGE OF TRUMANSBURG, TOMPKINS COUNTY, NEW YORK

SHEET TITLE
CONVEYANCE
MAP

DATE:	10/26/17	JOB No.	E17-19
SCALE:	1"=800'		
DRAWN BY:	TRT	SHEET	C2
CHECKED:	AJS		



- KEY**
- NAMED STREAM
 - UNNAMED TRIBUTARY
 - PONDS AND LAKES
 - DELINEATED WETLAND

ITHACA NEIGHBORHOOD HOUSING SERVICES
(South Street Extension)
File No. 2017-00927
Tompkins County, New York
Quad: Trumansburg, New York
Sheet 1 of 3





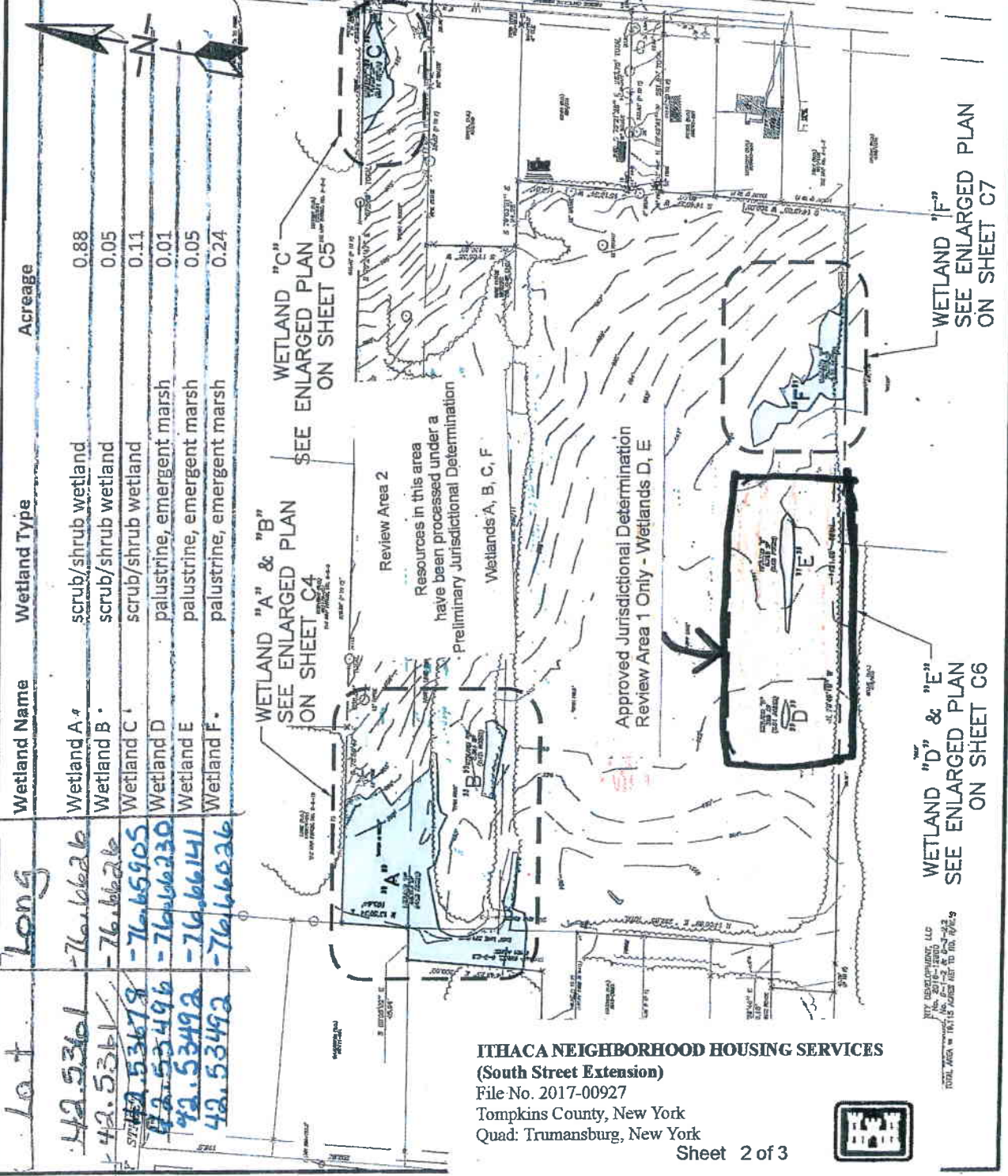
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ITHACA NEIGHBORHOOD HOUSING SERVICES
46 SOUTH STREET DEVELOPMENT
VILLAGE OF TRUMANSBURG, TOMPKINS COUNTY, NEW YORK

SHEET TITLE

**WETLAND
KEY
MAP**

DATE:	10/26/17	JOB No.	E17-19
SCALE:	1"=200'	DRAWN BY:	TRT
CHECKED:	AJS	SHEET	C3



Wetland Name	Wetland Type	Acreage
Wetland A	scrub/shrub wetland	0.88
Wetland B	scrub/shrub wetland	0.05
Wetland C	scrub/shrub wetland	0.11
Wetland D	palustrine, emergent marsh	0.01
Wetland E	palustrine, emergent marsh	0.05
Wetland F	palustrine, emergent marsh	0.24

Lot	Long
42.5361	-76.6626
42.5361	-76.6626
42.5361	-76.6595
42.5349	-76.6623
42.5349	-76.6614
42.5349	-76.6626

ITHACA NEIGHBORHOOD HOUSING SERVICES
(South Street Extension)
File No. 2017-00927
Tompkins County, New York
Quad: Trumansburg, New York



NY DEVELOPMENT, LLC
No. 2016-1880-2-2
TOTAL AREA: 1.115 ACRES (NET TO THE CITY)



ITHACA NEIGHBORHOOD HOUSING SERVICES
46 SOUTH STREET DEVELOPMENT
VILLAGE OF TRUMANSBURG, TOMPKINS COUNTY, NEW YORK

SHEET TITLE

WETLAND
"D" & "E"
MAP

REVISÉ 1/9/18

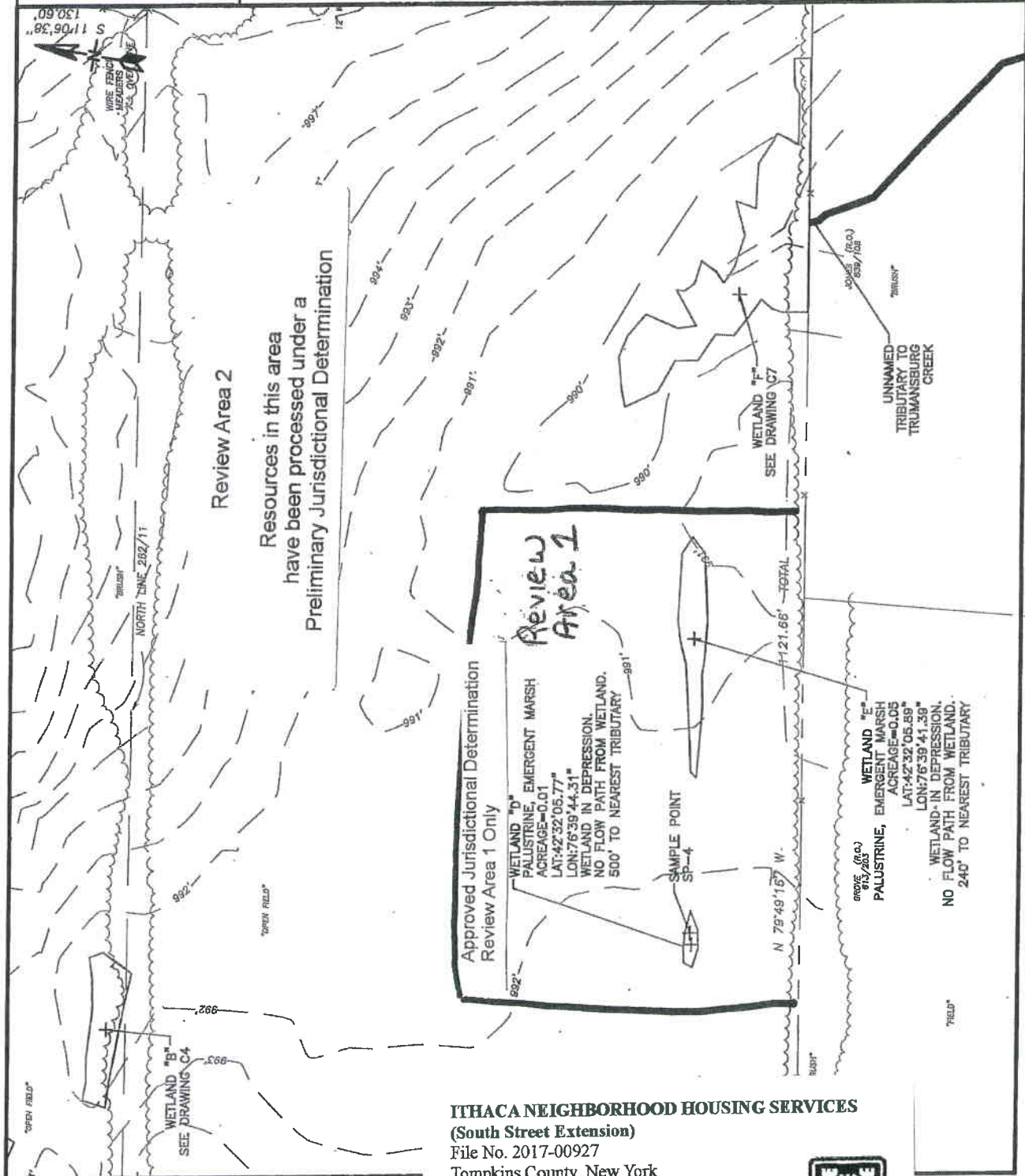
DATE: 10/26/17	JOB No.
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SCALE:

DRAWN BY: **TRT**

SHEET

66



ITHACA NEIGHBORHOOD HOUSING SERVICES
(South Street Extension)
 File No. 2017-00927
 Tompkins County, New York
 Quad: Trumansburg, New York



Exhibit D



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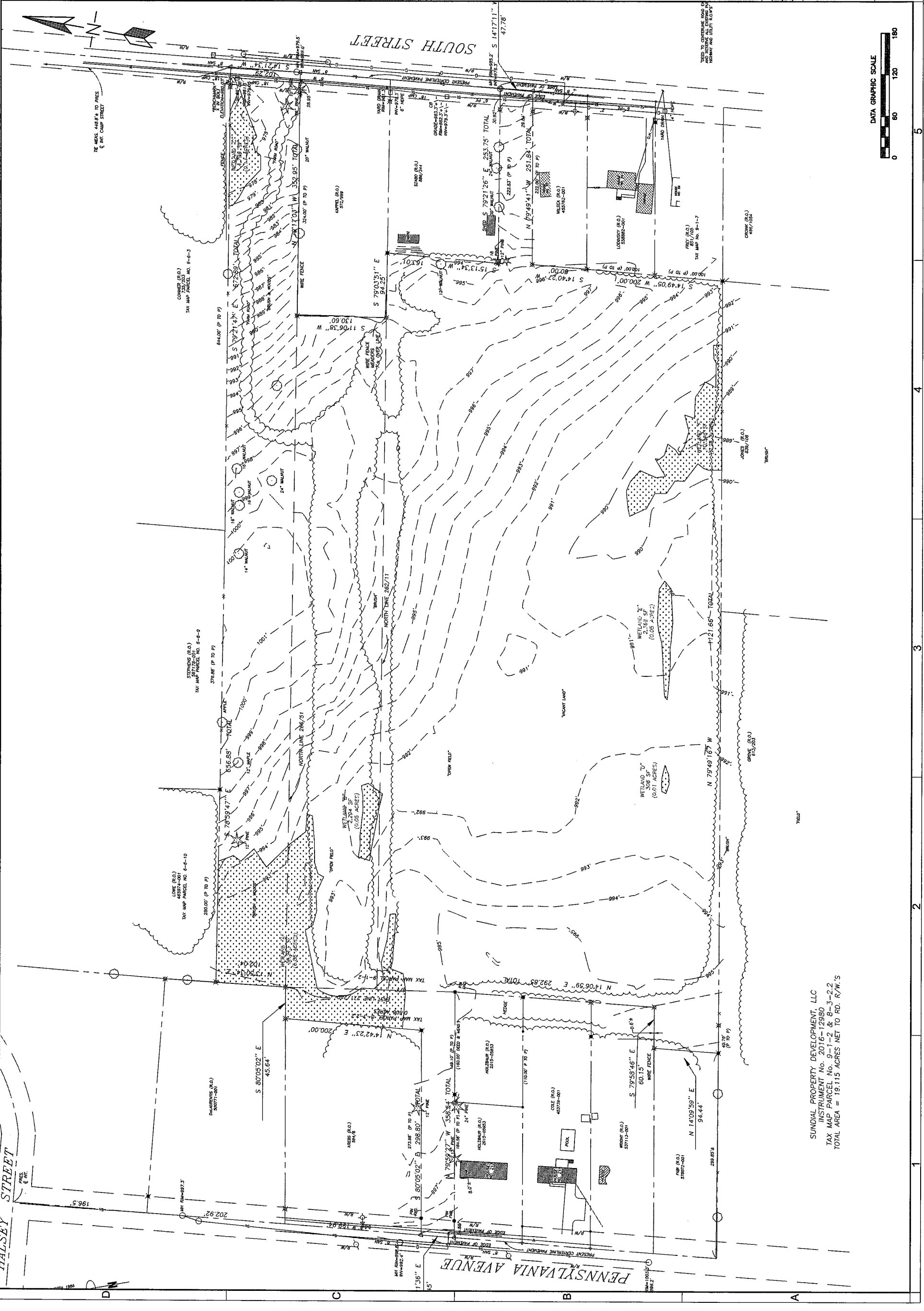
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**Ithaca Neighborhood Housing Services &
Sundial Property Development LLC
46 South Street
Trumansburg, New York**

DATE:	12/13/2017
PROJECT:	17003
DRAWN BY:	SRR/JRT
CHECKED:	AJS

EXISTING CONDITIONS PLAN

C101



SEQUENCING

- ## GENERAL NOTES

- CONSERVATION SEED MIX**

SPRING SEEDINGS		LATE SPRING & SUMMER SEEDINGS		LATE SUMMER & FALL SEEDINGS	
a) ANNUAL INTERPAGES:	0.70 LBS/1000 S.F.	a) SLOWGROWS:	0.90 LBS/1000 S.F.	a) ANNUAL INTERPAGES (COMMON)	0.70 LBS/1000 S.F.
b) SPRING ONTS:	2.00 LBS/1000 S.F.	b) ANNUAL INTERPAGES:	0.70 LBS/1000 S.F.	b) WINTER WTE (ARCTOSTYMA)	2.50 LBS/1000 S.F.
c) ANNUAL INTERPAGES:	0.35 LBS/1000 S.F.	c) PERSONAL INTERPAGES:	0.70 LBS/1000 S.F.	c) PERSONAL INTERPAGES (IMMUNOPH)	0.70 LBS/1000 S.F.
d) PERSONAL INTERPAGES:	0.70 LBS/1000 S.F.			d) PERSONAL INTERPAGES (IMMUNOPH)	0.70 LBS/1000 S.F.

100 LBS (2-3 BALES)/1000 S.F.

MULCH SHALL BE APPLIED OVER TEMPORARY OR PERMANENT SEEDING AND SHALL BE ANCHORED USING ONE OF THE FOLLOWING OPTIONS:

- ANCHOR MULCH TO THE SUBGRADE USING 1/2" GALVANIZED STEEL TIE RODS OR EQUIVALENT OVER MULCH.
- USE TRANSVERSE PALLETS TO THE CONTAINER.
- USE A MULCH ANCHORING TIE OR SQUARE SHANK TO CUT MULCH IN SO THAT MULCH IS TIED TO THE SOIL BY 2" OR MORE.
- APPLY A THICKER OVER MULCH CONSISTENT WITH MANUFACTURER'S SPECIFICATIONS.
- APPLY PAPER OVER MULCH OVER STORM MULCH AT A RATE OF 100 LBS PER 1000 S.F.
- SECURE MULCH IN PLACE WITH BODENSHAW METAL OR WITH PEG AND TIE SECURED BY CROSS-STRIPS SPACED AT 3' INTERVALS, AND TIEING DOWN IN A CROSS-CROSS PATTERN.

CLEAN STORM MULCH

100 LBS (2-3 BALES)/1000 S.F.

MULCH SHALL BE APPLIED OVER TEMPORARY OR PERMANENT SEEDING AND SHALL BE ANCHORED USING ONE OF THE FOLLOWING OPTIONS:

- ANCHOR MULCH TO THE SUBGRADE USING 1/2" GALVANIZED STEEL TIE RODS OR EQUIVALENT OVER MULCH.
- USE TRANSVERSE PALLETS TO THE CONTAINER.
- USE A MULCH ANCHORING TIE OR SQUARE SHANK TO CUT MULCH IN SO THAT MULCH IS TIED TO THE SOIL BY 2" OR MORE.
- APPLY A THICKER OVER MULCH CONSISTENT WITH MANUFACTURER'S SPECIFICATIONS.
- APPLY PAPER OVER MULCH OVER STORM MULCH AT A RATE OF 100 LBS PER 1000 S.F.
- SECURE MULCH IN PLACE WITH BODENSHAW METAL OR WITH PEG AND TIE SECURED BY CROSS-STRIPS SPACED AT 3' INTERVALS, AND TIEING DOWN IN A CROSS-CROSS PATTERN.

CLEAN STORM MULCH

NOT TO SCALE

NOT TO SCALE



EROSION AND SEDIMENT CONTROL PLAN

SCALE: 1"=60'

15

5

4

2

C102

46 South Street
Sundial Property Development LLC
Triton Neighborhood Housing Services &
Trumbull, New York

DATE:	12/13/2017
PROJECT:	17003
DRAWN BY:	SRR/TRT
CHECKED:	AJS

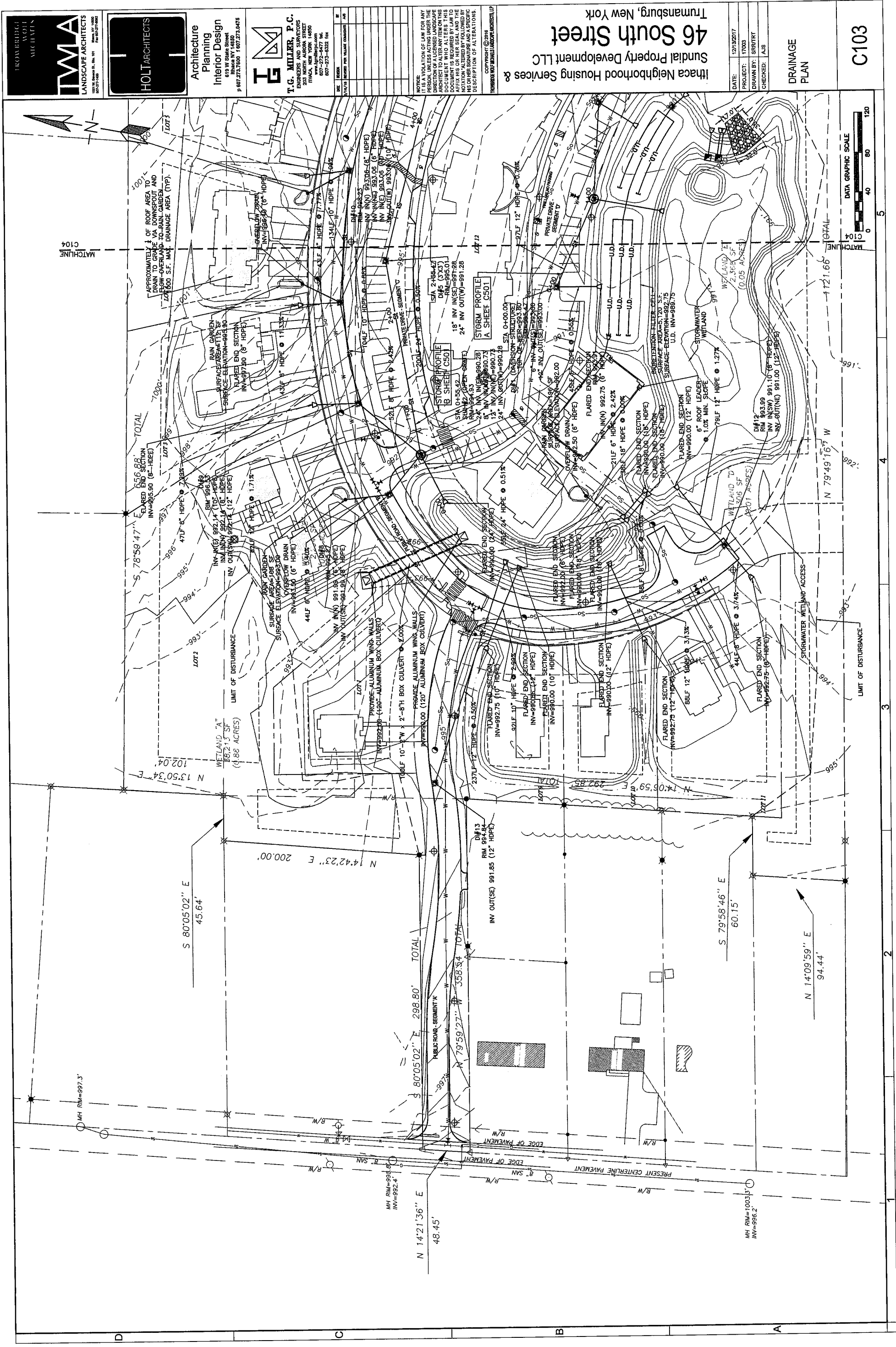
**EROSION AND
SEDIMENT
CONTROL PLAN**

**Architecture
Planning
Interior Design**
619 W State Street
Ithaca NY 14850
507 272 2000 / 507 272 0472



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607-272-8325 fax

ITHACA NEIGHBORHOOD HOUSING SERVICES & SUNDIAL PROPERTY DEVELOPMENT LLC

46 South Street
Trumansburg, New York

DATE: 12/15/2017

PROJECT: 17003

DRAWN BY: SRS/RTK

CHECKED: JUS

DRAINAGE PLAN

C103

NOTES

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CONTRACT NO. 2016

PREPARED BY: HOLT ARCHITECTS, LLP

DATA GRAPHIC SCALE

0 40 80 120

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NEW YORK, NY 10011
TEL: 212-677-1000 FAX: 212-677-1002

HOLTARCHITECTS

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607-272-8322 FAX

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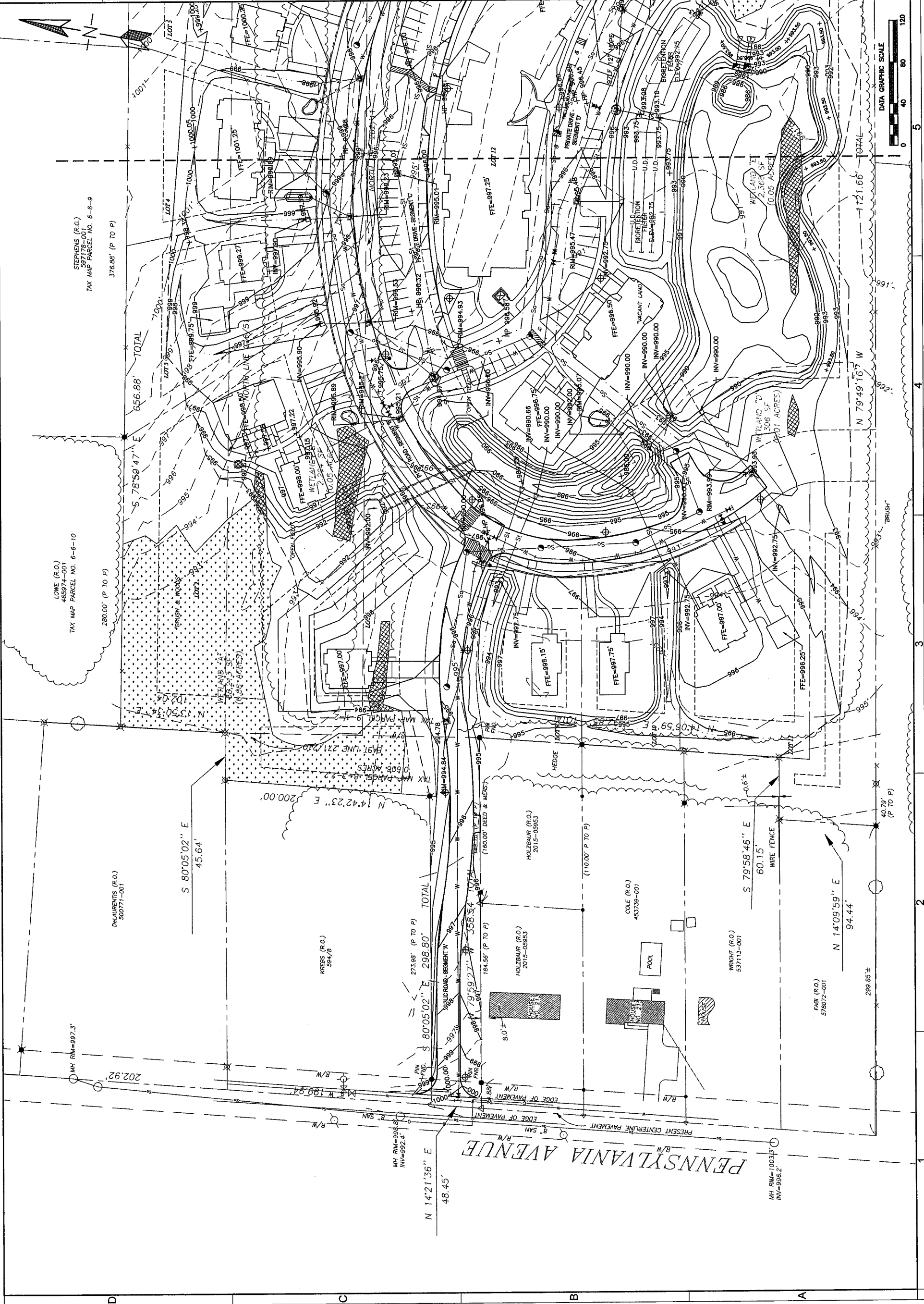
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Ithaca Neighborhood Housing Services &
Trumansburg, New York

DATE:	12/13/2017
PROJECT:	17003
DRAWN BY:	SRR/TRT
CHECKED:	AJS

GRADING PLAN

C105



THOMAS
WOLFE
MICHELSON

TWMA

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3	ISSUED FOR PERMITS	04/10/17
4	ISSUED FOR PERMITS	04/10/17
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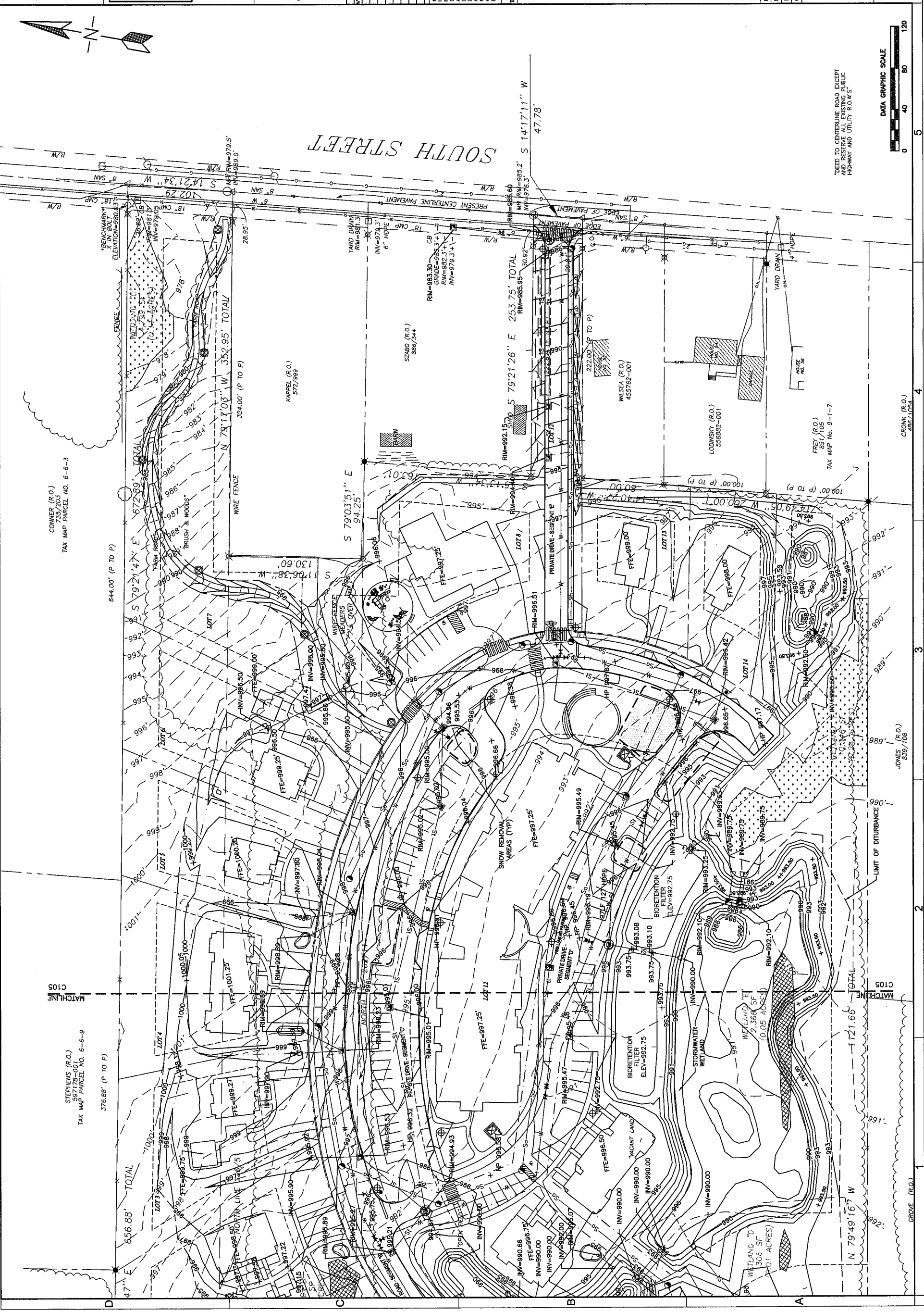
Ithaca Neighborhood Housing Services & Sundial Property Development LLC

46 South Street
Trumansburg, New York

DATE:	12/13/2017
PROJECT:	17003
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GRADING
PLAN

C106





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4/18	REVISED PER VILLAGE COMMENTS	AR

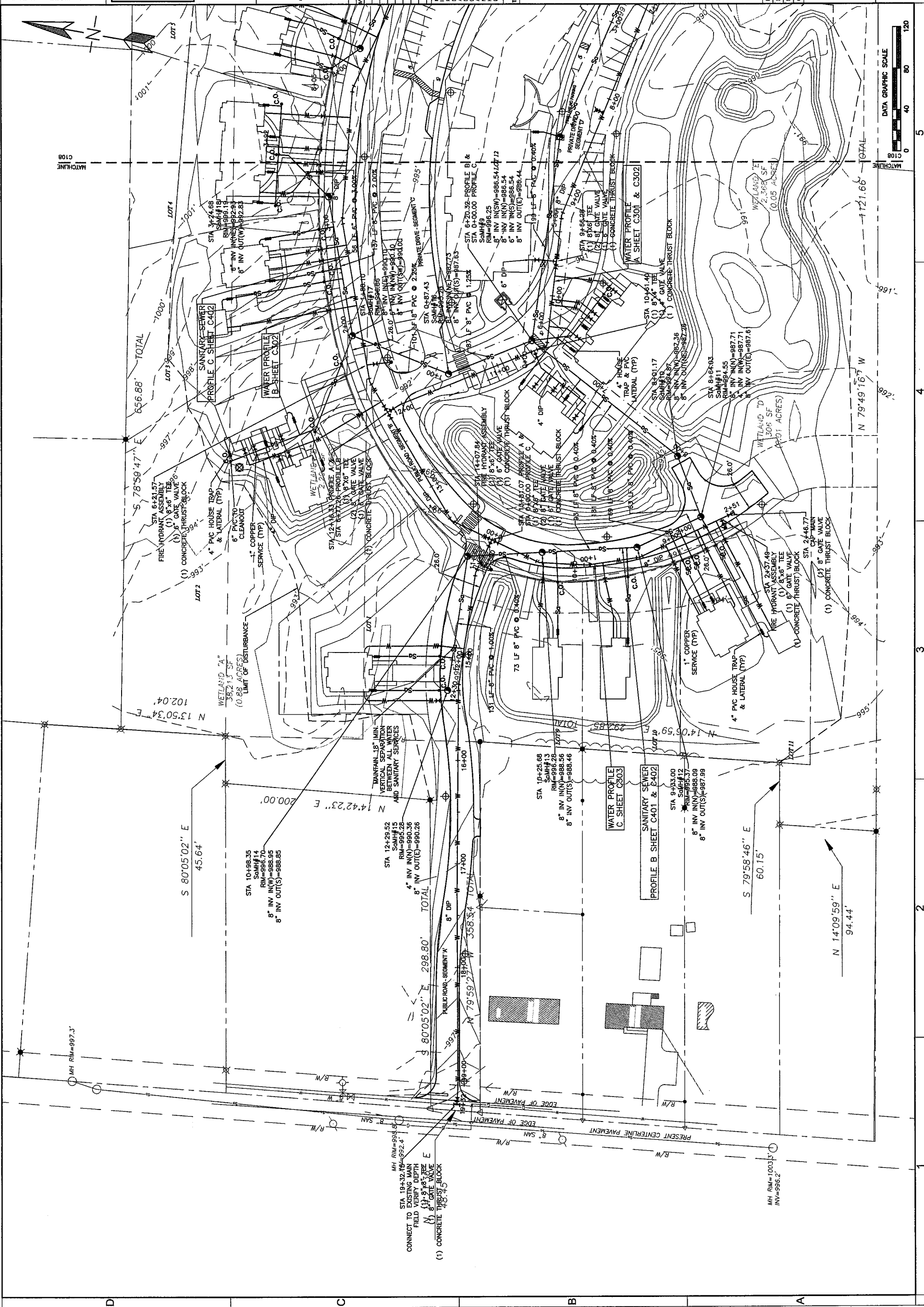
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UTILITY
PLAN

C107



FROM BRIDGE

WOOL

MICHIGAN

TWMA

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DATE: 12/13/2017
PROJECT: 17003
DRAWN BY: SRR/RTT
CHECKED: AJS

UTILITY PLAN

C108

ITHACA NEIGHBORHOOD HOUSING SERVICES & SUNDAI PROPERTY DEVELOPMENT LLC

46 South Street

Trumansburg, New York

DATE: 12/13/2017

PROJECT: 17003

DRAWN BY: SRR/RTT

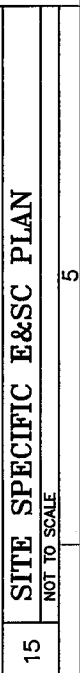
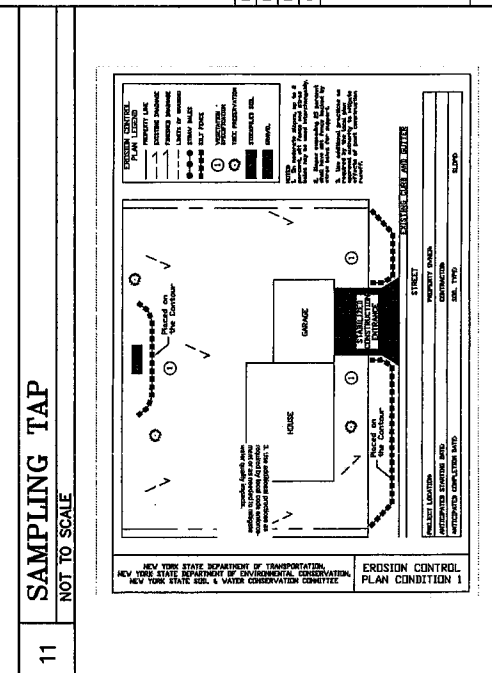
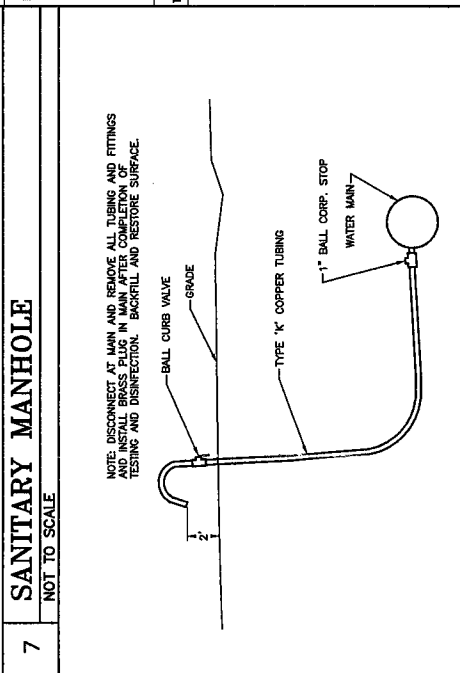
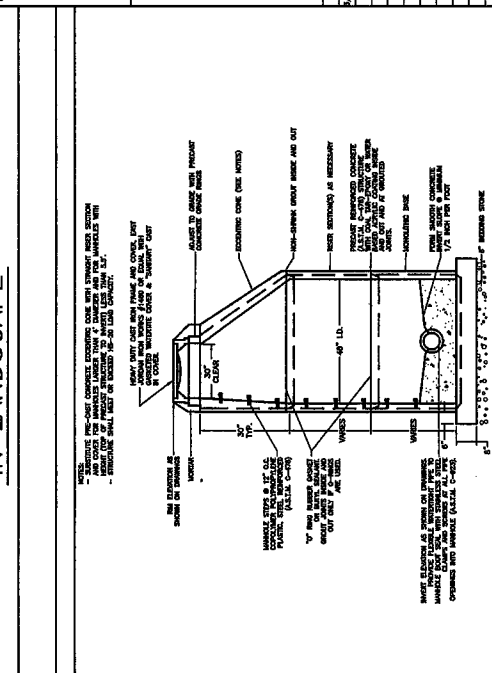
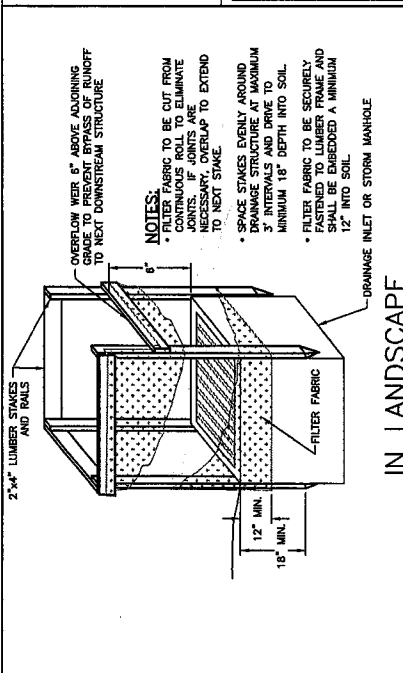
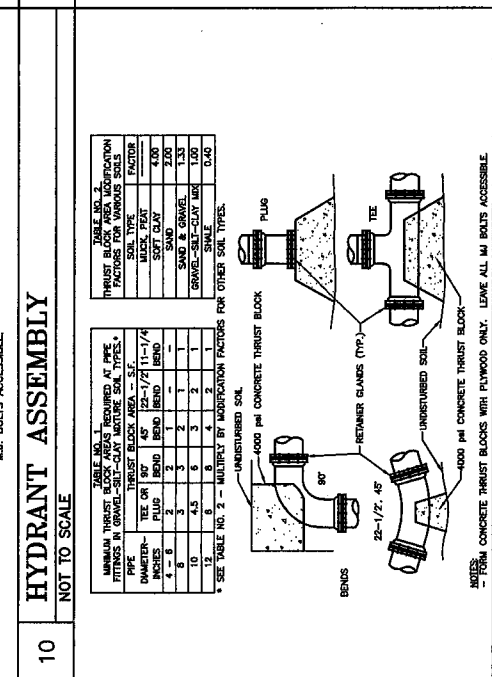
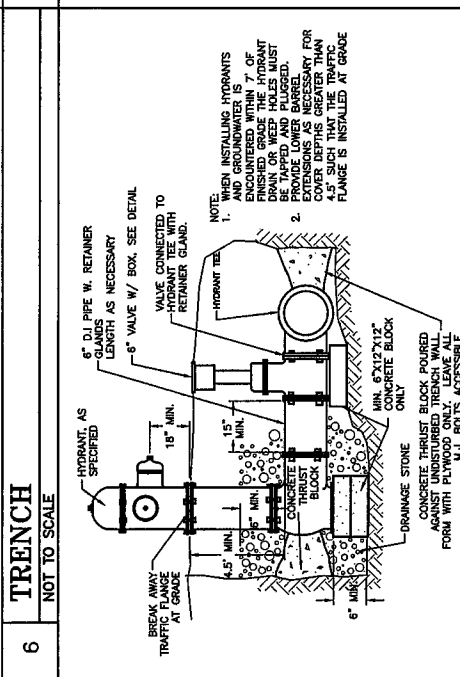
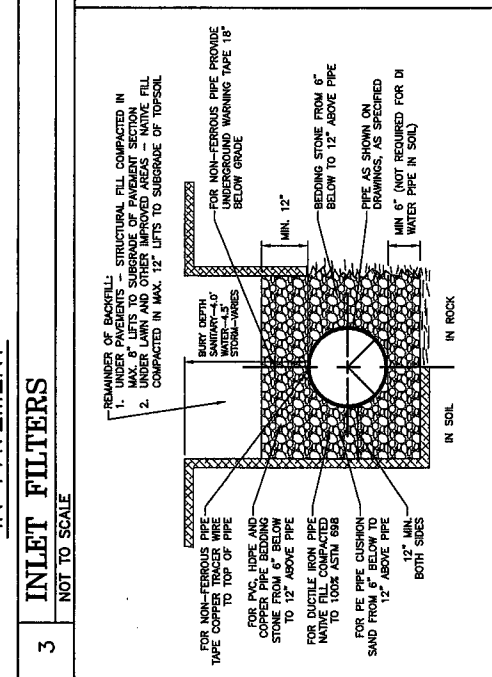
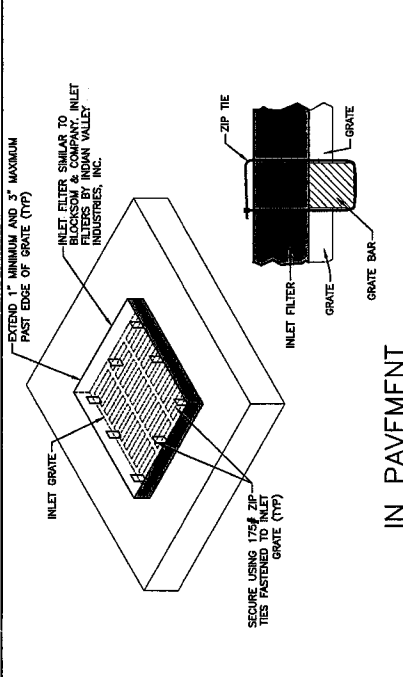
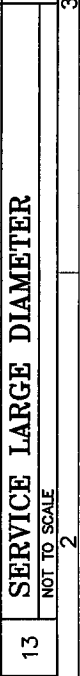
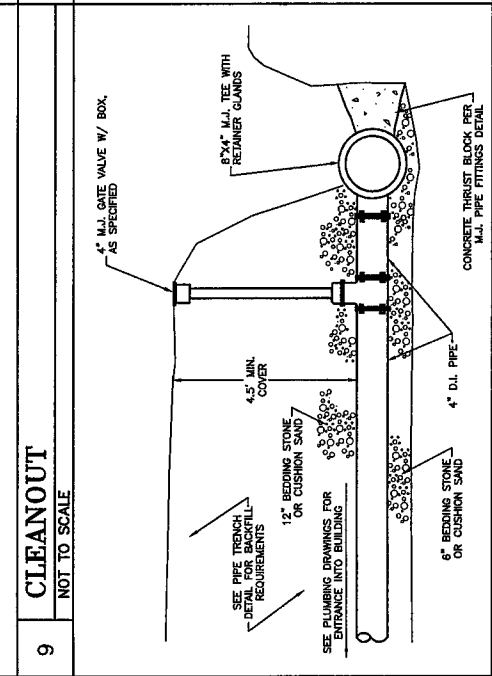
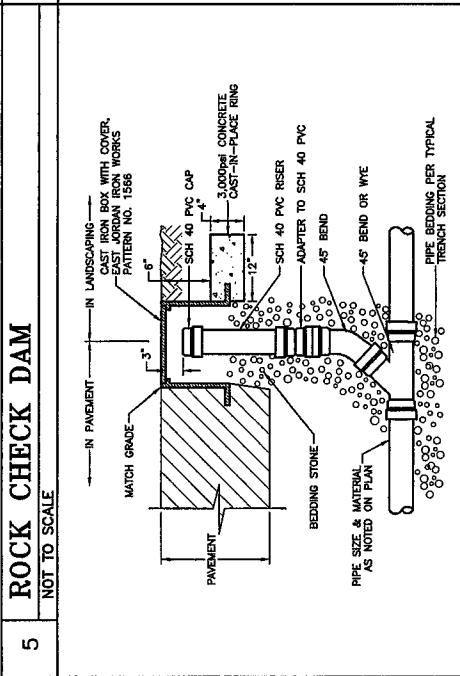
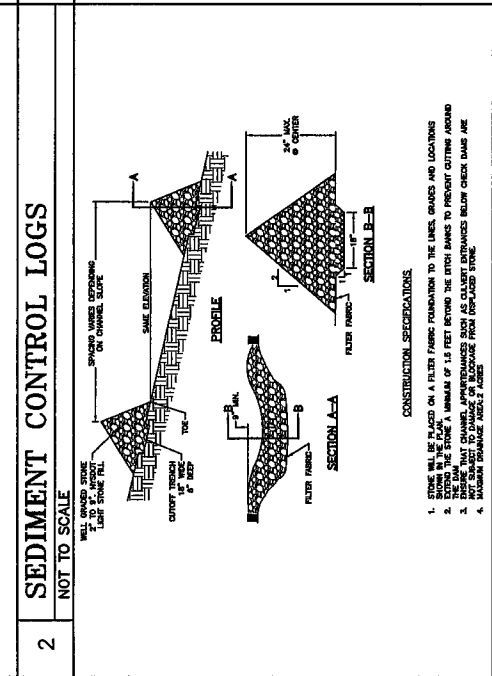
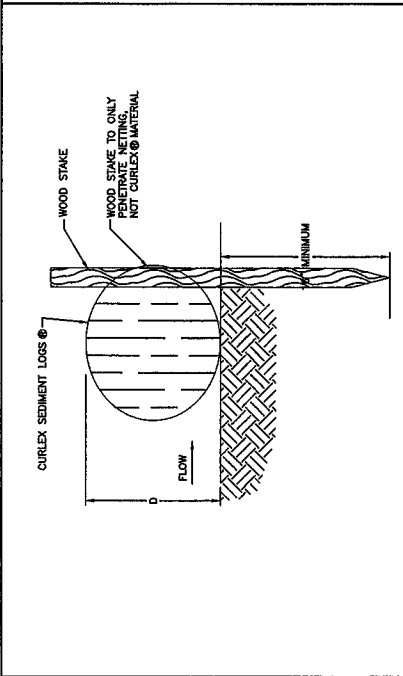
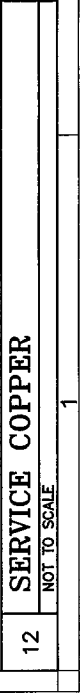
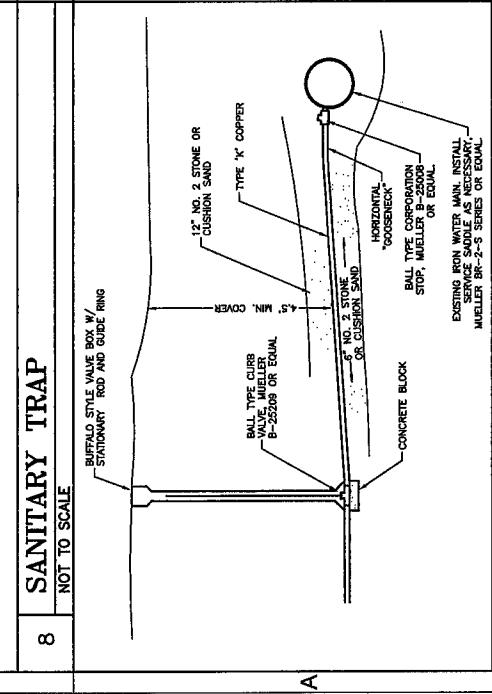
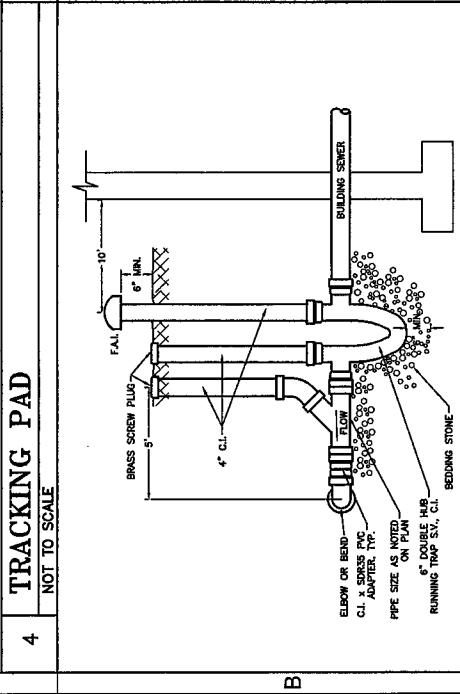
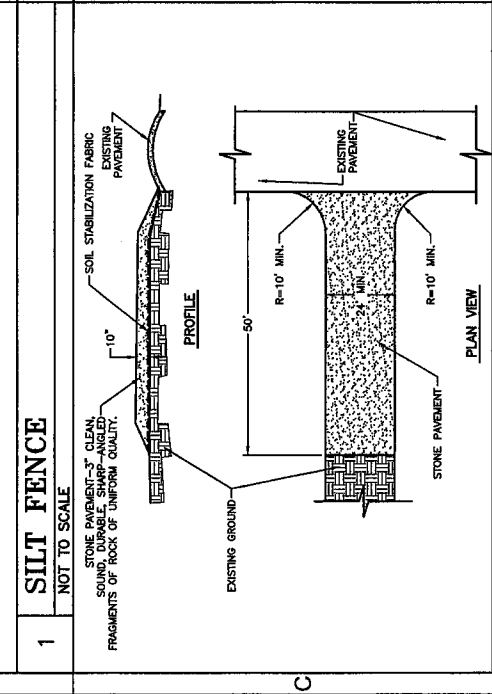
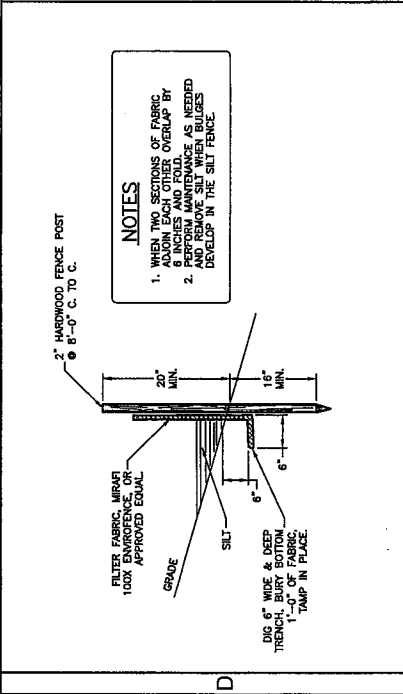
CHECKED: AJS

UTILITY PLAN

C108

This utility plan, titled "UTILITY PLAN" and labeled "C108", details the sewer and water infrastructure for a property at 46 South Street, Trumansburg, New York. The plan is oriented with North at the top, indicated by a north arrow. It shows a network of sewer lines (8" and 6" PVC) and water lines (8" and 6" PVC) with various manholes, valves, and thrust blocks. Key features include:

- Sanitary Sewer Profiles:** Profile A (Sheet C301 & C302) and Profile B (Sheet C401 & C402) are shown with stationing and elevations.
- Water Profile:** Profile C (Sheet C301 & C302) is also detailed.
- Manholes and Valves:** Numerous manholes (e.g., MH#4, MH#5, MH#6, MH#7, MH#8, MH#9, MH#10, MH#11, MH#12, MH#13, MH#14, MH#15, MH#16, MH#17, MH#18, MH#19, MH#20, MH#21, MH#22, MH#23, MH#24, MH#25, MH#26, MH#27, MH#28, MH#29, MH#30, MH#31, MH#32, MH#33, MH#34, MH#35, MH#36, MH#37, MH#38, MH#39, MH#40, MH#41, MH#42, MH#43, MH#44, MH#45, MH#46, MH#47, MH#48, MH#49, MH#50, MH#51, MH#52, MH#53, MH#54, MH#55, MH#56, MH#57, MH#58, MH#59, MH#60, MH#61, MH#62, MH#63, MH#64, MH#65, MH#66, MH#67, MH#68, MH#69, MH#70, MH#71, MH#72, MH#73, MH#74, MH#75, MH#76, MH#77, MH#78, MH#79, MH#80, MH#81, MH#82, MH#83, MH#84, MH#85, MH#86, MH#87, MH#88, MH#89, MH#90, MH#91, MH#92, MH#93, MH#94, MH#95, MH#96, MH#97, MH#98, MH#99, MH#100, MH#101, MH#102, MH#103, MH#104, MH#105, MH#106, MH#107, MH#108, MH#109, MH#110, MH#111, MH#112, MH#113, MH#114, MH#115, MH#116, MH#117, MH#118, MH#119, MH#120, MH#121, MH#122, MH#123, MH#124, MH#125, MH#126, MH#127, MH#128, MH#129, MH#130, MH#131, MH#132, MH#133, MH#134, 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Itasca Neighborhood Housing Services & Sundial Property Development LLC

46 South Street
Trumansburg, New York

DATE: 12/13/2017
PROJECT: 1703
DRAWN BY: BRRT/RT
CHECKED: AJS

DETAILS

C201

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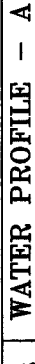
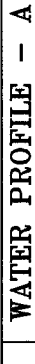
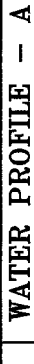
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Ithaca Neighborhood Housing Services &
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PROJECT:	17003
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CHECKED:	AJS

WATER PROFILES

C301





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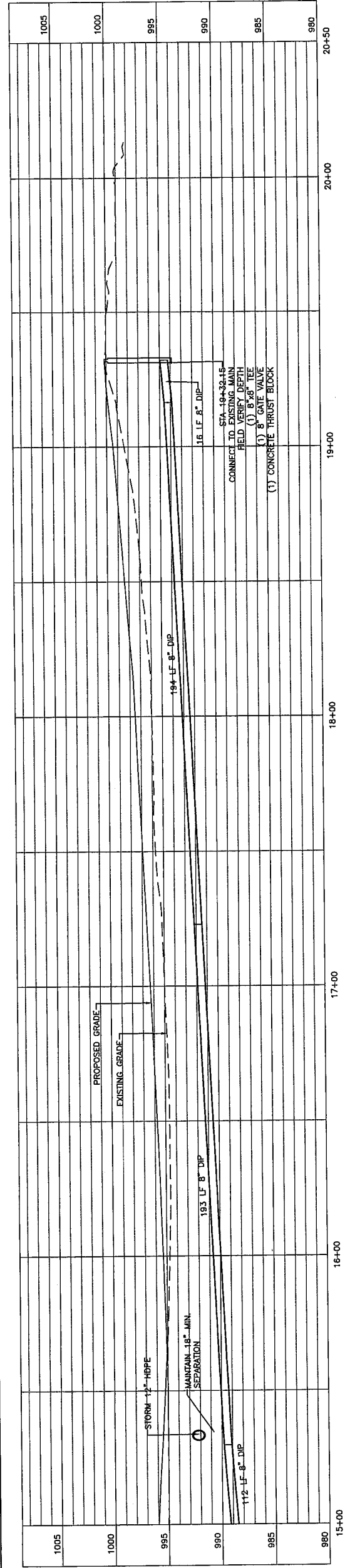
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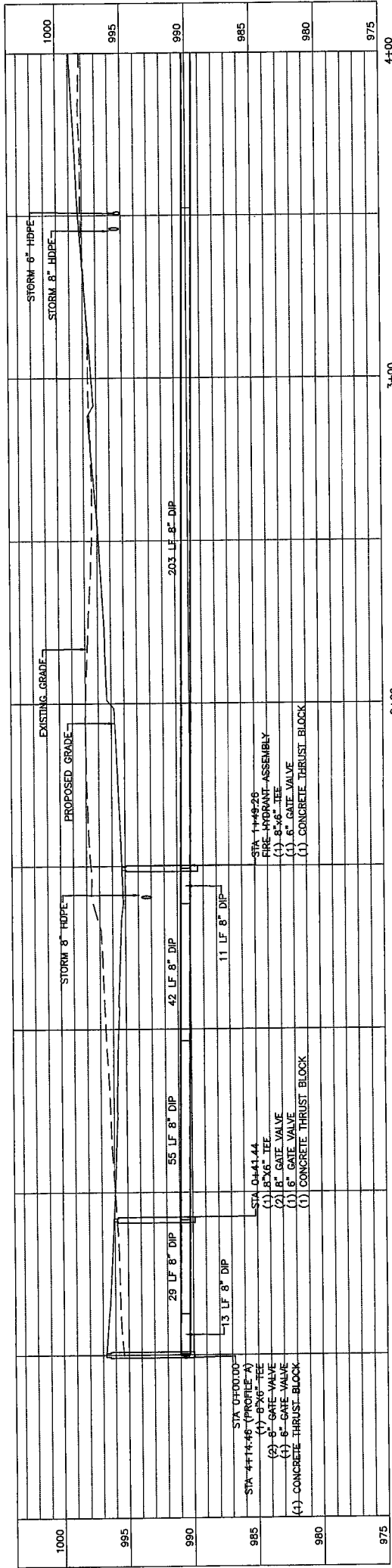
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C302



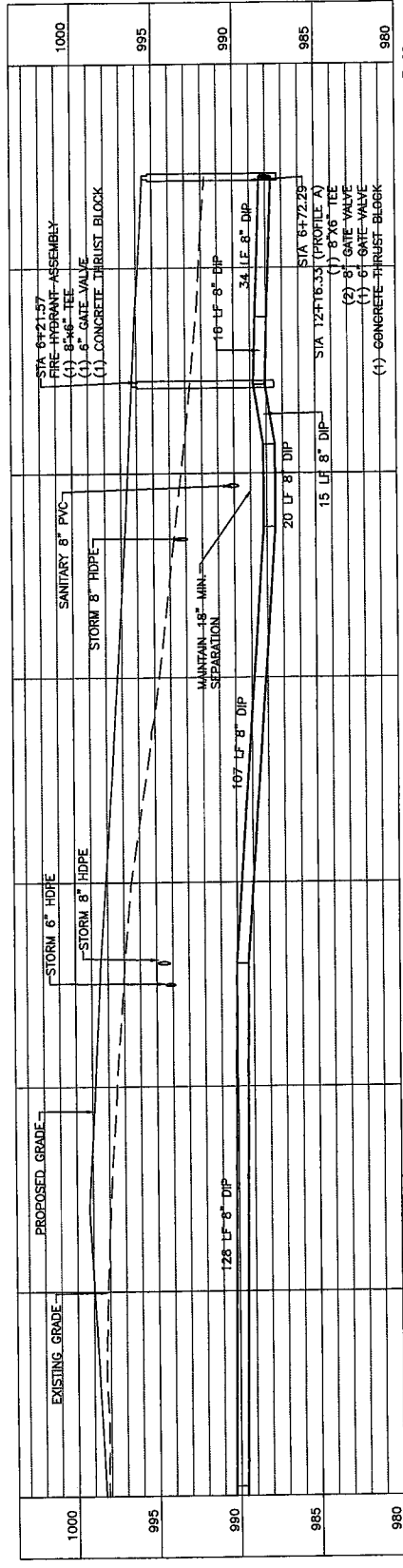
1 WATER PROFILE - A

SCALE: 1"=20' HORZ; 1"=5' VERT



2 WATER PROFILE - B

SCALE: 1"=20' HORZ; 1"=5' VERT



3 WATER PROFILE - B

SCALE: 1"=20' HORZ; 1"=5' VERT



**Architecture
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Interior Design**
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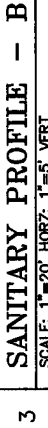
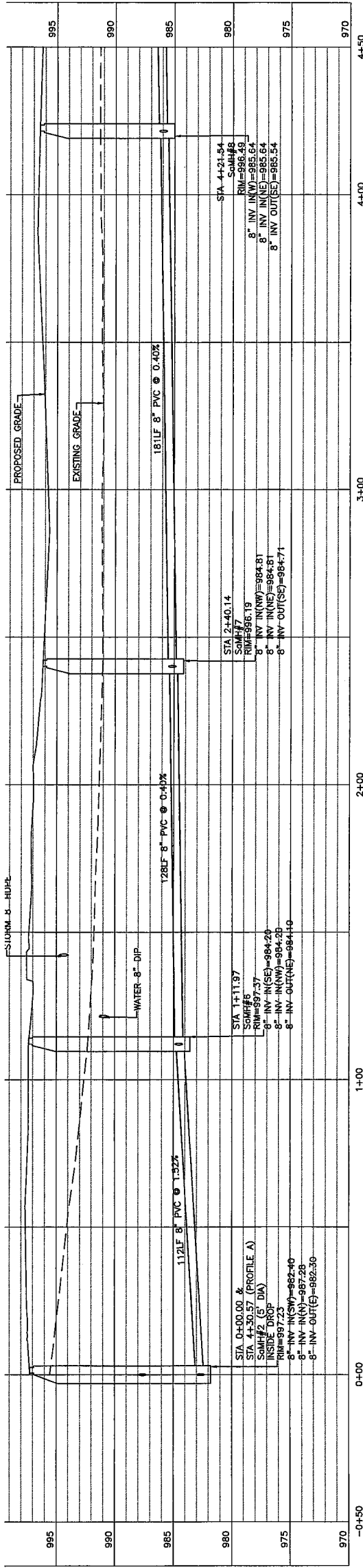
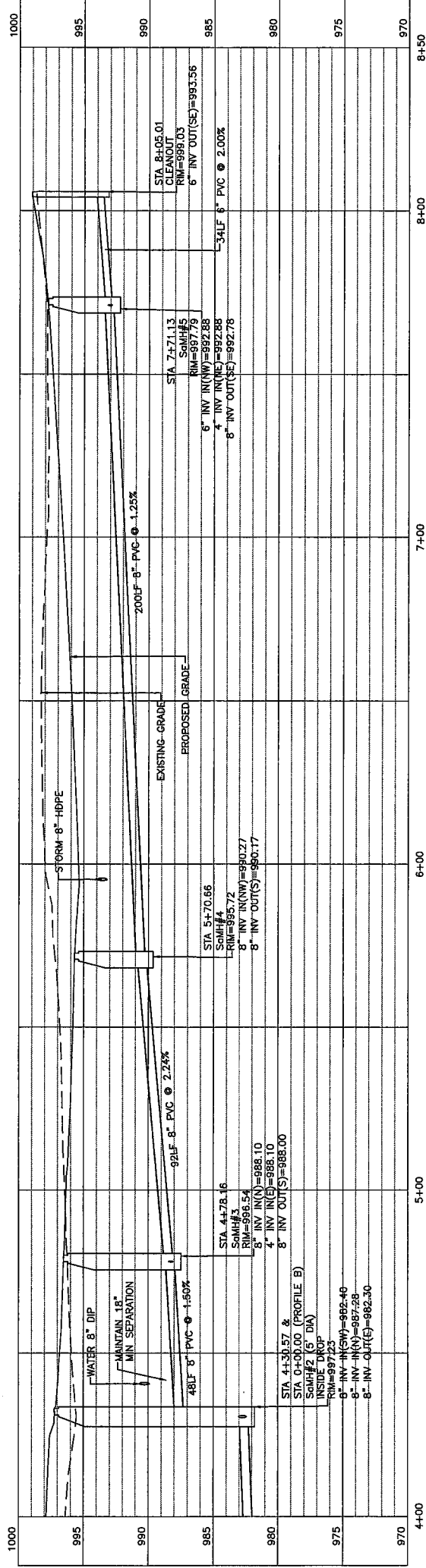
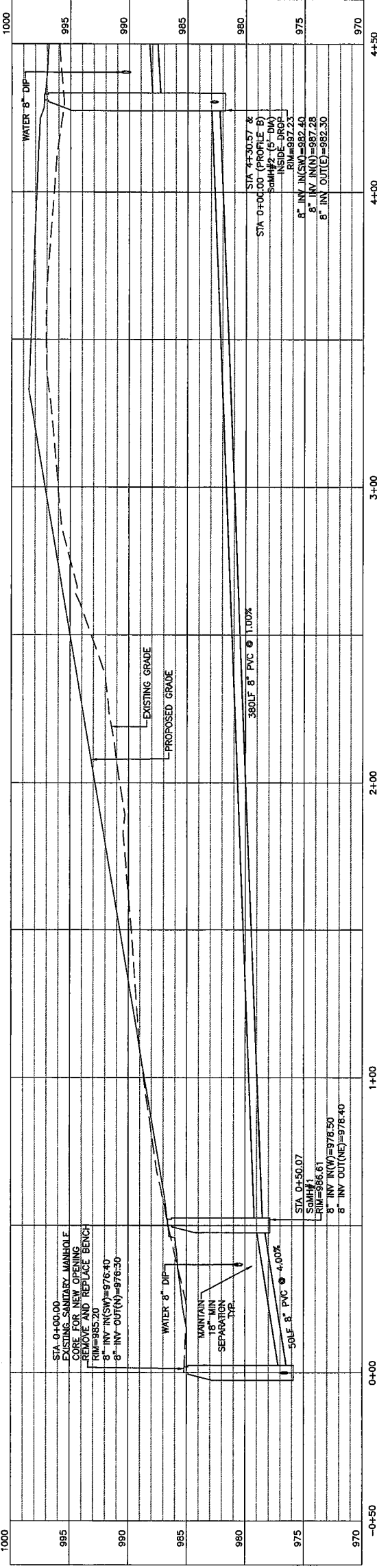
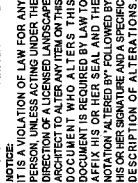
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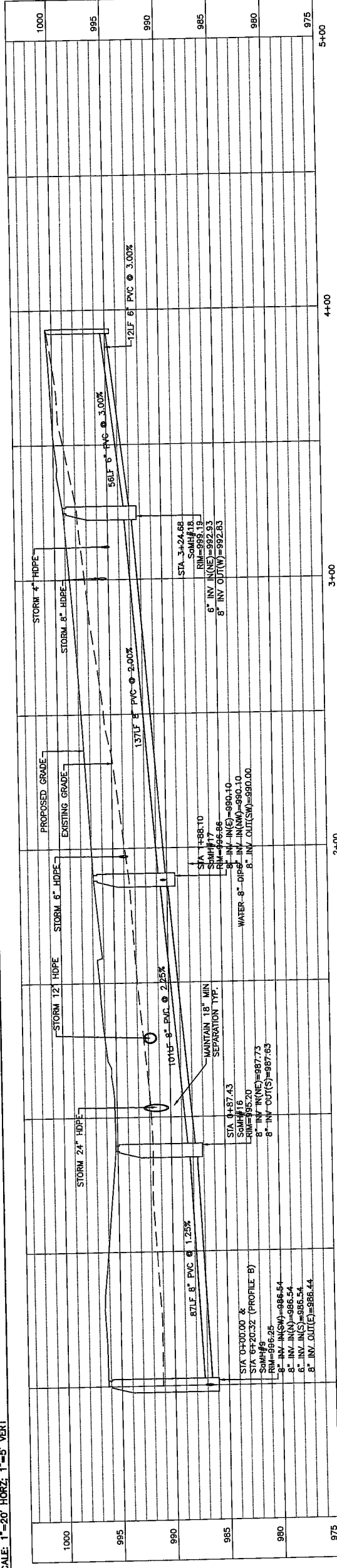
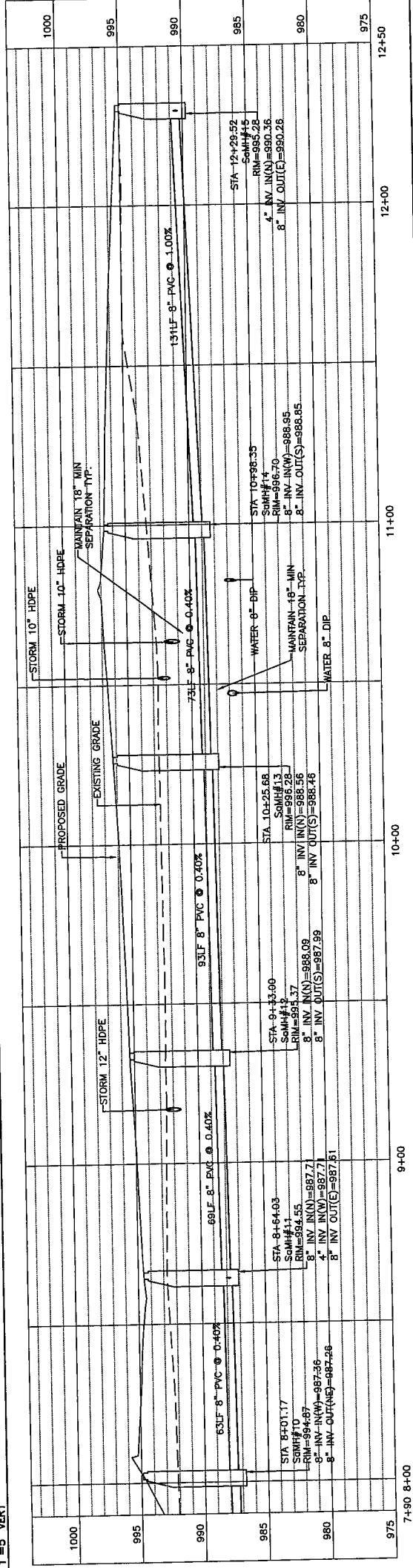
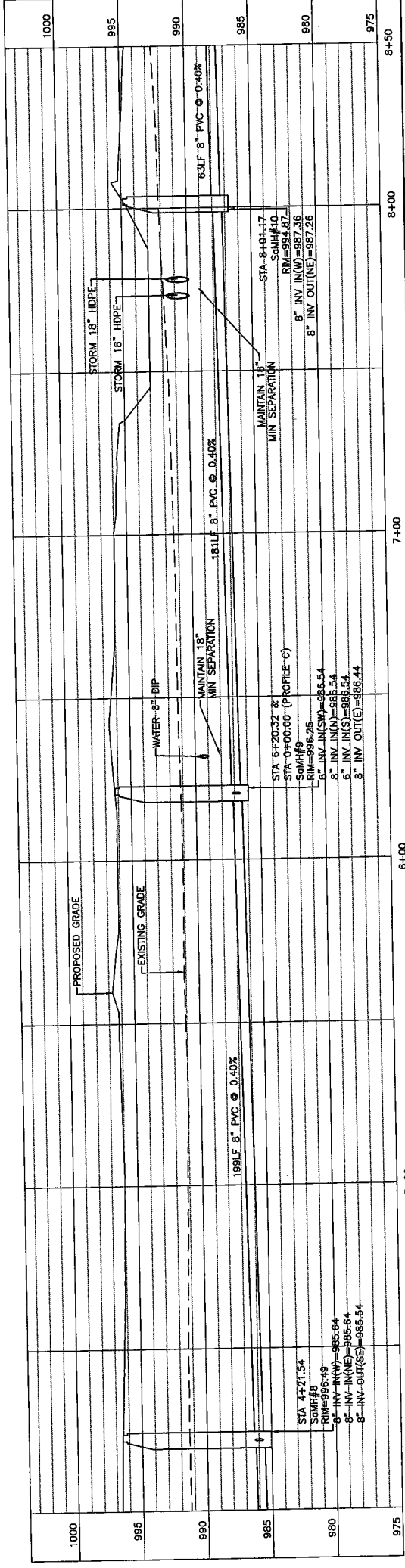
SANITARY PROFILES

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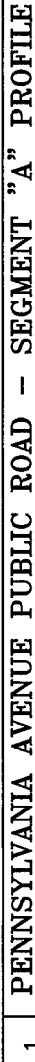
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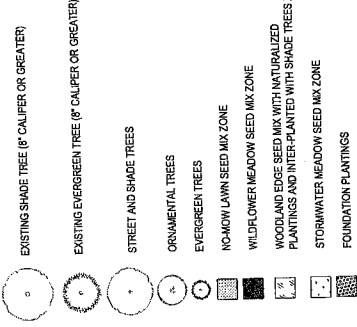


SCALE: 1"=20' HORZ; 1"=5' VERT



SCALE: 1"=20' HORZ; 1"=5' VERT

Exhibit E



DRAWING NOTES:
1. REFER TO L-105 FOR LISTS OF TYPICAL PLANT MATERIAL SPECIFIC TO ZONE.

Native status and frequency in the Cayuga region is taken from: Wiedley, F. R., S. Gaudetico, and P. L. Marini. 2008. Vascular plant species of the Cayuga Region of New York State. Cornell University, Ithaca, NY. <http://

STREET AND SHADE TREES

BOTANICAL NAME	COMMON NAME	MATURE HEIGHT	MATURE WIDTH	Species native to Cayuga region?	Species frequency in Cayuga region?
<i>Acer latifolium</i> "Frank A."	Redbarked Red Maple	45'	30'	Native	Common
<i>Acer spicatum</i> "Siberia"	Fall Festival Sugar Maple	50'	40'	Native	Common
<i>Alnus incana</i> "Siberia"	European Alder	30'	40'	Native	Common
<i>Carya americana</i> "Hemlock"	Shagbark Hickory	50'	35'	Non-native	Common
<i>Corylus americana</i> "Hemlock"	Shagbark Hickory	50'	35'	Non-native	Common
<i>Corylus americana</i> "Hemlock"	Shagbark Hickory	50'	35'	Non-native	Common
<i>Crataegus mollis</i> "C. C. McDaniel"	Prickly Thorn	15'	40'	Native	Common
<i>Fraxinus americana</i> "Hemlock"	White Oak	55'	45'	Native	Common
<i>Juniperus horizontalis</i> "Blue Chip"	Horizontal Juniper	10'	10'	Native	Common
<i>Quercus bicolor</i> "JFS-KW7"	White Oak	55'	45'	Native	Common
<i>Quercus macrocarpa</i> "JFS-KW7"	White Oak	55'	45'	Native	Common
<i>Thuja occidentalis</i> "Green Gem"	Green Gem Arborvitae	40'	30'	Native	Common

ORNAMENTAL TREES

BOTANICAL NAME	COMMON NAME	MATURE HEIGHT	MATURE WIDTH	Species native to Cayuga region?	Species frequency in Cayuga region?
<i>Abies balsamea</i> "Millers Pride"	Millers Pride Spruce	50'	30'	Native	Common
<i>Abies balsamea</i> "Millers Pride"	Millers Pride Spruce	50'	30'	Native	Common
<i>Abies balsamea</i> "Millers Pride"	Millers Pride Spruce	50'	30'	Native	Common
<i>Abies balsamea</i> "Millers Pride"	Millers Pride Spruce	50'	30'	Native	Common
<i>Abies balsamea</i> "Millers Pride"	Millers Pride Spruce	50'	30'	Native	Common
<i>Abies balsamea</i> "Millers Pride"	Millers Pride Spruce	50'	30'	Native	Common
<i>Abies balsamea</i> "Millers Pride"	Millers Pride Spruce	50'	30'	Native	Common
<i>Abies balsamea</i> "Millers Pride"	Millers Pride Spruce	50'	30'	Native	Common
<i>Abies balsamea</i> "Millers Pride"	Millers Pride Spruce	50'	30'	Native	Common
<i>Abies balsamea</i> "Millers Pride"	Millers Pride Spruce	50'	30'	Native	Common

EVERGREEN TREES

BOTANICAL NAME	COMMON NAME	MATURE HEIGHT	MATURE WIDTH	Species native to Cayuga region?	Species frequency in Cayuga region?
<i>Abies balsamea</i> "Millers Pride"	Millers Pride Spruce	50'	30'	Native	Common
<i>Abies balsamea</i> "Millers Pride"	Millers Pride Spruce	50'	30'	Native	Common
<i>Abies balsamea</i> "Millers Pride"	Millers Pride Spruce	50'	30'	Native	Common
<i>Abies balsamea</i> "Millers Pride"	Millers Pride Spruce	50'	30'	Native	Common
<i>Abies balsamea</i> "Millers Pride"	Millers Pride Spruce	50'	30'	Native	Common
<i>Abies balsamea</i> "Millers Pride"	Millers Pride Spruce	50'	30'	Native	Common
<i>Abies balsamea</i> "Millers Pride"	Millers Pride Spruce	50'	30'	Native	Common
<i>Abies balsamea</i> "Millers Pride"	Millers Pride Spruce	50'	30'	Native	Common
<i>Abies balsamea</i> "Millers Pride"	Millers Pride Spruce	50'	30'	Native	Common
<i>Abies balsamea</i> "Millers Pride"	Millers Pride Spruce	50'	30'	Native	Common

FOUNDATION PLANTINGS

BOTANICAL NAME	COMMON NAME	MATURE HEIGHT	MATURE WIDTH	Species native to Cayuga region?	Species frequency in Cayuga region?
<i>Abies balsamea</i> "Millers Pride"	Millers Pride Spruce	50'	30'	Native	Common
<i>Abies balsamea</i> "Millers Pride"	Millers Pride Spruce	50'	30'	Native	Common
<i>Abies balsamea</i> "Millers Pride"	Millers Pride Spruce	50'	30'	Native	Common
<i>Abies balsamea</i> "Millers Pride"	Millers Pride Spruce	50'	30'	Native	Common
<i>Abies balsamea</i> "Millers Pride"	Millers Pride Spruce	50'	30'	Native	Common
<i>Abies balsamea</i> "Millers Pride"	Millers Pride Spruce	50'	30'	Native	Common
<i>Abies balsamea</i> "Millers Pride"	Millers Pride Spruce	50'	30'	Native	Common
<i>Abies balsamea</i> "Millers Pride"	Millers Pride Spruce	50'	30'	Native	Common
<i>Abies balsamea</i> "Millers Pride"	Millers Pride Spruce	50'	30'	Native	Common
<i>Abies balsamea</i> "Millers Pride"	Millers Pride Spruce	50'	30'	Native	Common

NATURALIZATION PLANTINGS

BOTANICAL NAME	COMMON NAME	MATURE HEIGHT	MATURE WIDTH	Species native to Cayuga region?	Species frequency in Cayuga region?
<i>Abies balsamea</i> "Millers Pride"	Millers Pride Spruce	50'	30'	Native	Common
<i>Abies balsamea</i> "Millers Pride"	Millers Pride Spruce	50'	30'	Native	Common
<i>Abies balsamea</i> "Millers Pride"	Millers Pride Spruce	50'	30'	Native	Common
<i>Abies balsamea</i> "Millers Pride"	Millers Pride Spruce	50'	30'	Native	Common
<i>Abies balsamea</i> "Millers Pride"	Millers Pride Spruce	50'	30'	Native	Common
<i>Abies balsamea</i> "Millers Pride"	Millers Pride Spruce	50'	30'	Native	Common
<i>Abies balsamea</i> "Millers Pride"	Millers Pride Spruce	50'	30'	Native	Common
<i>Abies balsamea</i> "Millers Pride"	Millers Pride Spruce	50'	30'	Native	Common
<i>Abies balsamea</i> "Millers Pride"	Millers Pride Spruce	50'	30'	Native	Common
<i>Abies balsamea</i> "Millers Pride"	Millers Pride Spruce	50'	30'	Native	Common

VINES

BOTANICAL NAME	COMMON NAME	MATURE HEIGHT	MATURE WIDTH	Species native to Cayuga region?	Species frequency in Cayuga region?
<i>Abies balsamea</i> "Millers Pride"	Millers Pride Spruce	50'	30'	Native	Common
<i>Abies balsamea</i> "Millers Pride"	Millers Pride Spruce	50'	30'	Native	Common
<i>Abies balsamea</i> "Millers Pride"	Millers Pride Spruce	50'	30'	Native	Common
<i>Abies balsamea</i> "Millers Pride"	Millers Pride Spruce	50'	30'	Native	Common
<i>Abies balsamea</i> "Millers Pride"	Millers Pride Spruce	50'	30'	Native	Common
<i>Abies balsamea</i> "Millers Pride"	Millers Pride Spruce	50'	30'	Native	Common
<i>Abies balsamea</i> "Millers Pride"	Millers Pride Spruce	50'	30'	Native	Common
<i>Abies balsamea</i> "Millers Pride"	Millers Pride Spruce	50'	30'	Native	Common
<i>Abies balsamea</i> "Millers Pride"	Millers Pride Spruce	50'	30'	Native	Common
<i>Abies balsamea</i> "Millers Pride"	Millers Pride Spruce	50'	30'	Native	Common

DRAWING NOTES:
1. REFER TO L-104 FOR PLANTING ZONES.

Native status and frequency in the Cayuga region is taken from: Wiedley, F. R., S. Gaudetico, and P. L. Marini. 2008. Vascular plant species of the Cayuga Region of New York State. Cornell University, Ithaca, NY. <http://

STORMWATER MEADOW SEED MIX*

BOTANICAL NAME	COMMON NAME	Species native to Cayuga region?	Species frequency in Cayuga region?
<i>Abies balsamea</i> "Millers Pride"	Millers Pride Spruce	Native	Common
<i>Abies balsamea</i> "Millers Pride"	Millers Pride Spruce	Native	Common
<i>Abies balsamea</i> "Millers Pride"	Millers Pride Spruce	Native	Common
<i>Abies balsamea</i> "Millers Pride"	Millers Pride Spruce	Native	Common
<i>Abies balsamea</i> "Millers Pride"	Millers Pride Spruce	Native	Common
<i>Abies balsamea</i> "Millers Pride"	Millers Pride Spruce	Native	Common
<i>Abies balsamea</i> "Millers Pride"	Millers Pride Spruce	Native	Common
<i>Abies balsamea</i> "Millers Pride"	Millers Pride Spruce	Native	Common
<i>Abies balsamea</i> "Millers Pride"	Millers Pride Spruce	Native	Common
<i>Abies balsamea</i> "Millers Pride"	Millers Pride Spruce	Native	Common

WILDFLOWER MEADOW SEED MIX*

BOTANICAL NAME	COMMON NAME	Species native to Cayuga region?	Species frequency in Cayuga region?
<i>Abies balsamea</i> "Millers Pride"	Millers Pride Spruce	Native	Common
<i>Abies balsamea</i> "Millers Pride"	Millers Pride Spruce	Native	Common
<i>Abies balsamea</i> "Millers Pride"	Millers Pride Spruce	Native	Common
<i>Abies balsamea</i> "Millers Pride"	Millers Pride Spruce	Native	Common
<i>Abies balsamea</i> "Millers Pride"	Millers Pride Spruce	Native	Common
<i>Abies balsamea</i> "Millers Pride"	Millers Pride Spruce	Native	Common
<i>Abies balsamea</i> "Millers Pride"	Millers Pride Spruce	Native	Common
<i>Abies balsamea</i> "Millers Pride"	Millers Pride Spruce	Native	Common
<i>Abies balsamea</i> "Millers Pride"	Millers Pride Spruce	Native	Common
<i>Abies balsamea</i> "Millers Pride"	Millers Pride Spruce	Native	Common

WOODLAND EDGE SEED MIX*

BOTANICAL NAME	COMMON NAME	Species native to Cayuga region?	Species frequency in Cayuga region?
<i>Abies balsamea</i> "Millers Pride"	Millers Pride Spruce	Native	Common
<i>Abies balsamea</i> "Millers Pride"	Millers Pride Spruce	Native	Common
<i>Abies balsamea</i> "Millers Pride"	Millers Pride Spruce	Native	Common
<i>Abies balsamea</i> "Millers Pride"	Millers Pride Spruce	Native	Common
<i>Abies balsamea</i> "Millers Pride"	Millers Pride Spruce	Native	Common
<i>Abies balsamea</i> "Millers Pride"	Millers Pride Spruce	Native	Common
<i>Abies balsamea</i> "Millers Pride"	Millers Pride Spruce	Native	Common
<i>Abies balsamea</i> "Millers Pride"	Millers Pride Spruce	Native	Common
<i>Abies balsamea</i> "Millers Pride"	Millers Pride Spruce	Native	Common
<i>Abies balsamea</i> "Millers Pride"	Millers Pride Spruce	Native	Common

NO MOW LAWN SEED MIX*

BOTANICAL NAME	COMMON NAME	Species native to Cayuga region?	Species frequency in Cayuga region?
<i>Abies balsamea</i> "Millers Pride"	Millers Pride Spruce	Native	Common
<i>Abies balsamea</i> "Millers Pride"	Millers Pride Spruce	Native	Common
<i>Abies balsamea</i> "Millers Pride"	Millers Pride Spruce	Native	Common
<i>Abies balsamea</i> "Millers Pride"	Millers Pride Spruce	Native	Common
<i>Abies balsamea</i> "Millers Pride"	Millers Pride Spruce	Native	Common
<i>Abies balsamea</i> "Millers Pride"	Millers Pride Spruce	Native	Common
<i>Abies balsamea</i> "Millers Pride"	Millers Pride Spruce	Native	Common
<i>Abies balsamea</i> "Millers Pride"	Millers Pride Spruce	Native	Common
<i>Abies balsamea</i> "Millers Pride"	Millers Pride Spruce	Native	Common
<i>Abies balsamea</i> "Millers Pride"	Millers Pride Spruce	Native	Common

TROWBRIDGE
WOLF
MICHAELS

TWMA

LANDSCAPE ARCHITECTS

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DATE: 3/16/18 BY: 3/16/18

REVISION: 3/16/18

COMMENT: 3/16/18

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TROWBRIDGE WOLF MICHAELS

Sundial Property Development LLC
Ithaca Neighborhood Housing Services & Trumansburg, New York

46 South Street

DATE	12/13/2017
PROJECT	17003
DRAWN BY	RK
CHECKED	

LANDSCAPE
PLANT LISTS

L-105

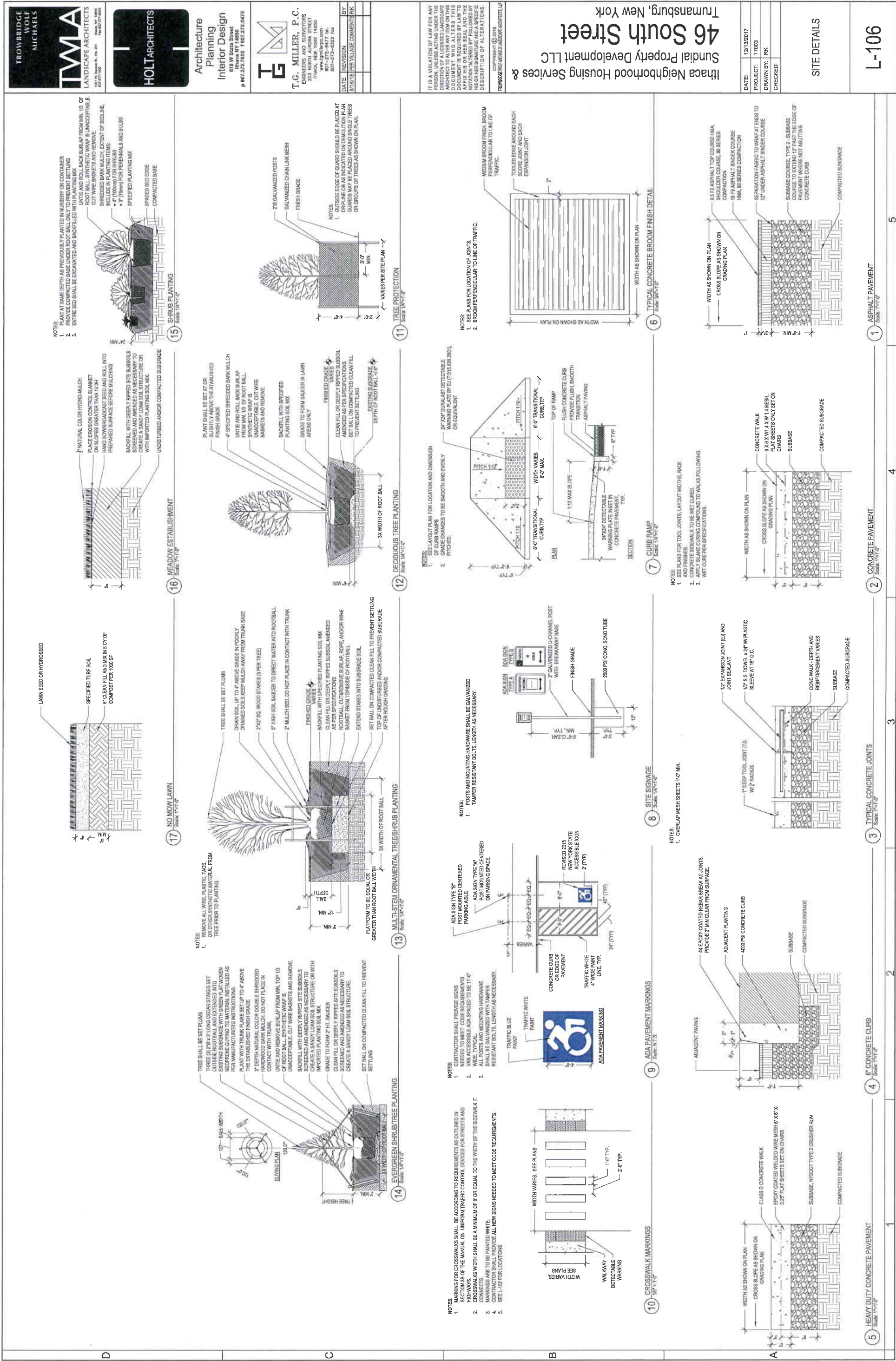


Exhibit F

TROWBRIDGE
WOLF
MICHAELS

Exhibit G

46 South Street

Preliminary Stormwater Calculations

Summary

***Village of Trumansburg
Tompkins County, New York***

Prepared for:

***Ithaca Neighborhood Housing Services &
Sundial Property Development LLC
115 West Clinton Street
Ithaca, NY 14850***

Prepared by:



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March 16, 2018

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PROJECT DESCRIPTION

Purpose and Extent of Proposed Development

The 46 South Street project is located in the Village of Trumansburg, Tompkins County, New York (Tax Map Parcels 9.-1-2 & 8.-3-2.2). The project includes the consolidation of the two parcels then the subdivision of the 19.115 acres into 15 parcels that will include market rate for-sale units, affordable for-sale townhomes, affordable rental townhomes, rental apartments and a nursery school. The project will also include various amenities such roads, parking and walkways.

The stormwater management objectives for the project focus on treatment of runoff from the post-developed site. As a townhome and multifamily residential property disturbing greater than one acre of land, a full Stormwater Pollution Prevention Plan (SWPPP) is required, including both temporary erosion controls and permanent stormwater management practices under the regulations of the Village of Trumansburg and New York State Department of Environmental Conservation (DEC). Stormwater management objectives for the site include:

- Providing water quality treatment by means of stormwater wetlands, a bioretention filter, and rain gardens.
- Provide Runoff Reduction by means of rain gardens and a bioretention filter.
- Providing stormwater detention to meet DEC's standards for mitigating runoff from the 1-, 10-, and 100-year storm events.

Project Disturbance Area

Total Disturbed Area: 14.91 acres

Existing Impervious Area: 0.00 acres

Proposed Impervious Area: 4.69 acres

Increase in Impervious Area: 4.69 acres

Description and Limitations of On-Site Soils

On-site soils consist of Howard gravelly loam (33.7%), Lansing gravelly silt loam (7.6%), Ovid silt loam (13.7%) and Rhinebeck silt loam (45.0%) based on the USDA Soil Surveys of Tompkins County. Based upon the classification of soils defined by the Natural Resource Conservation Service, the site contains 33% HSG "A" 8% HSG "B" and 59% HSG "D" soils.

A geotechnical investigation to determine the soil types and properties for the on-site soils was conducted by the geotechnical consultant, Empire Geo-Services Inc., in August 2017. The report shows higher groundwater in the areas associated with "D" soils in the USDA report.

POST-CONSTRUCTION STORMWATER MANAGEMENT

Existing Conditions

The project site is best characterized as undeveloped land, and will disturb approximately 14.91 acres. 100% of the existing site cover is pervious.

There are two watersheds in the vicinity of the project site that will be impacted by the proposed project. The western watershed (WS#1) has been divided into two subareas (WS#1A and WS#1B).

Water Quality Controls

The water quality strategy is designed to improve water quality by capturing and treating 90% of the average annual stormwater runoff volume. The required water quality volume is calculated from the following equation:

$$WQ_v = P \cdot (0.05 + 0.009 \cdot I) \cdot A / 12$$

Where:

$$\begin{aligned} P &= 90\% \text{ rainfall event (inches)} \\ &= 1.00 \text{ inches (Ithaca, NY)} \\ R_v &= (0.05 + 0.009 \cdot I) \text{ (minimum allowed value} = 0.20) \\ I &= \text{Imperviousness (\%)} \\ A &= \text{Drainage Area (s.f.)} \\ &= 19.12 \text{ acres (site acreage was used to determine requirements)} \end{aligned}$$

$$\begin{aligned} \text{Therefore: } I &= 4.69 \text{ acres} / 19.12 \text{ acres} \\ &= 25\% \end{aligned}$$

$$\begin{aligned} R_v &= (0.05 + 0.009 \cdot 25\%) \\ &= 0.27 \end{aligned}$$

$$\begin{aligned} \text{Required } WQ_v &= 1.00'' \cdot 0.27 \cdot 19.12 / 12 \\ &= 0.431 \text{ acre feet} \\ &= 18,795 \text{ cubic feet} \end{aligned}$$

The project plans to utilize both rooftop disconnection and tree planting credits towards the water quality and runoff reduction requirements. These credits are applied by recalculating the WQ_v and RR_v requirements while counting the disconnected rooftop portions and up to 100 square feet of impervious cover per tree as pervious surfaces.

Rooftop disconnections: Most of the buildings were counted towards this credit. The large multifamily building, half of the nursery, and half of the two buildings adjacent to existing Wetland "A" were not counted, as their roof runoff is unable to be directed to vegetated areas that meet the NYSDEC requirements. 0.74 acres of roofs are counted in this credit. Although the site soils are mostly HSG "D," soil restoration will be applied throughout the site where soils have been disturbed. Soil restoration is applied in the cleanup, restoration, and landscaping phase of construction followed by the permanent establishment of an appropriate, deep-rooted groundcover to help maintain the restored soil structure. The required measures of soil restoration will be outlined in greater detail in the Full SWPPP.

Tree Planting: Only trees along roads, having canopies greater than 16 feet in diameter were counted for this credit. If the tree canopies did not cover adequate impervious cover, they were not counted. 104 trees were counted, with 100 square feet of impervious cover being credited per tree (for a total of 0.24 acres).

The recalculated water quality volume is as shown as follows:

$$\begin{aligned} P &= 90\% \text{ rainfall event (inches)} \\ &= 1.00 \text{ inches (Ithaca, NY)} \\ R_v &= (0.05 + 0.009 \cdot I) \text{ (minimum allowed value} = 0.20) \end{aligned}$$

Water Quantity Controls

The water quantity practice is designed to reduce peak discharges for the 1, 10, and 100-year storms to below pre-developed rates at the point of analysis. In Watershed 1A some small storage will be continue to be provided in existing Wetland "A." However, Watersheds #1A and #1B will both drain to the proposed Stormwater Wetlands to attenuate post-developed peak flows. Watershed #1C will be mitigated by means of a separate Stormwater Wetland, and Watershed #1D is not captured and sheet drains off the site.

Watershed #2C contains the South Street drive, the majority of which will be captured by underground detention and then treated by a hydrodynamic separator unit. Watersheds #2A and #2C will remain largely unchanged, with some small areas of woods and meadow being converted to lawn prior to draining off of the site.

Table 3 summarizes resulting peak discharge rates from within each of these watersheds.

The existing 18" culvert along South Street will receive runoff from Watershed #2B and 2C. To ensure that the increase in rates of runoff to South Street will not negatively impact the culvert, it was analyzed in the HydroCAD model. The model results show that the pipe passes the 25-year storm without any issues. The 100-year storm would surcharge DI #14's grate and spill into the road. As most municipal road storm sewers are designed for 25-year storm events, this result was not unexpected. The pipe was not modeled in the existing conditions, as all of the structures contributing to the pipe are buried or the rims are higher than adjacent grades. Currently there is little, if any, stormwater entering the pipe through existing structures.

Practice Sizing

Bioretention Filter

The filter will capture and treat runoff from a portion of Watershed #1B. The filter is sized using Darcy's Law as presented in the New York State Stormwater Management Design Manual, using the following equation:

$$A_f = WQ_v (d_f) / [(k)(T)(d_f + h_f)]$$

Where:

$$\begin{aligned} A_f &= \text{Filter Area (sf)} \\ d_f &= \text{Filter Depth (feet)} = 2.0 \text{ feet} \\ h_f &= \text{Average Head Above Filter (feet)} = 0.5 \text{ feet} \\ T_f &= \text{Filtering Time (days)} = 2 \text{ days} \\ k &= \text{Soil Permeability (ft/day)} = 0.5 \text{ ft/day} \\ WQ_v &= \text{Water Quality Volume (cf)} \end{aligned}$$

Therefore:

$$\begin{aligned} P &= 90\% \text{ rainfall event (inches)} \\ &= 1.00 \text{ inches (Ithaca, NY)} \\ R_v &= (0.05 + 0.009 * I) \text{ (minimum allowed value} = 0.20) \\ I &= \text{Imperviousness (\%)} \\ A &= \text{Drainage Area (s.f.)} \\ &= 1.67 \text{ acres (site acreage was used to determine requirements)} \end{aligned}$$

$$\begin{aligned} \text{Therefore: } I &= (1.15 \text{ acres}) / 1.67 \text{ acres} \\ &= 69\% \end{aligned}$$

$$\begin{aligned} \text{Required } WQ_v &= 1.00'' * (0.05 + 0.009 * 69\%) * 1.67 / 12 \\ &= 0.093 \text{ acre feet} \\ &= 4,060 \text{ cubic feet} \end{aligned}$$

Therefore:

$$\begin{aligned} A_f &= 4,060 * 2.0 / [(0.5)(2)(2 + 0.5)] \\ A_f &= 3,609 \text{ square feet } \textbf{required} \end{aligned}$$

As bioretention filters in "C/D" soils only provide 40% RR_v, the filter will be oversized by 2.5 to provide enough surface area to provide 100% RR_v for the drainage area.

$$\begin{aligned} A_f &= 2.5 * 3,609 = 9,020 \text{ square feet } \textbf{required} \\ A_f &= 9,020 \text{ square feet } \textbf{provided} \end{aligned}$$

Two of the filters are located in HSG "A" soils and two in HSG "D" soils. Similar to bioretention filters, 100% of WQv treated is counted towards RRv in HSG "A/B" soils and 40% in HSG "C/D" soils. The RRv provided is as follows:

HSG "A" gardens	RRv	=	100% x 90 cubic feet x 2 filters
	RRv	=	180 cubic feet provided
HSG "C" gardens	RRv	=	40% x 90 cubic feet x 2 filters
	RRv	=	72 cubic feet provided

The RRv provided by the Rain Gardens added to the RRv provided by the Bioretention Filter meets the minimum RRv requirements for the site:

Bioretention RRv	=	4,060 cubic feet
Rain Garden RRv	=	180 cubic feet + 72 cubic feet
Total RRv	=	4,312 cubic feet provided
Required RRv	=	4,196 cubic feet (See attached calculations)

Hydrodynamic Separator

A hydrodynamic separator unit will be used to treat runoff from the South Street drive, before it enters the existing South Street storm sewer. See attached calculations for small storm hydrology calculations. These calculations, along with the HydroCAD data, was given to Contech in order to size the unit. Their sizing calculations are attached.

Stormwater Wetlands

The wetland practices are designed to mitigate stormwater discharges for the 1-, 10- and 100-year storm events, while provided WQv treatment for areas not treated by the bioretention filter (see attached calculations). The large stormwater wetland that treats WS#1B will have two outlet control structures, with three 18-inch culverts that discharge to existing Wetland "F" which is the Point of Analysis for Watershed #1. The smaller stormwater wetland practice will have a single outlet control structure with one 8-inch culvert that discharges to Wetland "F." Both practices have 3-inch orifices to provide Channel Protection.

The wetland practices were sized using HydroCAD, as can be seen in the attached calculations.

Existing Wetland "A" will remain largely unchanged. While the watershed is being reduced in size, HydroCAD was used to ensure that water elevations in the wetland were maintained during the 1-, 10- and 100-year storm events.

Underground Detention System

To manage runoff from the South Street drive, underground pipe storage is being proposed to mitigate the 1-, 10- and 100-year storm events. The piping has been sized in HydroCAD and includes an outlet control structure with a 3-inch orifice for channel protection and a weir to detain water in the upstream pipes.

46 South Street

Preliminary Stormwater Calculations

Summary

*Village of Trumansburg
Tompkins County, New York*

Prepared for:

*Ithaca Neighborhood Housing Services &
Sundial Property Development LLC
115 West Clinton Street
Ithaca, NY 14850*

Prepared by:



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March 16, 2018

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Where:

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Rv	=	(0.05+0.009*I) (minimum allowed value = 0.20)
I	=	Imperviousness (%)
A	=	Drainage Area (s.f.)
	=	19.12 acres (site acreage was used to determine requirements)

Therefore:	I	=	4.69 acres / 19.12 acres
		=	25%

Rv	=	(0.05+0.009*25%)
	=	0.27

Required WQ _v	=	1.00 * 0.27 * 19.12 / 12
	=	0.431 acre feet
	=	18,795 cubic feet

The project plans to utilize both rooftop disconnection and tree planting credits towards the water quality and runoff reduction requirements. These credits are applied by recalculating the WQ_v and RR_v requirements while counting the disconnected rooftop portions and up to 100 square feet of impervious cover per tree as pervious surfaces.

Rooftop disconnections: Most of the buildings were counted towards this credit. The large multifamily building, half of the nursery, and half of the two buildings adjacent to existing Wetland "A" were not counted, as their roof runoff is unable to be directed to vegetated areas that meet the NYSDEC requirements. 0.74 acres of roofs are counted in this credit. Although the site soils are mostly HSG "D," soil restoration will be applied throughout the site where soils have been disturbed. Soil restoration is applied in the cleanup, restoration, and landscaping phase of construction followed by the permanent establishment of an appropriate, deep-rooted groundcover to help maintain the restored soil structure. The required measures of soil restoration will be outlined in greater detail in the Full SWPPP.

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Watershed #2C contains the South Street drive, the majority of which will be captured by underground detention and then treated by a hydrodynamic separator unit. Watersheds #2A and #2C will remain largely unchanged, with some small areas of woods and meadow being converted to lawn prior to draining off of the site.

Table 3 summarizes resulting peak discharge rates from within each of these watersheds.

The existing 18" culvert along South Street will receive runoff from Watershed #2B and 2C. To ensure that the increase in rates of runoff to South Street will not negatively impact the culvert, it was analyzed in the HydroCAD model. The model results show that the pipe passes the 25-year storm without any issues. The 100-year storm would surcharge DI #14's grate and spill into the road. As most municipal road storm sewers are designed for 25-year storm events, this result was not unexpected. The pipe was not modeled in the existing conditions, as all of the structures contributing to the pipe are buried or the rims are higher than adjacent grades. Currently there is little, if any, stormwater entering the pipe through existing structures.

Practice Sizing

Bioretention Filter

The filter will capture and treat runoff from a portion of Watershed #1B. The filter is sized using Darcy's Law as presented in the New York State Stormwater Management Design Manual, using the following equation:

$$A_f = WQ_v (d_f) / [(k)(T)(d_f + h_f)]$$

Where:

$$\begin{aligned} A_f &= \text{Filter Area (sf)} \\ d_f &= \text{Filter Depth (feet)} = 2.0 \text{ feet} \\ h_f &= \text{Average Head Above Filter (feet)} = 0.5 \text{ feet} \\ T_f &= \text{Filtering Time (days)} = 2 \text{ days} \\ k &= \text{Soil Permeability (ft/day)} = 0.5 \text{ ft/day} \\ WQ_v &= \text{Water Quality Volume (cf)} \end{aligned}$$

Therefore:

$$\begin{aligned} P &= 90\% \text{ rainfall event (inches)} \\ &= 1.00 \text{ inches (Ithaca, NY)} \\ R_v &= (0.05 + 0.009 * I) \text{ (minimum allowed value} = 0.20) \\ I &= \text{Imperviousness (\%)} \\ A &= \text{Drainage Area (s.f.)} \\ &= 1.67 \text{ acres (site acreage was used to determine requirements)} \end{aligned}$$

$$\begin{aligned} \text{Therefore: } I &= (1.15 \text{ acres}) / 1.67 \text{ acres} \\ &= 69\% \end{aligned}$$

$$\begin{aligned} \text{Required } WQ_v &= 1.00'' * (0.05 + 0.009 * 69\%) * 1.67 / 12 \\ &= 0.093 \text{ acre feet} \\ &= 4,060 \text{ cubic feet} \end{aligned}$$

Therefore:

$$\begin{aligned} A_f &= 4,060 * 2.0 / [(0.5)(2)(2 + 0.5)] \\ A_f &= 3,609 \text{ square feet } \textbf{required} \end{aligned}$$

As bioretention filters in "C/D" soils only provide 40% RRv, the filter will be oversized by 2.5 to provide enough surface area to provide 100% RRv for the drainage area.

$$\begin{aligned} A_f &= 2.5 * 3,609 = 9,020 \text{ square feet } \textbf{required} \\ A_f &= 9,020 \text{ square feet } \textbf{provided} \end{aligned}$$

Two of the filters are located in HSG "A" soils and two in HSG "D" soils. Similar to bioretention filters, 100% of WQv treated is counted towards RRv in HSG "A/B" soils and 40% in HSG "C/D" soils. The RRv provided is as follows:

HSG "A" gardens	RRv	=	100% x 90 cubic feet x 2 filters
	RRv	=	180 cubic feet <i>provided</i>
HSG "C" gardens	RRv	=	40% x 90 cubic feet x 2 filters
	RRv	=	72 cubic feet <i>provided</i>

The RRv provided by the Rain Gardens added to the RRv provided by the Bioretention Filter meets the minimum RRv requirements for the site:

Bioretention RRv	=	4,060 cubic feet
Rain Garden RRv	=	180 cubic feet + 72 cubic feet
Total RRv	=	4,312 cubic feet <i>provided</i>
Required RRv	=	4,196 cubic feet (See attached calculations)

Hydrodynamic Separator

A hydrodynamic separator unit will be used to treat runoff from the South Street drive, before it enters the existing South Street storm sewer. See attached calculations for small storm hydrology calculations. These calculations, along with the HydroCAD data, was given to Contech in order to size the unit. Their sizing calculations are attached.

Stormwater Wetlands

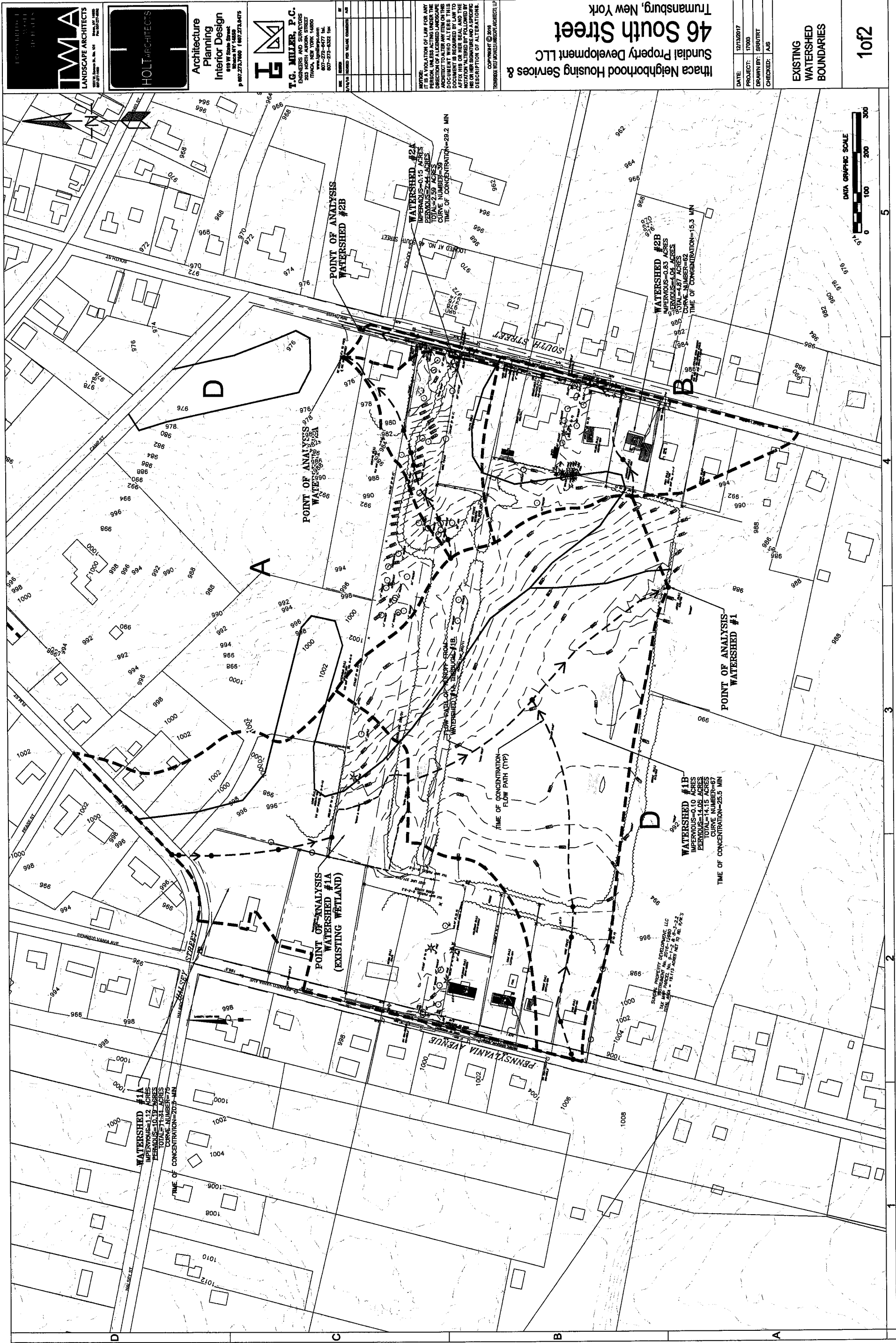
The wetland practices are designed to mitigate stormwater discharges for the 1-, 10- and 100-year storm events, while provided WQv treatment for areas not treated by the bioretention filter (see attached calculations). The large stormwater wetland that treats WS#1B will have two outlet control structures, with three 18-inch culverts that discharge to existing Wetland "F" which is the Point of Analysis for Watershed #1. The smaller stormwater wetland practice will have a single outlet control structure with one 8-inch culvert that discharges to Wetland "F." Both practices have 3-inch orifices to provide Chanel Protection.

The wetland practices were sized using HydroCAD, as can be seen in the attached calculations.

Existing Wetland "A" will remain largely unchanged. While the watershed is being reduced in size, HydroCAD was used to ensure that water elevations in the wetland were maintained during the 1-, 10- and 100-year storm events.

Underground Detention System

To manage runoff from the South Street drive, underground pipe storage is being proposed to mitigate the 1-, 10- and 100-year storm events. The piping has been sized in HydroCAD and includes and outlet control structure with a 3-inch orifice for channel protection and a weir to detain water in the upstream pipes.



EXISTING
WATERSHED
BOUNDARIES

DATE: 12/13/2017
PROJECT: 17008
DRAWN BY: SRR/JRT
CHECKED: JAS

Ithaca Neighborhood Housing Services &
Sundial Property Development LLC
46 South Street
Trumansburg, New York

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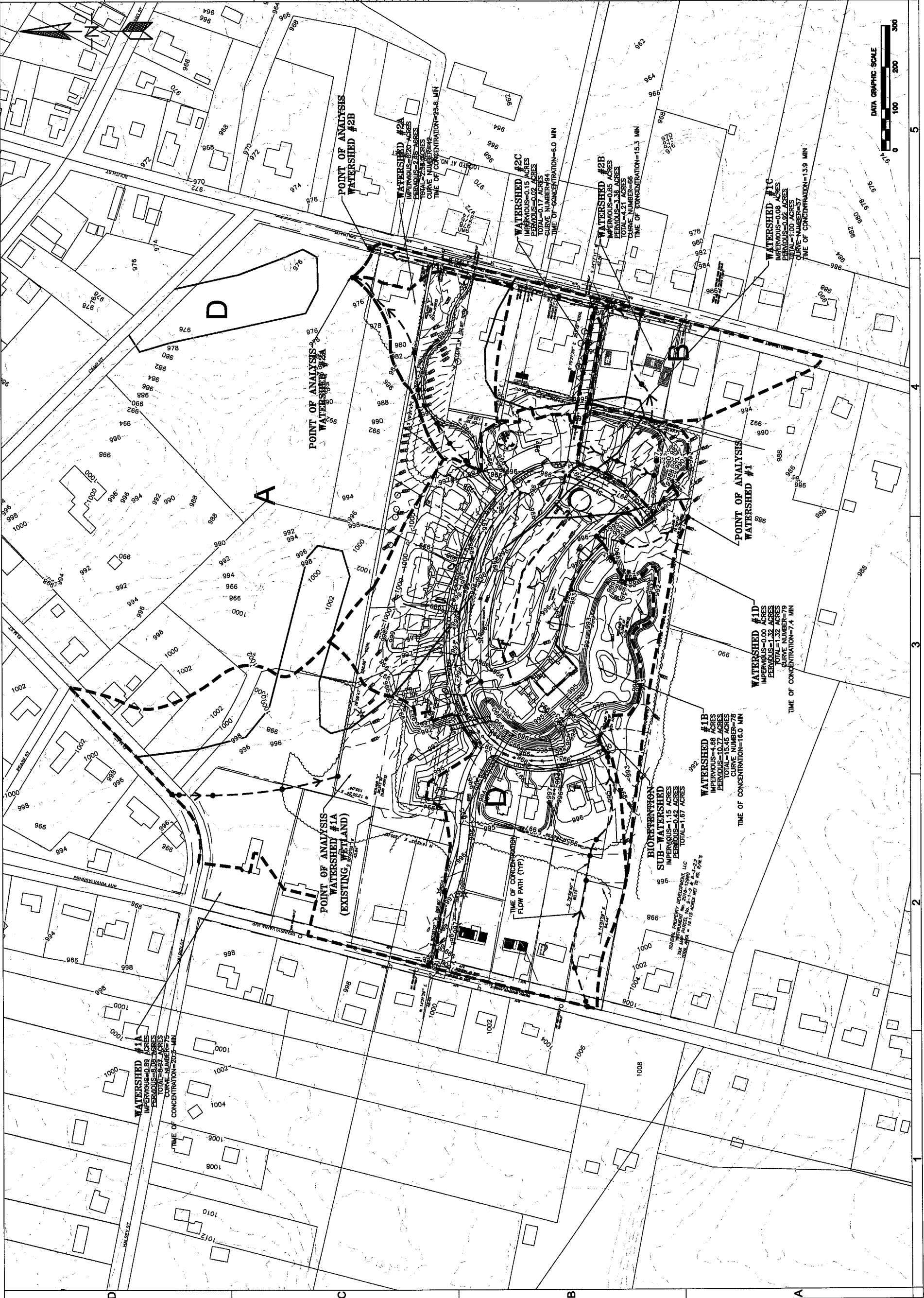
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THOMBRIDGE WOLF MICHAELS LANDSCAPE ARCHITECTS, LLP

DATE:	12/13/2017
PROJECT:	17003
DRAWN BY:	SRP/TRT
CHECKED:	AJS

**PROPOSED
WATERSHED
BOUNDARIES**

20f2



Site Water Quality Volume

$$WQ_v = P * R_v * A / 12$$

Where: $R_v = (0.05 + 0.009 * I)$ (min 0.20)

Impervious Cover (acres):

Site Area (acres):

Imperviousness, I (%):

WQ Storm, P (in):

Rv:

WQ Volume Required (acre-feet):

WQ Volume Required (cubic feet):

Site Runoff Reduction Calculations

$$RR_v = (P) (R_v^*) (A_i) / 12$$

Where: $A_i = (S) (A_{ic})$

Impervious Cover (acres), Aic:

WQ Storm, P:

HSG Reduction Factor, S:

Impervious Cover targeted for RRv, Ai:

Rv*:

Minimum RRv (acre-feet):

Minimum RRv (cubic feet):

HSG:

- A 6.15 Ac (32%)
- B 1.55 Ac (8%)
- C 0.00 Ac (0%)
- D 11.42 Ac (60%)

Site Water Quality Volume Recalculated After Accounting for Tree Plantings

$$WQ_v = P * R_v * A / 12$$

Where: $R_v = (0.05 + 0.009 * I)$ (min 0.20)

Impervious Cover (acres): minus 104 trees x 100sf
(0.24 acres)

Drainage Area (acres):

Imperviousness, I (%):

WQ Storm, P (in):

Rv:

WQ Volume Required (acre-feet):

WQ Volume Required (cubic feet):

Site Runoff Reduction Calculations After Accounting for Tree Plantings

$$RR_v = (P) (R_v^*) (A_i) / 12$$

Where: $A_i = (S) (A_{ic})$

Impervious Cover (acres), A_{ic} :

WQ Storm, P:

HSG Reduction Factor, S:

Impervious Cover targeted for RR_v , A_i :

R_v^* :

Minimum RR_v (acre-feet):

Minimum RR_v (cubic feet):

HSG:

A	6.15 Ac	(615%)
B	1.55 Ac	(155%)
C	0.00 Ac	(0%)
D	11.42 Ac	(1142%)

Rain Garden Design

Water Quality Volume

$$WQ_v = P * R_v * A / 12$$

Where: $R_v = (0.05 + 0.009 * I)$

Impervious Cover (acres):

Drainage Area (acres):

Imperviousness, I (%):

WQ Storm, P (in):

R_v:

WQ Volume Required (acre-feet):

WQ Volume Required (cubic feet):

Rain Garden Sizing

$$V = V_{sm} + V_{dl} + (dp * A)$$

$$V_{sm} = A * d_{sm} * n_{sm}$$

$$V_{dl} = A * d_{dl} * n_{dl}$$

WQ_v (cf):

Rain Garden Surface Area, a_{gr} (s.f.):

Depth of Soil Media, d_{sm} (ft):

Depth of Drainage Layer, d_{dl} (ft):

Depth of Ponding, d_p (ft):

Porosity of Soil Media, n_{sm}:

Porosity of Drainage Layer, n_{dl}:

Volume of Soil Layer, V_{sm} (ft):

Small Storm Hydrology Calculations - Hydrodynamic Separator

Water Quality Volume

$$WQ_v = P * R_v * A / 12$$

$$\text{Where: } R_v = (0.05 + 0.009 * I) \text{ (min 0.20)}$$

Impervious Cover (acres): 0.150

Drainage Area, A (acres): 0.170

Imperviousness, I (%): 88%

WQ Storm, P (in): 1.00

Rv: 0.84

WQ Volume Required (acre-feet): 0.012

WQ Volume Required (cubic feet): 520

Small Storm Hydrology

$$CN = 1000 / [10 + 5P + 10Q - 10(Q^2 + 1.25 QP)^{1/2}]$$

$$Q = WQ_v * 12 / DA$$

$$Q_p = q_u * A * WQ_v$$

$$A = \text{Drainage Area} / 640 = \text{square miles}$$

WQv (ac-ft): 0.012

Runoff Volume, Q (in): 0.84

Adjusted Curve Number, CN: 99

Initial Abstracton, Ia: 0.041 (from TR-55, Table 4-I)

WQ Storm, P (in): 1.00

Ia/P: 0.041

Unit Peak Discharge, qu (cfs/sq mi/inch): 1,000 (from TR-55, Exhibit 4-II)

Drainage Area, A (sq mi) 0.00027

Qp: 0.22

Small Storm Hydrology Calculations - DI #2

Water Quality Volume

$$WQ_v = P * R_v * A / 12$$

$$\text{Where: } R_v = (0.05 + 0.009 * I) \text{ (min 0.20)}$$

Impervious Cover (acres): 0.570

Drainage Area, A (acres): 0.900

Imperviousness, I (%): 63%

WQ Storm, P (in): 1.00

Rv: 0.62

WQ Volume Required (acre-feet): 0.047

WQ Volume Required (cubic feet): 2,025

Small Storm Hydrology

$$CN = 1000 / [10 + 5P + 10Q - 10(Q^2 + 1.25 QP)^{1/2}]$$

$$Q = WQ_v * 12 / DA$$

$$Q_p = q_u * A * WQ_v$$

$$A = \text{Drainage Area} / 640 = \text{square miles}$$

WQv (ac-ft): 0.047

Runoff Volume, Q (in): 0.62

Adjusted Curve Number, CN: 96

Initial Abstracton, Ia: 0.083 (from TR-55, Table 4-I)

WQ Storm, P (in): 1.00

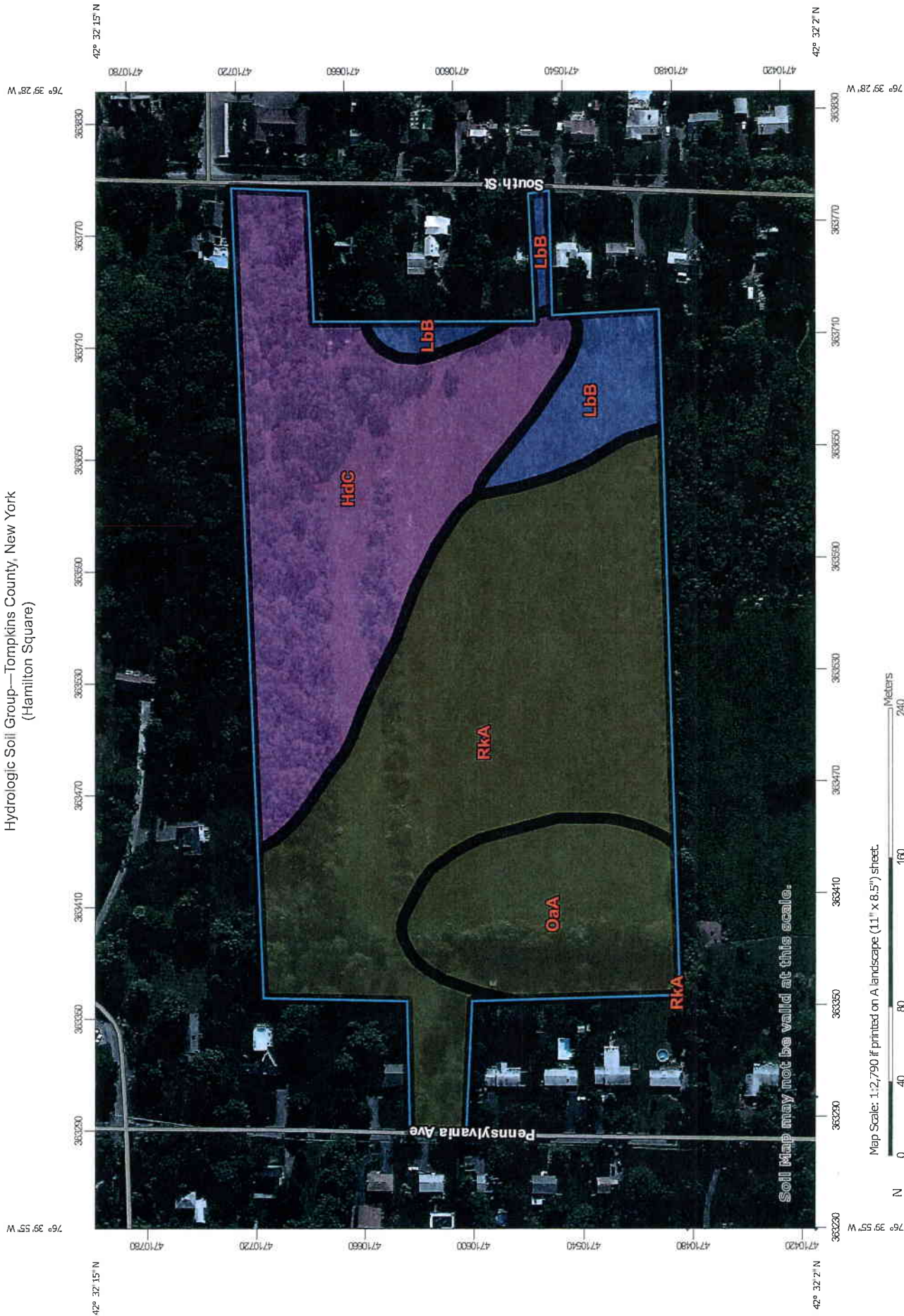
Ia/P: 0.083

Unit Peak Discharge, qu (cfs/sq mi/inch): 1,000 (from TR-55, Exhibit 4-II)

Drainage Area, A (sq mi) 0.00141

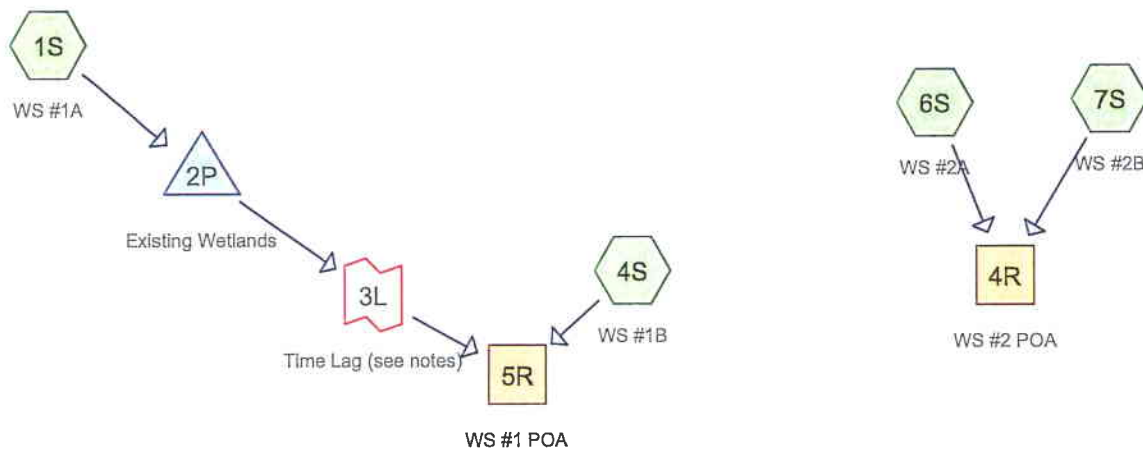
Qp: 0.87

Hydrologic Soil Group—Tompkins County, New York (Hamilton Square)



Hydrologic Soil Group

Hydrologic Soil Group— Summary by Map Unit — Tompkins County, New York (NY109)				
Map unit symbol	Map unit name	Rating	Acres In AOI	Percent of AOI
HdC	Howard gravelly loam, 5 to 15 percent simple slopes	A	7.5	33.7%
LbB	Lansing gravelly silt loam, 3 to 8 percent slopes	B	1.7	7.6%
OaA	Ovid silt loam, 0 to 6 percent slopes	C/D	3.1	13.7%
RkA	Rhinebeck silt loam, 0 to 2 percent slopes	C/D	10.1	45.0%
Totals for Area of Interest			22.4	100.0%



Existing Condition Summaries

Routing Diagram for Existing

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Existing

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Existing Conditions Summaries
Type II 24-hr 1-yr Rainfall=1.96"

Printed 3/15/2018

Page 2

Summary for Subcatchment 1S: WS #1A

Runoff = 3.52 cfs @ 12.17 hrs, Volume= 0.296 af, Depth> 0.31"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
Type II 24-hr 1-yr Rainfall=1.96"

Area (ac)	CN	Description
1.120	98	Paved parking, HSG D
0.580	30	Woods, Good, HSG A
2.000	77	Woods, Good, HSG D
0.490	78	Meadow, non-grazed, HSG D
1.100	39	>75% Grass cover, Good, HSG A
6.020	80	>75% Grass cover, Good, HSG D
11.310	75	Weighted Average
10.190		90.10% Pervious Area
1.120		9.90% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
0.5	18	0.0100	0.63		Sheet Flow, Smooth surfaces n= 0.011 P2= 2.31"
13.0	82	0.0100	0.11		Sheet Flow, Grass: Short n= 0.150 P2= 2.31"
1.9	171	0.0090	1.53		Shallow Concentrated Flow, Unpaved Kv= 16.1 fps
4.9	140	0.0090	0.47		Shallow Concentrated Flow, Woodland Kv= 5.0 fps
20.3	411	Total			

Summary for Subcatchment 4S: WS #1B

Runoff = 0.87 cfs @ 12.32 hrs, Volume= 0.154 af, Depth> 0.13"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
Type II 24-hr 1-yr Rainfall=1.96"

Area (ac)	CN	Description
0.100	98	Paved parking, HSG D
1.210	30	Woods, Good, HSG A
0.790	77	Woods, Good, HSG D
8.460	78	Meadow, non-grazed, HSG D
1.710	30	Meadow, non-grazed, HSG A
0.850	58	Meadow, non-grazed, HSG B
1.030	80	>75% Grass cover, Good, HSG D
14.150	67	Weighted Average
14.050		99.29% Pervious Area
0.100		0.71% Impervious Area

Existing

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Existing Conditions Summaries
Type II 24-hr 1-yr Rainfall=1.96"

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Page 4

Summary for Subcatchment 7S: WS #2B

Runoff = 0.07 cfs @ 12.51 hrs, Volume= 0.024 af, Depth> 0.06"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
Type II 24-hr 1-yr Rainfall=1.96"

Area (ac)	CN	Description
0.830	98	Paved parking, HSG D
0.100	30	Woods, Good, HSG A
0.580	30	Meadow, non-grazed, HSG A
0.140	58	Meadow, non-grazed, HSG B
0.300	39	>75% Grass cover, Good, HSG A
2.920	61	>75% Grass cover, Good, HSG B
4.870	62	Weighted Average
4.040		82.96% Pervious Area
0.830		17.04% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
9.8	100	0.0300	0.17		Sheet Flow, Grass: Short n= 0.150 P2= 2.31"
1.3	180	0.0210	2.33		Shallow Concentrated Flow, Unpaved Kv= 16.1 fps
1.7	206	0.0100	2.03		Shallow Concentrated Flow, Paved Kv= 20.3 fps
2.5	470	0.0100	3.09	5.46	Pipe Channel, 18.0" Round Area= 1.8 sf Perim= 4.7' r= 0.38' n= 0.025 Corrugated metal
15.3	956	Total			

Summary for Reach 4R: WS #2 POA

Inflow Area = 7.460 ac, 13.14% Impervious, Inflow Depth > 0.04" for 1-yr event

Inflow = 0.07 cfs @ 12.51 hrs, Volume= 0.024 af

Outflow = 0.07 cfs @ 12.51 hrs, Volume= 0.024 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Summary for Reach 5R: WS #1 POA

Inflow Area = 25.460 ac, 4.79% Impervious, Inflow Depth > 0.18" for 1-yr event

Inflow = 2.13 cfs @ 12.92 hrs, Volume= 0.381 af

Outflow = 2.13 cfs @ 12.92 hrs, Volume= 0.381 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Existing

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Existing Conditions Summaries
Type II 24-hr 10-yr Rainfall=3.36"

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Page 6

Summary for Subcatchment 1S: WS #1A

Runoff = 14.41 cfs @ 12.14 hrs, Volume= 1.022 af, Depth> 1.08"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
Type II 24-hr 10-yr Rainfall=3.36"

Area (ac)	CN	Description
1.120	98	Paved parking, HSG D
0.580	30	Woods, Good, HSG A
2.000	77	Woods, Good, HSG D
0.490	78	Meadow, non-grazed, HSG D
1.100	39	>75% Grass cover, Good, HSG A
6.020	80	>75% Grass cover, Good, HSG D
11.310	75	Weighted Average
10.190		90.10% Pervious Area
1.120		9.90% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
0.5	18	0.0100	0.63		Sheet Flow, Smooth surfaces n= 0.011 P2= 2.31"
13.0	82	0.0100	0.11		Sheet Flow, Grass: Short n= 0.150 P2= 2.31"
1.9	171	0.0090	1.53		Shallow Concentrated Flow, Unpaved Kv= 16.1 fps
4.9	140	0.0090	0.47		Shallow Concentrated Flow, Woodland Kv= 5.0 fps
20.3	411	Total			

Summary for Subcatchment 4S: WS #1B

Runoff = 8.86 cfs @ 12.22 hrs, Volume= 0.799 af, Depth> 0.68"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
Type II 24-hr 10-yr Rainfall=3.36"

Area (ac)	CN	Description
0.100	98	Paved parking, HSG D
1.210	30	Woods, Good, HSG A
0.790	77	Woods, Good, HSG D
8.460	78	Meadow, non-grazed, HSG D
1.710	30	Meadow, non-grazed, HSG A
0.850	58	Meadow, non-grazed, HSG B
1.030	80	>75% Grass cover, Good, HSG D
14.150	67	Weighted Average
14.050		99.29% Pervious Area
0.100		0.71% Impervious Area

Existing

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Existing Conditions Summaries
Type II 24-hr 10-yr Rainfall=3.36"

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Page 8

Summary for Subcatchment 7S: WS #2B**Runoff = 2.61 cfs @ 12.11 hrs, Volume= 0.193 af, Depth> 0.48"**Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
Type II 24-hr 10-yr Rainfall=3.36"

Area (ac)	CN	Description
0.830	98	Paved parking, HSG D
0.100	30	Woods, Good, HSG A
0.580	30	Meadow, non-grazed, HSG A
0.140	58	Meadow, non-grazed, HSG B
0.300	39	>75% Grass cover, Good, HSG A
2.920	61	>75% Grass cover, Good, HSG B
4.870	62	Weighted Average
4.040		82.96% Pervious Area
0.830		17.04% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
9.8	100	0.0300	0.17		Sheet Flow, Grass: Short n= 0.150 P2= 2.31"
1.3	180	0.0210	2.33		Shallow Concentrated Flow, Unpaved Kv= 16.1 fps
1.7	206	0.0100	2.03		Shallow Concentrated Flow, Paved Kv= 20.3 fps
2.5	470	0.0100	3.09	5.46	Pipe Channel, 18.0" Round Area= 1.8 sf Perim= 4.7' r= 0.38' n= 0.025 Corrugated metal
15.3	956	Total			

Summary for Reach 4R: WS #2 POA

Inflow Area = 7.460 ac, 13.14% Impervious, Inflow Depth > 0.31" for 10-yr event
 Inflow = 2.61 cfs @ 12.11 hrs, Volume= 0.193 af
Outflow = 2.61 cfs @ 12.11 hrs, Volume= 0.193 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Summary for Reach 5R: WS #1 POA

Inflow Area = 25.460 ac, 4.79% Impervious, Inflow Depth > 0.82" for 10-yr event
 Inflow = 16.79 cfs @ 12.67 hrs, Volume= 1.738 af
Outflow = 16.79 cfs @ 12.67 hrs, Volume= 1.738 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

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Existing Conditions Summaries
Type II 24-hr 100-yr Rainfall=5.73"

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Summary for Subcatchment 1S: WS #1A

Runoff = 37.85 cfs @ 12.13 hrs, Volume= 2.643 af, Depth> 2.80"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
Type II 24-hr 100-yr Rainfall=5.73"

Area (ac)	CN	Description
1.120	98	Paved parking, HSG D
0.580	30	Woods, Good, HSG A
2.000	77	Woods, Good, HSG D
0.490	78	Meadow, non-grazed, HSG D
1.100	39	>75% Grass cover, Good, HSG A
6.020	80	>75% Grass cover, Good, HSG D
11.310	75	Weighted Average
10.190		90.10% Pervious Area
1.120		9.90% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
0.5	18	0.0100	0.63		Sheet Flow, Smooth surfaces n= 0.011 P2= 2.31"
13.0	82	0.0100	0.11		Sheet Flow, Grass: Short n= 0.150 P2= 2.31"
1.9	171	0.0090	1.53		Shallow Concentrated Flow, Unpaved Kv= 16.1 fps
4.9	140	0.0090	0.47		Shallow Concentrated Flow, Woodland Kv= 5.0 fps
20.3	411	Total			

Summary for Subcatchment 4S: WS #1B

Runoff = 30.82 cfs @ 12.20 hrs, Volume= 2.483 af, Depth> 2.11"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
Type II 24-hr 100-yr Rainfall=5.73"

Area (ac)	CN	Description
0.100	98	Paved parking, HSG D
1.210	30	Woods, Good, HSG A
0.790	77	Woods, Good, HSG D
8.460	78	Meadow, non-grazed, HSG D
1.710	30	Meadow, non-grazed, HSG A
0.850	58	Meadow, non-grazed, HSG B
1.030	80	>75% Grass cover, Good, HSG D
14.150	67	Weighted Average
14.050		99.29% Pervious Area
0.100		0.71% Impervious Area

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Existing Conditions Summaries
Type II 24-hr 100-yr Rainfall=5.73"

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Summary for Subcatchment 7S: WS #2B

Runoff = 11.39 cfs @ 12.09 hrs, Volume= 0.697 af, Depth> 1.72"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
Type II 24-hr 100-yr Rainfall=5.73"

Area (ac)	CN	Description
0.830	98	Paved parking, HSG D
0.100	30	Woods, Good, HSG A
0.580	30	Meadow, non-grazed, HSG A
0.140	58	Meadow, non-grazed, HSG B
0.300	39	>75% Grass cover, Good, HSG A
2.920	61	>75% Grass cover, Good, HSG B
4.870	62	Weighted Average
4.040		82.96% Pervious Area
0.830		17.04% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
9.8	100	0.0300	0.17		Sheet Flow, Grass: Short n= 0.150 P2= 2.31"
1.3	180	0.0210	2.33		Shallow Concentrated Flow, Unpaved Kv= 16.1 fps
1.7	206	0.0100	2.03		Shallow Concentrated Flow, Paved Kv= 20.3 fps
2.5	470	0.0100	3.09	5.46	Pipe Channel, 18.0" Round Area= 1.8 sf Perim= 4.7' r= 0.38' n= 0.025 Corrugated metal
15.3	956	Total			

Summary for Reach 4R: WS #2 POA

Inflow Area = 7.460 ac, 13.14% Impervious, Inflow Depth > 1.22" for 100-yr event

Inflow = 11.43 cfs @ 12.09 hrs, Volume= 0.760 af

Outflow = 11.43 cfs @ 12.09 hrs, Volume= 0.760 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

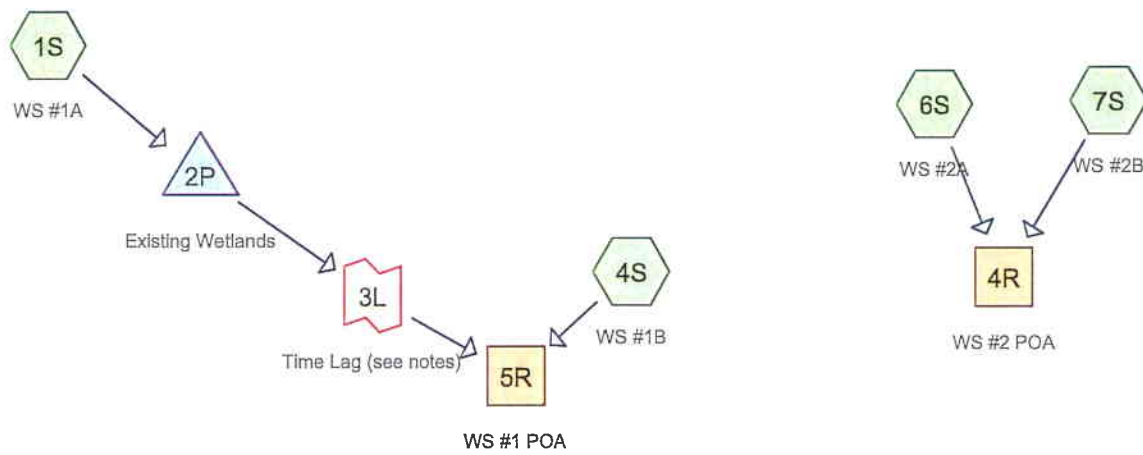
Summary for Reach 5R: WS #1 POA

Inflow Area = 25.460 ac, 4.79% Impervious, Inflow Depth > 2.37" for 100-yr event

Inflow = 46.33 cfs @ 12.64 hrs, Volume= 5.022 af

Outflow = 46.33 cfs @ 12.64 hrs, Volume= 5.022 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs



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Type II 24-hr 1-yr Rainfall=1.96"

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Summary for Subcatchment 1S: WS #1A

Runoff = 3.52 cfs @ 12.17 hrs, Volume= 0.296 af, Depth> 0.31"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
Type II 24-hr 1-yr Rainfall=1.96"

Area (ac)	CN	Description
1.120	98	Paved parking, HSG D
0.580	30	Woods, Good, HSG A
2.000	77	Woods, Good, HSG D
0.490	78	Meadow, non-grazed, HSG D
1.100	39	>75% Grass cover, Good, HSG A
6.020	80	>75% Grass cover, Good, HSG D
11.310	75	Weighted Average
10.190		90.10% Pervious Area
1.120		9.90% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
0.5	18	0.0100	0.63		Sheet Flow, Smooth surfaces n= 0.011 P2= 2.31"
13.0	82	0.0100	0.11		Sheet Flow, Grass: Short n= 0.150 P2= 2.31"
1.9	171	0.0090	1.53		Shallow Concentrated Flow, Unpaved Kv= 16.1 fps
4.9	140	0.0090	0.47		Shallow Concentrated Flow, Woodland Kv= 5.0 fps
20.3	411	Total			

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Type II 24-hr 1-yr Rainfall=1.96"

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Summary for Subcatchment 4S: WS #1B

Runoff = 0.87 cfs @ 12.32 hrs, Volume= 0.154 af, Depth> 0.13"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
Type II 24-hr 1-yr Rainfall=1.96"

Area (ac)	CN	Description
0.100	98	Paved parking, HSG D
1.210	30	Woods, Good, HSG A
0.790	77	Woods, Good, HSG D
8.460	78	Meadow, non-grazed, HSG D
1.710	30	Meadow, non-grazed, HSG A
0.850	58	Meadow, non-grazed, HSG B
1.030	80	>75% Grass cover, Good, HSG D
14.150	67	Weighted Average
14.050		99.29% Pervious Area
0.100		0.71% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
0.4	14	0.0100	0.60		Sheet Flow, Smooth surfaces n= 0.011 P2= 2.31"
9.3	86	0.0250	0.15		Sheet Flow, Grass: Short n= 0.150 P2= 2.31"
1.7	218	0.0180	2.16		Shallow Concentrated Flow, Unpaved Kv= 16.1 fps
1.9	77	0.0180	0.67		Shallow Concentrated Flow, Woodland Kv= 5.0 fps
6.2	539	0.0080	1.44		Shallow Concentrated Flow, Unpaved Kv= 16.1 fps
6.0	452	0.0060	1.25		Shallow Concentrated Flow, Unpaved Kv= 16.1 fps
25.5	1,386	Total			

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Type II 24-hr 1-yr Rainfall=1.96"

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Summary for Subcatchment 6S: WS #2A

[45] Hint: Runoff=Zero

Runoff = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af, Depth= 0.00"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
Type II 24-hr 1-yr Rainfall=1.96"

Area (ac)	CN	Description
0.150	98	Paved parking, HSG D
1.220	30	Woods, Good, HSG A
1.100	39	>75% Grass cover, Good, HSG A
0.120	61	>75% Grass cover, Good, HSG B
2.590	39	Weighted Average
2.440		94.21% Pervious Area
0.150		5.79% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
10.5	43	0.0120	0.07		Sheet Flow, Grass: Dense n= 0.240 P2= 2.31"
11.8	57	0.0440	0.08		Sheet Flow, Woods: Light underbrush n= 0.400 P2= 2.31"
2.0	151	0.0660	1.28		Shallow Concentrated Flow, Woodland Kv= 5.0 fps
0.1	32	0.0660	4.14		Shallow Concentrated Flow, Unpaved Kv= 16.1 fps
0.8	60	0.0660	1.28		Shallow Concentrated Flow, Woodland Kv= 5.0 fps
4.0	188	0.0240	0.77		Shallow Concentrated Flow, Woodland Kv= 5.0 fps
29.2	531	Total			

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Type II 24-hr 1-yr Rainfall=1.96"

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Summary for Subcatchment 7S: WS #2B

Runoff = 0.07 cfs @ 12.51 hrs, Volume= 0.024 af, Depth> 0.06"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
Type II 24-hr 1-yr Rainfall=1.96"

Area (ac)	CN	Description
0.830	98	Paved parking, HSG D
0.100	30	Woods, Good, HSG A
0.580	30	Meadow, non-grazed, HSG A
0.140	58	Meadow, non-grazed, HSG B
0.300	39	>75% Grass cover, Good, HSG A
2.920	61	>75% Grass cover, Good, HSG B
4.870	62	Weighted Average
4.040		82.96% Pervious Area
0.830		17.04% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
9.8	100	0.0300	0.17		Sheet Flow, Grass: Short n= 0.150 P2= 2.31"
1.3	180	0.0210	2.33		Shallow Concentrated Flow, Unpaved Kv= 16.1 fps
1.7	206	0.0100	2.03		Shallow Concentrated Flow, Paved Kv= 20.3 fps
2.5	470	0.0100	3.09	5.46	Pipe Channel, 18.0" Round Area= 1.8 sf Perim= 4.7' r= 0.38' n= 0.025 Corrugated metal
15.3	956	Total			

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Type II 24-hr 1-yr Rainfall=1.96"

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Summary for Reach 4R: WS #2 POA

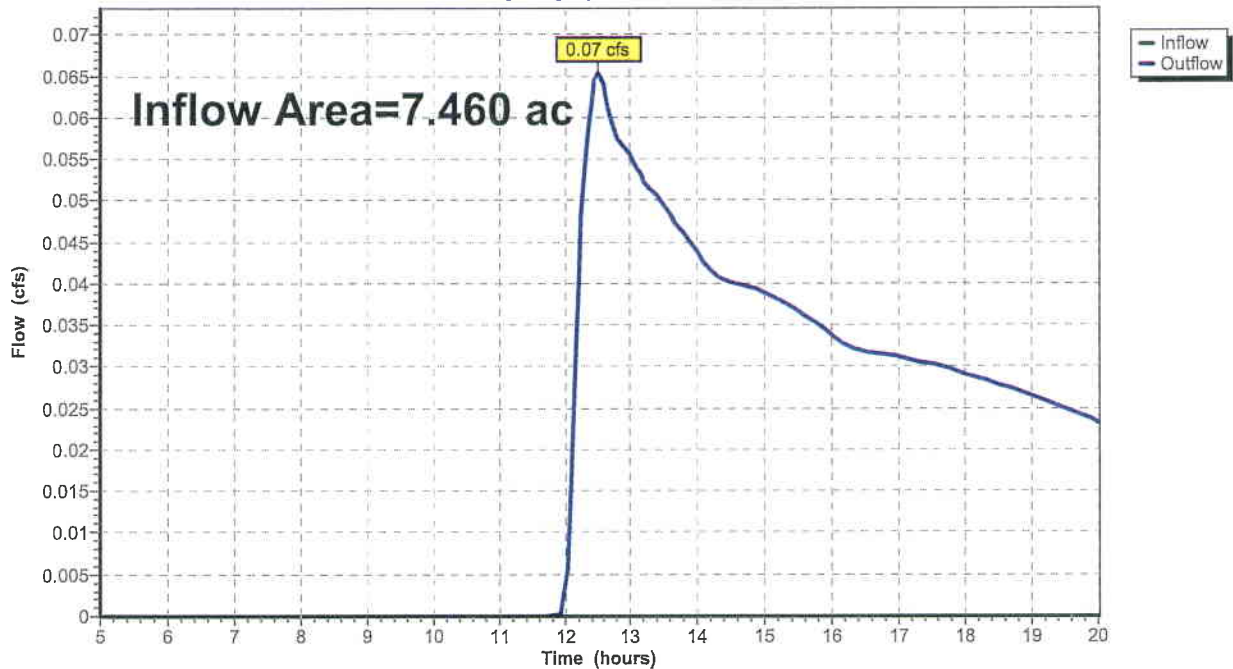
[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 7.460 ac, 13.14% Impervious, Inflow Depth > 0.04" for 1-yr event
Inflow = 0.07 cfs @ 12.51 hrs, Volume= 0.024 af
Outflow = 0.07 cfs @ 12.51 hrs, Volume= 0.024 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Reach 4R: WS #2 POA

Hydrograph



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Type II 24-hr 1-yr Rainfall=1.96"

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Summary for Pond 2P: Existing Wetlands

Inflow Area = 11.310 ac, 9.90% Impervious, Inflow Depth > 0.31" for 1-yr event
 Inflow = 3.52 cfs @ 12.17 hrs, Volume= 0.296 af
 Outflow = 1.69 cfs @ 12.43 hrs, Volume= 0.233 af, Atten= 52%, Lag= 15.7 min
 Primary = 1.69 cfs @ 12.43 hrs, Volume= 0.233 af

Routing by Dyn-Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
 Peak Elev= 992.53' @ 12.43 hrs Surf.Area= 13,368 sf Storage= 3,552 cf

Plug-Flow detention time= 99.1 min calculated for 0.232 af (79% of inflow)
 Center-of-Mass det. time= 39.1 min (882.5 - 843.5)

Volume	Invert	Avail.Storage	Storage Description
#1	991.90'	14,723 cf	Custom Stage Data (Prismatic) Listed below (Recalc)

Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
991.90	0	0	0
992.00	539	27	27
992.50	12,019	3,140	3,166
993.00	34,207	11,557	14,723

Device	Routing	Invert	Outlet Devices
#1	Primary	992.42'	Asymmetrical Weir, C= 3.27 Offset (feet) -82.00 -58.00 0.00 51.00 Height (feet) 0.58 0.25 0.00 0.58

Primary OutFlow Max=1.68 cfs @ 12.43 hrs HW=992.53' TW=0.00' (Dynamic Tailwater)

↑1=Asymmetrical Weir (Weir Controls 1.68 cfs @ 0.43 fps)

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Type II 24-hr 1-yr Rainfall=1.96"

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Stage-Discharge for Pond 2P: Existing Wetlands

Elevation (feet)	Primary (cfs)	Elevation (feet)	Primary (cfs)	Elevation (feet)	Primary (cfs)
991.90	0.00	992.43	0.00	992.96	80.24
991.91	0.00	992.44	0.02	992.97	83.61
991.92	0.00	992.45	0.07	992.98	87.06
991.93	0.00	992.46	0.13	992.99	90.58
991.94	0.00	992.47	0.23	993.00	94.18
991.95	0.00	992.48	0.37		
991.96	0.00	992.49	0.54		
991.97	0.00	992.50	0.76		
991.98	0.00	992.51	1.02		
991.99	0.00	992.52	1.32		
992.00	0.00	992.53	1.68		
992.01	0.00	992.54	2.09		
992.02	0.00	992.55	2.55		
992.03	0.00	992.56	3.07		
992.04	0.00	992.57	3.65		
992.05	0.00	992.58	4.29		
992.06	0.00	992.59	4.99		
992.07	0.00	992.60	5.75		
992.08	0.00	992.61	6.58		
992.09	0.00	992.62	7.49		
992.10	0.00	992.63	8.46		
992.11	0.00	992.64	9.50		
992.12	0.00	992.65	10.62		
992.13	0.00	992.66	11.81		
992.14	0.00	992.67	13.08		
992.15	0.00	992.68	14.42		
992.16	0.00	992.69	15.84		
992.17	0.00	992.70	17.33		
992.18	0.00	992.71	18.89		
992.19	0.00	992.72	20.51		
992.20	0.00	992.73	22.21		
992.21	0.00	992.74	23.97		
992.22	0.00	992.75	25.80		
992.23	0.00	992.76	27.70		
992.24	0.00	992.77	29.67		
992.25	0.00	992.78	31.70		
992.26	0.00	992.79	33.81		
992.27	0.00	992.80	35.98		
992.28	0.00	992.81	38.22		
992.29	0.00	992.82	40.53		
992.30	0.00	992.83	42.91		
992.31	0.00	992.84	45.36		
992.32	0.00	992.85	47.87		
992.33	0.00	992.86	50.46		
992.34	0.00	992.87	53.12		
992.35	0.00	992.88	55.85		
992.36	0.00	992.89	58.64		
992.37	0.00	992.90	61.51		
992.38	0.00	992.91	64.45		
992.39	0.00	992.92	67.47		
992.40	0.00	992.93	70.55		
992.41	0.00	992.94	73.71		
992.42	0.00	992.95	76.93		

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Type II 24-hr 10-yr Rainfall=3.36"

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Summary for Subcatchment 1S: WS #1A

Runoff = 14.41 cfs @ 12.14 hrs, Volume= 1.022 af, Depth> 1.08"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
Type II 24-hr 10-yr Rainfall=3.36"

Area (ac)	CN	Description
1.120	98	Paved parking, HSG D
0.580	30	Woods, Good, HSG A
2.000	77	Woods, Good, HSG D
0.490	78	Meadow, non-grazed, HSG D
1.100	39	>75% Grass cover, Good, HSG A
6.020	80	>75% Grass cover, Good, HSG D
11.310	75	Weighted Average
10.190		90.10% Pervious Area
1.120		9.90% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
0.5	18	0.0100	0.63		Sheet Flow, Smooth surfaces n= 0.011 P2= 2.31"
13.0	82	0.0100	0.11		Sheet Flow, Grass: Short n= 0.150 P2= 2.31"
1.9	171	0.0090	1.53		Shallow Concentrated Flow, Unpaved Kv= 16.1 fps
4.9	140	0.0090	0.47		Shallow Concentrated Flow, Woodland Kv= 5.0 fps
20.3	411	Total			

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Type II 24-hr 10-yr Rainfall=3.36"

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Summary for Subcatchment 4S: WS #1B

Runoff = 8.86 cfs @ 12.22 hrs, Volume= 0.799 af, Depth> 0.68"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
Type II 24-hr 10-yr Rainfall=3.36"

Area (ac)	CN	Description
0.100	98	Paved parking, HSG D
1.210	30	Woods, Good, HSG A
0.790	77	Woods, Good, HSG D
8.460	78	Meadow, non-grazed, HSG D
1.710	30	Meadow, non-grazed, HSG A
0.850	58	Meadow, non-grazed, HSG B
1.030	80	>75% Grass cover, Good, HSG D
14.150	67	Weighted Average
14.050		99.29% Pervious Area
0.100		0.71% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
0.4	14	0.0100	0.60		Sheet Flow, Smooth surfaces n= 0.011 P2= 2.31"
9.3	86	0.0250	0.15		Sheet Flow, Grass: Short n= 0.150 P2= 2.31"
1.7	218	0.0180	2.16		Shallow Concentrated Flow, Unpaved Kv= 16.1 fps
1.9	77	0.0180	0.67		Shallow Concentrated Flow, Woodland Kv= 5.0 fps
6.2	539	0.0080	1.44		Shallow Concentrated Flow, Unpaved Kv= 16.1 fps
6.0	452	0.0060	1.25		Shallow Concentrated Flow, Unpaved Kv= 16.1 fps
25.5	1,386	Total			

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Type II 24-hr 10-yr Rainfall=3.36"

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Summary for Subcatchment 6S: WS #2A

[73] Warning: Peak may fall outside time span

Runoff = 0.00 cfs @ 20.00 hrs, Volume= 0.000 af, Depth> 0.00"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
Type II 24-hr 10-yr Rainfall=3.36"

Area (ac)	CN	Description
0.150	98	Paved parking, HSG D
1.220	30	Woods, Good, HSG A
1.100	39	>75% Grass cover, Good, HSG A
0.120	61	>75% Grass cover, Good, HSG B
2.590	39	Weighted Average
2.440		94.21% Pervious Area
0.150		5.79% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
10.5	43	0.0120	0.07		Sheet Flow, Grass: Dense n= 0.240 P2= 2.31"
11.8	57	0.0440	0.08		Sheet Flow, Woods: Light underbrush n= 0.400 P2= 2.31"
2.0	151	0.0660	1.28		Shallow Concentrated Flow, Woodland Kv= 5.0 fps
0.1	32	0.0660	4.14		Shallow Concentrated Flow, Unpaved Kv= 16.1 fps
0.8	60	0.0660	1.28		Shallow Concentrated Flow, Woodland Kv= 5.0 fps
4.0	188	0.0240	0.77		Shallow Concentrated Flow, Woodland Kv= 5.0 fps
29.2	531	Total			

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Type II 24-hr 10-yr Rainfall=3.36"

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Summary for Subcatchment 7S: WS #2B

Runoff = 2.61 cfs @ 12.11 hrs, Volume= 0.193 af, Depth> 0.48"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
Type II 24-hr 10-yr Rainfall=3.36"

Area (ac)	CN	Description
0.830	98	Paved parking, HSG D
0.100	30	Woods, Good, HSG A
0.580	30	Meadow, non-grazed, HSG A
0.140	58	Meadow, non-grazed, HSG B
0.300	39	>75% Grass cover, Good, HSG A
2.920	61	>75% Grass cover, Good, HSG B
4.870	62	Weighted Average
4.040		82.96% Pervious Area
0.830		17.04% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
9.8	100	0.0300	0.17		Sheet Flow, Grass: Short n= 0.150 P2= 2.31"
1.3	180	0.0210	2.33		Shallow Concentrated Flow, Unpaved Kv= 16.1 fps
1.7	206	0.0100	2.03		Shallow Concentrated Flow, Paved Kv= 20.3 fps
2.5	470	0.0100	3.09	5.46	Pipe Channel, 18.0" Round Area= 1.8 sf Perim= 4.7' r= 0.38' n= 0.025 Corrugated metal
15.3	956	Total			

Existing

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Type II 24-hr 10-yr Rainfall=3.36"

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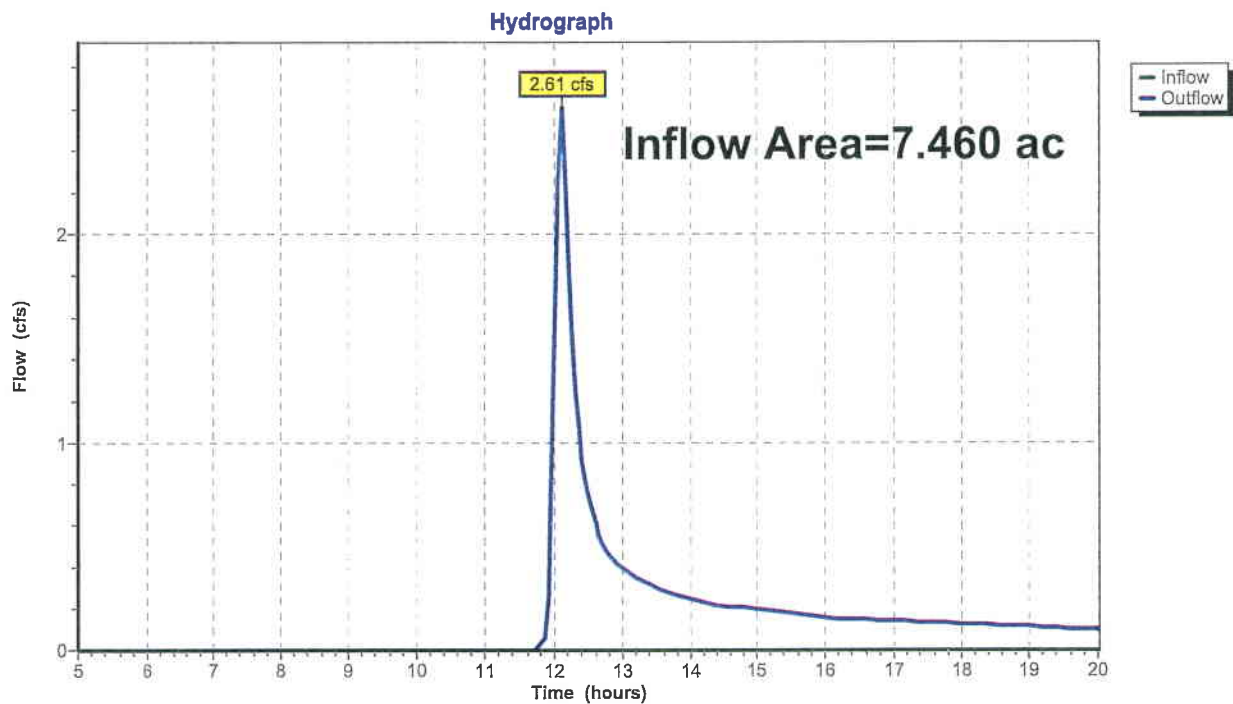
Summary for Reach 4R: WS #2 POA

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 7.460 ac, 13.14% Impervious, Inflow Depth > 0.31" for 10-yr event
Inflow = 2.61 cfs @ 12.11 hrs, Volume= 0.193 af
Outflow = 2.61 cfs @ 12.11 hrs, Volume= 0.193 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Reach 4R: WS #2 POA



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Type II 24-hr 10-yr Rainfall=3.36"

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Summary for Pond 2P: Existing Wetlands

Inflow Area = 11.310 ac, 9.90% Impervious, Inflow Depth > 1.08" for 10-yr event
 Inflow = 14.41 cfs @ 12.14 hrs, Volume= 1.022 af
 Outflow = 13.76 cfs @ 12.19 hrs, Volume= 0.955 af, Atten= 5%, Lag= 2.9 min
 Primary = 13.76 cfs @ 12.19 hrs, Volume= 0.955 af

Routing by Dyn-Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
 Peak Elev= 992.68' @ 12.19 hrs Surf.Area= 19,790 sf Storage= 5,952 cf

Plug-Flow detention time= 34.7 min calculated for 0.951 af (93% of inflow)
 Center-of-Mass det. time= 12.2 min (827.2 - 815.0)

Volume	Invert	Avail.Storage	Storage Description
#1	991.90'	14,723 cf	Custom Stage Data (Prismatic) Listed below (Recalc)

Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
991.90	0	0	0
992.00	539	27	27
992.50	12,019	3,140	3,166
993.00	34,207	11,557	14,723

Device	Routing	Invert	Outlet Devices
#1	Primary	992.42'	Asymmetrical Weir, C= 3.27 Offset (feet) -82.00 -58.00 0.00 51.00 Height (feet) 0.58 0.25 0.00 0.58

Primary OutFlow Max=13.65 cfs @ 12.19 hrs HW=992.67' TW=0.00' (Dynamic Tailwater)

↑1=Asymmetrical Weir (Weir Controls 13.65 cfs @ 0.67 fps)

Existing

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Type II 24-hr 10-yr Rainfall=3.36"

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Stage-Discharge for Pond 2P: Existing Wetlands

Elevation (feet)	Primary (cfs)	Elevation (feet)	Primary (cfs)	Elevation (feet)	Primary (cfs)
991.90	0.00	992.43	0.00	992.96	80.24
991.91	0.00	992.44	0.02	992.97	83.61
991.92	0.00	992.45	0.07	992.98	87.06
991.93	0.00	992.46	0.13	992.99	90.58
991.94	0.00	992.47	0.23	993.00	94.18
991.95	0.00	992.48	0.37		
991.96	0.00	992.49	0.54		
991.97	0.00	992.50	0.76		
991.98	0.00	992.51	1.02		
991.99	0.00	992.52	1.32		
992.00	0.00	992.53	1.68		
992.01	0.00	992.54	2.09		
992.02	0.00	992.55	2.55		
992.03	0.00	992.56	3.07		
992.04	0.00	992.57	3.65		
992.05	0.00	992.58	4.29		
992.06	0.00	992.59	4.99		
992.07	0.00	992.60	5.75		
992.08	0.00	992.61	6.58		
992.09	0.00	992.62	7.49		
992.10	0.00	992.63	8.46		
992.11	0.00	992.64	9.50		
992.12	0.00	992.65	10.62		
992.13	0.00	992.66	11.81		
992.14	0.00	992.67	13.08		
992.15	0.00	992.68	14.42		
992.16	0.00	992.69	15.84		
992.17	0.00	992.70	17.33		
992.18	0.00	992.71	18.89		
992.19	0.00	992.72	20.51		
992.20	0.00	992.73	22.21		
992.21	0.00	992.74	23.97		
992.22	0.00	992.75	25.80		
992.23	0.00	992.76	27.70		
992.24	0.00	992.77	29.67		
992.25	0.00	992.78	31.70		
992.26	0.00	992.79	33.81		
992.27	0.00	992.80	35.98		
992.28	0.00	992.81	38.22		
992.29	0.00	992.82	40.53		
992.30	0.00	992.83	42.91		
992.31	0.00	992.84	45.36		
992.32	0.00	992.85	47.87		
992.33	0.00	992.86	50.46		
992.34	0.00	992.87	53.12		
992.35	0.00	992.88	55.85		
992.36	0.00	992.89	58.64		
992.37	0.00	992.90	61.51		
992.38	0.00	992.91	64.45		
992.39	0.00	992.92	67.47		
992.40	0.00	992.93	70.55		
992.41	0.00	992.94	73.71		
992.42	0.00	992.95	76.93		

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Type II 24-hr 100-yr Rainfall=5.73"

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Summary for Subcatchment 1S: WS #1A

Runoff = 37.85 cfs @ 12.13 hrs, Volume= 2.643 af, Depth> 2.80"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
Type II 24-hr 100-yr Rainfall=5.73"

Area (ac)	CN	Description
1.120	98	Paved parking, HSG D
0.580	30	Woods, Good, HSG A
2.000	77	Woods, Good, HSG D
0.490	78	Meadow, non-grazed, HSG D
1.100	39	>75% Grass cover, Good, HSG A
6.020	80	>75% Grass cover, Good, HSG D
11.310	75	Weighted Average
10.190		90.10% Pervious Area
1.120		9.90% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
0.5	18	0.0100	0.63		Sheet Flow, Smooth surfaces n= 0.011 P2= 2.31"
13.0	82	0.0100	0.11		Sheet Flow, Grass: Short n= 0.150 P2= 2.31"
1.9	171	0.0090	1.53		Shallow Concentrated Flow, Unpaved Kv= 16.1 fps
4.9	140	0.0090	0.47		Shallow Concentrated Flow, Woodland Kv= 5.0 fps
20.3	411	Total			

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Type II 24-hr 100-yr Rainfall=5.73"

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Summary for Subcatchment 4S: WS #1B

Runoff = 30.82 cfs @ 12.20 hrs, Volume= 2.483 af, Depth> 2.11"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
Type II 24-hr 100-yr Rainfall=5.73"

Area (ac)	CN	Description
0.100	98	Paved parking, HSG D
1.210	30	Woods, Good, HSG A
0.790	77	Woods, Good, HSG D
8.460	78	Meadow, non-grazed, HSG D
1.710	30	Meadow, non-grazed, HSG A
0.850	58	Meadow, non-grazed, HSG B
1.030	80	>75% Grass cover, Good, HSG D
14.150	67	Weighted Average
14.050		99.29% Pervious Area
0.100		0.71% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
0.4	14	0.0100	0.60		Sheet Flow, Smooth surfaces n= 0.011 P2= 2.31"
9.3	86	0.0250	0.15		Sheet Flow, Grass: Short n= 0.150 P2= 2.31"
1.7	218	0.0180	2.16		Shallow Concentrated Flow, Unpaved Kv= 16.1 fps
1.9	77	0.0180	0.67		Shallow Concentrated Flow, Woodland Kv= 5.0 fps
6.2	539	0.0080	1.44		Shallow Concentrated Flow, Unpaved Kv= 16.1 fps
6.0	452	0.0060	1.25		Shallow Concentrated Flow, Unpaved Kv= 16.1 fps
25.5	1,386	Total			

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Type II 24-hr 100-yr Rainfall=5.73"

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Summary for Subcatchment 6S: WS #2A

Runoff = 0.26 cfs @ 12.44 hrs, Volume= 0.063 af, Depth> 0.29"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
Type II 24-hr 100-yr Rainfall=5.73"

Area (ac)	CN	Description
0.150	98	Paved parking, HSG D
1.220	30	Woods, Good, HSG A
1.100	39	>75% Grass cover, Good, HSG A
0.120	61	>75% Grass cover, Good, HSG B
2.590	39	Weighted Average
2.440		94.21% Pervious Area
0.150		5.79% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
10.5	43	0.0120	0.07		Sheet Flow, Grass: Dense n= 0.240 P2= 2.31"
11.8	57	0.0440	0.08		Sheet Flow, Woods: Light underbrush n= 0.400 P2= 2.31"
2.0	151	0.0660	1.28		Shallow Concentrated Flow, Woodland Kv= 5.0 fps
0.1	32	0.0660	4.14		Shallow Concentrated Flow, Unpaved Kv= 16.1 fps
0.8	60	0.0660	1.28		Shallow Concentrated Flow, Woodland Kv= 5.0 fps
4.0	188	0.0240	0.77		Shallow Concentrated Flow, Woodland Kv= 5.0 fps
29.2	531	Total			

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Type II 24-hr 100-yr Rainfall=5.73"

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Summary for Subcatchment 7S: WS #2B

Runoff = 11.39 cfs @ 12.09 hrs, Volume= 0.697 af, Depth> 1.72"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
Type II 24-hr 100-yr Rainfall=5.73"

Area (ac)	CN	Description
0.830	98	Paved parking, HSG D
0.100	30	Woods, Good, HSG A
0.580	30	Meadow, non-grazed, HSG A
0.140	58	Meadow, non-grazed, HSG B
0.300	39	>75% Grass cover, Good, HSG A
2.920	61	>75% Grass cover, Good, HSG B
4.870	62	Weighted Average
4.040		82.96% Pervious Area
0.830		17.04% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
9.8	100	0.0300	0.17		Sheet Flow, Grass: Short n= 0.150 P2= 2.31"
1.3	180	0.0210	2.33		Shallow Concentrated Flow, Unpaved Kv= 16.1 fps
1.7	206	0.0100	2.03		Shallow Concentrated Flow, Paved Kv= 20.3 fps
2.5	470	0.0100	3.09	5.46	Pipe Channel, 18.0" Round Area= 1.8 sf Perim= 4.7' r= 0.38' n= 0.025 Corrugated metal
15.3	956	Total			

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Type II 24-hr 100-yr Rainfall=5.73"

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Summary for Reach 4R: WS #2 POA

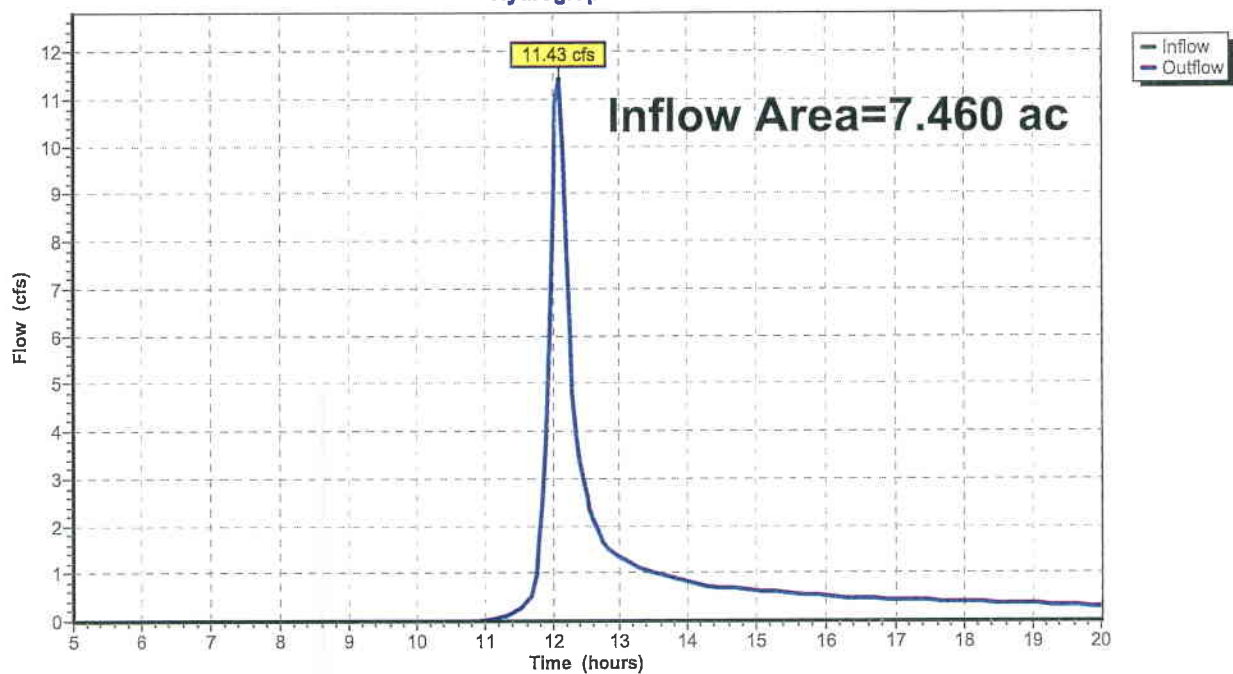
[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 7.460 ac, 13.14% Impervious, Inflow Depth > 1.22" for 100-yr event
Inflow = 11.43 cfs @ 12.09 hrs, Volume= 0.760 af
Outflow = 11.43 cfs @ 12.09 hrs, Volume= 0.760 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Reach 4R: WS #2 POA

Hydrograph



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Type II 24-hr 100-yr Rainfall=5.73"

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Summary for Pond 2P: Existing Wetlands

Inflow Area = 11.310 ac, 9.90% Impervious, Inflow Depth > 2.80" for 100-yr event
 Inflow = 37.85 cfs @ 12.13 hrs, Volume= 2.643 af
 Outflow = 37.06 cfs @ 12.17 hrs, Volume= 2.571 af, Atten= 2%, Lag= 2.0 min
 Primary = 37.06 cfs @ 12.17 hrs, Volume= 2.571 af

Routing by Dyn-Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
 Peak Elev= 992.80' @ 12.17 hrs Surf.Area= 25,548 sf Storage= 8,893 cf

Plug-Flow detention time= 18.6 min calculated for 2.562 af (97% of inflow)
 Center-of-Mass det. time= 8.4 min (803.7 - 795.3)

Volume	Invert	Avail.Storage	Storage Description
#1	991.90'	14,723 cf	Custom Stage Data (Prismatic) Listed below (Recalc)

Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
991.90	0	0	0
992.00	539	27	27
992.50	12,019	3,140	3,166
993.00	34,207	11,557	14,723

Device	Routing	Invert	Outlet Devices
#1	Primary	992.42'	Asymmetrical Weir, C= 3.27 Offset (feet) -82.00 -58.00 0.00 51.00 Height (feet) 0.58 0.25 0.00 0.58

Primary OutFlow Max=36.63 cfs @ 12.17 hrs HW=992.80' TW=0.00' (Dynamic Tailwater)
 1=Asymmetrical Weir (Weir Controls 36.63 cfs @ 1.01 fps)

Existing

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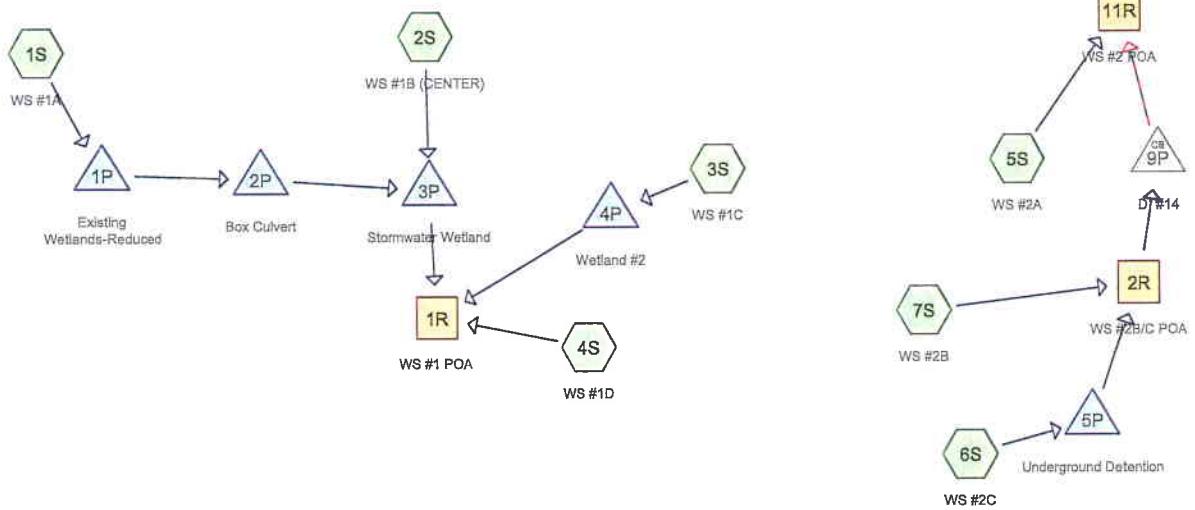
Type II 24-hr 100-yr Rainfall=5.73"

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Stage-Discharge for Pond 2P: Existing Wetlands

Elevation (feet)	Primary (cfs)	Elevation (feet)	Primary (cfs)	Elevation (feet)	Primary (cfs)
991.90	0.00	992.43	0.00	992.96	80.24
991.91	0.00	992.44	0.02	992.97	83.61
991.92	0.00	992.45	0.07	992.98	87.06
991.93	0.00	992.46	0.13	992.99	90.58
991.94	0.00	992.47	0.23	993.00	94.18
991.95	0.00	992.48	0.37		
991.96	0.00	992.49	0.54		
991.97	0.00	992.50	0.76		
991.98	0.00	992.51	1.02		
991.99	0.00	992.52	1.32		
992.00	0.00	992.53	1.68		
992.01	0.00	992.54	2.09		
992.02	0.00	992.55	2.55		
992.03	0.00	992.56	3.07		
992.04	0.00	992.57	3.65		
992.05	0.00	992.58	4.29		
992.06	0.00	992.59	4.99		
992.07	0.00	992.60	5.75		
992.08	0.00	992.61	6.58		
992.09	0.00	992.62	7.49		
992.10	0.00	992.63	8.46		
992.11	0.00	992.64	9.50		
992.12	0.00	992.65	10.62		
992.13	0.00	992.66	11.81		
992.14	0.00	992.67	13.08		
992.15	0.00	992.68	14.42		
992.16	0.00	992.69	15.84		
992.17	0.00	992.70	17.33		
992.18	0.00	992.71	18.89		
992.19	0.00	992.72	20.51		
992.20	0.00	992.73	22.21		
992.21	0.00	992.74	23.97		
992.22	0.00	992.75	25.80		
992.23	0.00	992.76	27.70		
992.24	0.00	992.77	29.67		
992.25	0.00	992.78	31.70		
992.26	0.00	992.79	33.81		
992.27	0.00	992.80	35.98		
992.28	0.00	992.81	38.22		
992.29	0.00	992.82	40.53		
992.30	0.00	992.83	42.91		
992.31	0.00	992.84	45.36		
992.32	0.00	992.85	47.87		
992.33	0.00	992.86	50.46		
992.34	0.00	992.87	53.12		
992.35	0.00	992.88	55.85		
992.36	0.00	992.89	58.64		
992.37	0.00	992.90	61.51		
992.38	0.00	992.91	64.45		
992.39	0.00	992.92	67.47		
992.40	0.00	992.93	70.55		
992.41	0.00	992.94	73.71		
992.42	0.00	992.95	76.93		



Proposed Condition Summaries

Routing Diagram for Proposed

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Proposed

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Proposed Conditions Summaries
Type II 24-hr 1-yr Rainfall=1.96"

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Page 2

Summary for Subcatchment 1S: WS #1A

Runoff = 2.79 cfs @ 12.17 hrs, Volume= 0.235 af, Depth> 0.31"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
Type II 24-hr 1-yr Rainfall=1.96"

Area (ac)	CN	Description
0.890	98	Paved parking, HSG D
0.260	30	Woods, Good, HSG A
1.580	77	Woods, Good, HSG D
1.100	39	>75% Grass cover, Good, HSG A
5.140	80	>75% Grass cover, Good, HSG D
8.970	75	Weighted Average
8.080		90.08% Pervious Area
0.890		9.92% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
0.5	18	0.0100	0.63		Sheet Flow, Smooth surfaces n= 0.011 P2= 2.31"
13.0	82	0.0100	0.11		Sheet Flow, Grass: Short n= 0.150 P2= 2.31"
1.9	171	0.0090	1.53		Shallow Concentrated Flow, Unpaved Kv= 16.1 fps
4.9	140	0.0090	0.47		Shallow Concentrated Flow, Woodland Kv= 5.0 fps
20.3	411	Total			

Summary for Subcatchment 2S: WS #1B (CENTER)

Runoff = 7.89 cfs @ 12.10 hrs, Volume= 0.525 af, Depth> 0.41"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
Type II 24-hr 1-yr Rainfall=1.96"

Area (ac)	CN	Description
4.680	98	Paved parking, HSG D
2.190	39	>75% Grass cover, Good, HSG A
0.210	61	>75% Grass cover, Good, HSG B
7.610	80	>75% Grass cover, Good, HSG D
0.470	30	Woods, Good, HSG A
0.290	77	Woods, Good, HSG D
15.450	78	Weighted Average
10.770		69.71% Pervious Area
4.680		30.29% Impervious Area

Proposed

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Proposed Conditions Summaries

Type II 24-hr 1-yr Rainfall=1.96"

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Area (ac)	CN	Description
0.680	78	Meadow, non-grazed, HSG D
0.640	80	>75% Grass cover, Good, HSG D
1.320	79	Weighted Average
1.320		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
4.5	65	0.0900	0.24		Sheet Flow, Grass: Short n= 0.150 P2= 2.31"
2.9	186	0.0044	1.07		Shallow Concentrated Flow, Unpaved Kv= 16.1 fps
7.4	251	Total			

Summary for Subcatchment 5S: WS #2A

Runoff = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af, Depth= 0.00"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
Type II 24-hr 1-yr Rainfall=1.96"

Area (ac)	CN	Description
0.200	98	Paved parking, HSG D
0.940	30	Woods, Good, HSG A
1.120	39	>75% Grass cover, Good, HSG A
0.120	61	>75% Grass cover, Good, HSG B
2.380	42	Weighted Average
2.180		91.60% Pervious Area
0.200		8.40% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.1	40	0.0250	0.13		Sheet Flow, Grass: Short n= 0.150 P2= 2.31"
12.3	60	0.0440	0.08		Sheet Flow, Woods: Light underbrush n= 0.400 P2= 2.31"
0.8	60	0.0660	1.28		Shallow Concentrated Flow, Woodland Kv= 5.0 fps
0.4	95	0.0660	4.14		Shallow Concentrated Flow, Unpaved Kv= 16.1 fps
1.2	90	0.0660	1.28		Shallow Concentrated Flow, Woodland Kv= 5.0 fps
4.0	188	0.0240	0.77		Shallow Concentrated Flow, Woodland Kv= 5.0 fps
23.8	533	Total			

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15.3 956 Total

Summary for Reach 1R: WS #1 POA

Inflow Area = 26.740 ac, 21.13% Impervious, Inflow Depth > 0.10" for 1-yr event
 Inflow = 1.06 cfs @ 12.00 hrs, Volume= 0.228 af
 Outflow = 1.06 cfs @ 12.00 hrs, Volume= 0.228 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Summary for Reach 2R: WS #2B/C POA

Inflow Area = 4.380 ac, 22.83% Impervious, Inflow Depth > 0.16" for 1-yr event
 Inflow = 0.41 cfs @ 12.16 hrs, Volume= 0.058 af
 Outflow = 0.41 cfs @ 12.16 hrs, Volume= 0.058 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Summary for Reach 11R: WS #2 POA

Inflow Area = 6.760 ac, 17.75% Impervious, Inflow Depth > 0.10" for 1-yr event
 Inflow = 0.41 cfs @ 12.16 hrs, Volume= 0.058 af
 Outflow = 0.41 cfs @ 12.16 hrs, Volume= 0.058 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Summary for Pond 1P: Existing Wetlands-Reduced

Inflow Area = 8.970 ac, 9.92% Impervious, Inflow Depth > 0.31" for 1-yr event
 Inflow = 2.79 cfs @ 12.17 hrs, Volume= 0.235 af
 Outflow = 1.05 cfs @ 12.53 hrs, Volume= 0.173 af, Atten= 62%, Lag= 21.5 min
 Primary = 1.05 cfs @ 12.53 hrs, Volume= 0.173 af

Routing by Dyn-Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
 Peak Elev= 992.51' @ 12.53 hrs Surf.Area= 12,324 sf Storage= 3,267 cf

Plug-Flow detention time= 119.5 min calculated for 0.173 af (74% of inflow)
 Center-of-Mass det. time= 49.2 min (892.7 - 843.5)

Volume	Invert	Avail.Storage	Storage Description
#1	991.90'	21,366 cf	Custom Stage Data (Prismatic) Listed below (Recalc)

Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
991.90	0	0	0
992.00	539	27	27
992.50	12,019	3,140	3,166
993.00	30,390	10,602	13,769
993.25	30,390	7,598	21,366

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Peak Elev= 990.55' @ 20.00 hrs Surf.Area= 42,095 sf Storage= 22,531 cf

Plug-Flow detention time= 257.3 min calculated for 0.179 af (26% of inflow)
Center-of-Mass det. time= 136.0 min (982.5 - 846.5)

Volume	Invert	Avail.Storage	Storage Description
#1	990.00'	169,355 cf	Custom Stage Data (Prismatic) Listed below (Recalc)

Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
990.00	39,300	0	0
993.00	54,445	140,618	140,618
993.50	60,505	28,738	169,355

Device	Routing	Invert	Outlet Devices
#1	Primary	990.00'	18.0" Round Culvert x3 X 3.00 L= 50.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 990.00' / 989.75' S= 0.0050 ' S= 0.0050 ' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 1.77 sf
#2	Device 1	990.00'	3.0" Vert. Orificex2 X 2.00 C= 0.600
#3	Device 1	992.00'	36.0" x 36.0" Horiz. Grate#1 C= 0.600 Limited to weir flow at low heads
#4	Device 1	992.00'	36.0" x 60.0" Horiz. Grate#2 C= 0.600 Limited to weir flow at low heads
#5	Secondary	993.00'	32.0' long x 10.0' breadth Broad-Crested Rectangular Weir Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 Coef. (English) 2.49 2.56 2.70 2.69 2.68 2.69 2.67 2.64

Primary OutFlow Max=0.31 cfs @ 20.00 hrs HW=990.55' TW=0.00' (Dynamic Tailwater)

1=Culvert x3 (Passes 0.31 cfs of 3.17 cfs potential flow)
2=Orificex2 (Orifice Controls 0.31 cfs @ 3.15 fps)
3=Grate#1 (Controls 0.00 cfs)
4=Grate#2 (Controls 0.00 cfs)

Secondary OutFlow Max=0.00 cfs @ 5.00 hrs HW=990.00' (Free Discharge)

5=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Summary for Pond 4P: Wetland #2

Inflow Area = 1.000 ac, 8.00% Impervious, Inflow Depth > 0.02" for 1-yr event
Inflow = 0.00 cfs @ 17.70 hrs, Volume= 0.001 af
Outflow = 0.00 cfs @ 20.00 hrs, Volume= 0.000 af, Atten= 78%, Lag= 138.1 min
Primary = 0.00 cfs @ 20.00 hrs, Volume= 0.000 af
Secondary = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af

Routing by Dyn-Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
Peak Elev= 990.77' @ 20.00 hrs Surf.Area= 3,221 sf Storage= 52 cf

Plug-Flow detention time= 275.7 min calculated for 0.000 af (8% of inflow)
Center-of-Mass det. time= 92.2 min (1,105.8 - 1,013.5)

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n= 0.013 Corrugated PE, smooth interior, Flow Area= 1.23 sf
#2 Device 1 980.55' **3.0" Vert. Orifice** C= 0.600
#3 Device 1 982.95' **2.0' long Sharp-Crested Rectangular Weir** 2 End Contraction(s)

Primary OutFlow Max=0.15 cfs @ 12.09 hrs HW=981.10' TW=0.00' (Dynamic Tailwater)

↑ **1=Culvert** (Passes 0.15 cfs of 1.80 cfs potential flow)
↑ **2=Orifice** (Orifice Controls 0.15 cfs @ 3.14 fps)
↑ **3=Sharp-Crested Rectangular Weir** (Controls 0.00 cfs)

Summary for Pond 9P: DI #14

Inflow Area = 4.380 ac, 22.83% Impervious, Inflow Depth > 0.16" for 1-yr event
Inflow = 0.41 cfs @ 12.16 hrs, Volume= 0.058 af
Outflow = 0.41 cfs @ 12.16 hrs, Volume= 0.058 af, Atten= 0%, Lag= 0.0 min
Primary = 0.41 cfs @ 12.16 hrs, Volume= 0.058 af
Secondary = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af

Routing by Dyn-Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Peak Elev= 979.93' @ 12.16 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	979.30'	18.0" Round Existing Culvert L= 308.0' CMP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 979.30' / 979.05' S= 0.0008 ' S= 0.0008 ' Cc= 0.900 n= 0.025 Corrugated metal, Flow Area= 1.77 sf
#2	Secondary	983.30'	17.2" x 17.2" Horiz. Grate EJIW 5115M2 C= 0.600 Limited to weir flow at low heads

Primary OutFlow Max=0.41 cfs @ 12.16 hrs HW=979.93' TW=0.00' (Dynamic Tailwater)

↑ **1=Existing Culvert** (Barrel Controls 0.41 cfs @ 0.87 fps)

Secondary OutFlow Max=0.00 cfs @ 5.00 hrs HW=979.30' TW=0.00' (Dynamic Tailwater)

↑ **2=Grate EJIW 5115M2** (Controls 0.00 cfs)

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Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
0.4	14	0.0100	0.60		Sheet Flow, Smooth surfaces n= 0.011 P2= 2.31"
9.3	86	0.0250	0.15		Sheet Flow, Grass: Short n= 0.150 P2= 2.31"
1.7	218	0.0180	2.16		Shallow Concentrated Flow, Unpaved Kv= 16.1 fps
1.5	62	0.0180	0.67		Shallow Concentrated Flow, Woodland Kv= 5.0 fps
0.3	60	0.0330	2.92		Shallow Concentrated Flow, Unpaved Kv= 16.1 fps
2.7	250	0.0025	1.56	15.55	Trap/Vee/Rect Channel Flow, Bot.W=0.00' D=1.00' Z= 10.0 ' /' Top.W=20.00' n= 0.030 Short grass
0.1	77	0.0480	9.94	7.81	Pipe Channel, 12.0" Round Area= 0.8 sf Perim= 3.1' r= 0.25' n= 0.013 Corrugated PE, smooth interior
16.0	767	Total			

Summary for Subcatchment 3S: WS #1C

Runoff = 0.28 cfs @ 12.11 hrs, Volume= 0.026 af, Depth> 0.31"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
Type II 24-hr 10-yr Rainfall=3.36"

Area (ac)	CN	Description
0.080	98	Paved parking, HSG D
0.320	39	>75% Grass cover, Good, HSG A
0.600	61	>75% Grass cover, Good, HSG B
1.000	57	Weighted Average
0.920		92.00% Pervious Area
0.080		8.00% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
12.9	100	0.0150	0.13		Sheet Flow, Grass: Short n= 0.150 P2= 2.31"
1.0	100	0.0100	1.61		Shallow Concentrated Flow, Unpaved Kv= 16.1 fps
13.9	200	Total			

Summary for Subcatchment 4S: WS #1D

Runoff = 3.22 cfs @ 11.99 hrs, Volume= 0.147 af, Depth> 1.33"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
Type II 24-hr 10-yr Rainfall=3.36"

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Type II 24-hr 10-yr Rainfall=3.36"

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Summary for Subcatchment 6S: WS #2C

Runoff = 0.73 cfs @ 11.96 hrs, Volume= 0.036 af, Depth> 2.53"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
Type II 24-hr 10-yr Rainfall=3.36"

Area (ac)	CN	Description
0.150	98	Paved parking, HSG B
0.020	61	>75% Grass cover, Good, HSG B
0.170	94	Weighted Average
0.020		11.76% Pervious Area
0.150		88.24% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.1	100	0.0350	1.46		Sheet Flow, Smooth surfaces n= 0.011 P2= 2.31"
0.6	140	0.0350	3.80		Shallow Concentrated Flow, Paved Kv= 20.3 fps
4.3					Direct Entry,
6.0	240	Total			

Summary for Subcatchment 7S: WS #2B

Runoff = 3.36 cfs @ 12.10 hrs, Volume= 0.224 af, Depth> 0.64"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
Type II 24-hr 10-yr Rainfall=3.36"

Area (ac)	CN	Description
0.850	98	Paved parking, HSG D
0.100	30	Woods, Good, HSG A
0.350	39	>75% Grass cover, Good, HSG A
2.910	61	>75% Grass cover, Good, HSG B
4.210	66	Weighted Average
3.360		79.81% Pervious Area
0.850		20.19% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
9.8	100	0.0300	0.17		Sheet Flow, Grass: Short n= 0.150 P2= 2.31"
1.3	180	0.0210	2.33		Shallow Concentrated Flow, Unpaved Kv= 16.1 fps
1.7	206	0.0100	2.03		Shallow Concentrated Flow, Paved Kv= 20.3 fps
2.5	470	0.0100	3.09	5.46	Pipe Channel, 18.0" Round Area= 1.8 sf Perim= 4.7' r= 0.38' n= 0.025 Corrugated metal

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Device	Routing	Invert	Outlet Devices
#1	Primary	992.42'	Asymmetrical Weir, C= 3.27 Offset (feet) -26.27 -25.00 0.00 20.00 26.27 Height (feet) 0.58 0.13 0.00 0.13 0.58

Primary OutFlow Max=10.57 cfs @ 12.20 hrs HW=992.65' TW=992.45' (Dynamic Tailwater)

↑**1=Asymmetrical Weir** (Weir Controls 10.57 cfs @ 0.98 fps)

Summary for Pond 2P: Box Culvert

Inflow Area = 8.970 ac, 9.92% Impervious, Inflow Depth > 1.00" for 10-yr event
Inflow = 10.62 cfs @ 12.20 hrs, Volume= 0.745 af
Outflow = 10.29 cfs @ 12.25 hrs, Volume= 0.739 af, Atten= 3%, Lag= 2.5 min
Primary = 10.29 cfs @ 12.25 hrs, Volume= 0.739 af

Routing by Dyn-Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
Peak Elev= 992.46' @ 12.25 hrs Surf.Area= 4,119 sf Storage= 1,818 cf

Plug-Flow detention time= 5.9 min calculated for 0.736 af (99% of inflow)
Center-of-Mass det. time= 2.9 min (832.2 - 829.3)

Volume	Invert	Avail.Storage	Storage Description
#1	992.00'	4,045 cf	Custom Stage Data (Prismatic) Listed below (Recalc)
Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
992.00	3,730	0	0
992.50	4,150	1,970	1,970
993.00	4,150	2,075	4,045

Device	Routing	Invert	Outlet Devices
#1	Primary	992.00'	122.0" W x 32.0" H Box Culvert L= 150.0' Box, headwall w/3 square edges, Ke= 0.500 Inlet / Outlet Invert= 992.00' / 990.00' S= 0.0133 '/' Cc= 0.900 n= 0.011 Concrete pipe, straight & clean, Flow Area= 27.11 sf

Primary OutFlow Max=10.24 cfs @ 12.25 hrs HW=992.46' TW=990.86' (Dynamic Tailwater)

↑**1=Culvert** (Inlet Controls 10.24 cfs @ 2.18 fps)

Summary for Pond 3P: Stormwater Wetland

Inflow Area = 24.420 ac, 22.81% Impervious, Inflow Depth > 1.16" for 10-yr event
Inflow = 31.58 cfs @ 12.13 hrs, Volume= 2.368 af
Outflow = 0.64 cfs @ 20.00 hrs, Volume= 0.394 af, Atten= 98%, Lag= 472.1 min
Primary = 0.64 cfs @ 20.00 hrs, Volume= 0.394 af
Secondary = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af

Routing by Dyn-Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

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Volume	Invert	Avail.Storage	Storage Description
#1	990.75'	10,990 cf	Custom Stage Data (Prismatic) Listed below (Recalc)

Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
990.75	3,160	0	0
991.00	4,100	908	908
992.00	5,025	4,563	5,470
993.00	6,015	5,520	10,990

Device	Routing	Invert	Outlet Devices
#1	Primary	990.75'	8.0" Round Culvert L= 25.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 990.75' / 990.50' S= 0.0100 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.35 sf
#2	Device 1	990.75'	3.0" Vert. Orifice C= 0.600
#3	Device 1	992.50'	36.0" x 36.0" Horiz. Grate C= 0.600 Limited to weir flow at low heads
#4	Secondary	993.00'	32.0' long x 10.0' breadth Broad-Crested Rectangular Weir Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 Coef. (English) 2.49 2.56 2.70 2.69 2.68 2.69 2.67 2.64

Primary OutFlow Max=0.03 cfs @ 14.35 hrs HW=990.88' TW=0.00' (Dynamic Tailwater)

1=Culvert (Passes 0.03 cfs of 0.05 cfs potential flow)

2=Orifice (Orifice Controls 0.03 cfs @ 1.24 fps)

3=Grate (Controls 0.00 cfs)

Secondary OutFlow Max=0.00 cfs @ 5.00 hrs HW=990.75' (Free Discharge)

4=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Summary for Pond 5P: Underground Detention

Inflow Area = 0.170 ac, 88.24% Impervious, Inflow Depth > 2.53" for 10-yr event
 Inflow = 0.73 cfs @ 11.96 hrs, Volume= 0.036 af
Outflow = 0.22 cfs @ 12.11 hrs, Volume= 0.036 af, Atten= 70%, Lag= 8.7 min
 Primary = 0.22 cfs @ 12.11 hrs, Volume= 0.036 af

Routing by Dyn-Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
 Peak Elev= 981.55' @ 12.11 hrs Surf.Area= 0.015 ac Storage= 0.011 af

Plug-Flow detention time= 21.6 min calculated for 0.036 af (99% of inflow)
 Center-of-Mass det. time= 19.2 min (769.2 - 750.0)

Volume	Invert	Avail.Storage	Storage Description
#1	980.55'	0.029 af	30.0" Round Pipe Storage x 2 L= 130.0'

Device	Routing	Invert	Outlet Devices
#1	Primary	980.35'	15.0" Round Culvert L= 95.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 980.35' / 979.30' S= 0.0111 '/' Cc= 0.900

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Summary for Subcatchment 1S: WS #1A

Runoff = 30.02 cfs @ 12.13 hrs, Volume= 2.096 af, Depth> 2.80"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
Type II 24-hr 100-yr Rainfall=5.73"

Area (ac)	CN	Description
0.890	98	Paved parking, HSG D
0.260	30	Woods, Good, HSG A
1.580	77	Woods, Good, HSG D
1.100	39	>75% Grass cover, Good, HSG A
5.140	80	>75% Grass cover, Good, HSG D
8.970	75	Weighted Average
8.080		90.08% Pervious Area
0.890		9.92% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
0.5	18	0.0100	0.63		Sheet Flow, Smooth surfaces n= 0.011 P2= 2.31"
13.0	82	0.0100	0.11		Sheet Flow, Grass: Short n= 0.150 P2= 2.31"
1.9	171	0.0090	1.53		Shallow Concentrated Flow, Unpaved Kv= 16.1 fps
4.9	140	0.0090	0.47		Shallow Concentrated Flow, Woodland Kv= 5.0 fps
20.3	411	Total			

Summary for Subcatchment 2S: WS #1B (CENTER)

Runoff = 64.12 cfs @ 12.08 hrs, Volume= 3.975 af, Depth> 3.09"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
Type II 24-hr 100-yr Rainfall=5.73"

Area (ac)	CN	Description
4.680	98	Paved parking, HSG D
2.190	39	>75% Grass cover, Good, HSG A
0.210	61	>75% Grass cover, Good, HSG B
7.610	80	>75% Grass cover, Good, HSG D
0.470	30	Woods, Good, HSG A
0.290	77	Woods, Good, HSG D
15.450	78	Weighted Average
10.770		69.71% Pervious Area
4.680		30.29% Impervious Area

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Area (ac)	CN	Description
0.680	78	Meadow, non-grazed, HSG D
0.640	80	>75% Grass cover, Good, HSG D
1.320	79	Weighted Average
1.320		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
4.5	65	0.0900	0.24		Sheet Flow, Grass: Short n= 0.150 P2= 2.31"
2.9	186	0.0044	1.07		Shallow Concentrated Flow, Unpaved Kv= 16.1 fps
7.4	251	Total			

Summary for Subcatchment 5S: WS #2A

Runoff = 0.56 cfs @ 12.27 hrs, Volume= 0.086 af, Depth> 0.43"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
Type II 24-hr 100-yr Rainfall=5.73"

Area (ac)	CN	Description
0.200	98	Paved parking, HSG D
0.940	30	Woods, Good, HSG A
1.120	39	>75% Grass cover, Good, HSG A
0.120	61	>75% Grass cover, Good, HSG B
2.380	42	Weighted Average
2.180		91.60% Pervious Area
0.200		8.40% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.1	40	0.0250	0.13		Sheet Flow, Grass: Short n= 0.150 P2= 2.31"
12.3	60	0.0440	0.08		Sheet Flow, Woods: Light underbrush n= 0.400 P2= 2.31"
0.8	60	0.0660	1.28		Shallow Concentrated Flow, Woodland Kv= 5.0 fps
0.4	95	0.0660	4.14		Shallow Concentrated Flow, Unpaved Kv= 16.1 fps
1.2	90	0.0660	1.28		Shallow Concentrated Flow, Woodland Kv= 5.0 fps
4.0	188	0.0240	0.77		Shallow Concentrated Flow, Woodland Kv= 5.0 fps
23.8	533	Total			

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15.3 956 Total

Summary for Reach 1R: WS #1 POA

Inflow Area = 26.740 ac, 21.13% Impervious, Inflow Depth > 1.94" for 100-yr event
 Inflow = 28.18 cfs @ 12.42 hrs, Volume= 4.332 af
Outflow = 28.18 cfs @ 12.42 hrs, Volume= 4.332 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Summary for Reach 2R: WS #2B/C POA

Inflow Area = 4.380 ac, 22.83% Impervious, Inflow Depth > 2.14" for 100-yr event
 Inflow = 12.11 cfs @ 12.08 hrs, Volume= 0.779 af
 Outflow = 12.11 cfs @ 12.08 hrs, Volume= 0.779 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Summary for Reach 11R: WS #2 POA

Inflow Area = 6.760 ac, 17.75% Impervious, Inflow Depth > 1.54" for 100-yr event
 Inflow = 12.35 cfs @ 12.09 hrs, Volume= 0.865 af
Outflow = 12.35 cfs @ 12.09 hrs, Volume= 0.865 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Summary for Pond 1P: Existing Wetlands-Reduced

Inflow Area = 8.970 ac, 9.92% Impervious, Inflow Depth > 2.80" for 100-yr event
 Inflow = 30.02 cfs @ 12.13 hrs, Volume= 2.096 af
Outflow = 24.60 cfs @ 12.20 hrs, Volume= 2.026 af, Atten= 18%, Lag= 4.3 min
 Primary = 24.60 cfs @ 12.20 hrs, Volume= 2.026 af

Routing by Dyn-Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
 Peak Elev= 992.88' @ 12.25 hrs Surf.Area= 26,162 sf Storage= 10,515 cf

Plug-Flow detention time= 23.1 min calculated for 2.019 af (96% of inflow)
 Center-of-Mass det. time= 10.8 min (806.2 - 795.3)

Volume	Invert	Avail.Storage	Storage Description
#1	991.90'	21,366 cf	Custom Stage Data (Prismatic) Listed below (Recalc)

Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
991.90	0	0	0
992.00	539	27	27
992.50	12,019	3,140	3,166
993.00	30,390	10,602	13,769
993.25	30,390	7,598	21,366

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Proposed Conditions Summaries
Type II 24-hr 100-yr Rainfall=5.73"

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Peak Elev= 992.58' @ 12.46 hrs Surf.Area= 52,305 sf Storage= 117,990 cf

Plug-Flow detention time= 129.3 min calculated for 3.893 af (65% of inflow)
Center-of-Mass det. time= 58.8 min (853.1 - 794.2)

Volume	Invert	Avail.Storage	Storage Description
#1	990.00'	169,355 cf	Custom Stage Data (Prismatic) Listed below (Recalc)

Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
990.00	39,300	0	0
993.00	54,445	140,618	140,618
993.50	60,505	28,738	169,355

Device	Routing	Invert	Outlet Devices
#1	Primary	990.00'	18.0" Round Culvert x3 X 3.00 L= 50.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 990.00' / 989.75' S= 0.0050 ' ' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 1.77 sf
#2	Device 1	990.00'	3.0" Vert. Orificex2 X 2.00 C= 0.600
#3	Device 1	992.00'	36.0" x 36.0" Horiz. Grate#1 C= 0.600 Limited to weir flow at low heads
#4	Device 1	992.00'	36.0" x 60.0" Horiz. Grate#2 C= 0.600 Limited to weir flow at low heads
#5	Secondary	993.00'	32.0' long x 10.0' breadth Broad-Crested Rectangular Weir Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 Coef. (English) 2.49 2.56 2.70 2.69 2.68 2.69 2.67 2.64

Primary OutFlow Max=27.23 cfs @ 12.46 hrs HW=992.58' TW=0.00' (Dynamic Tailwater)

1=Culvert x3 (Inlet Controls 27.23 cfs @ 5.14 fps)
2=Orificex2 (Passes < 0.74 cfs potential flow)
3=Grate#1 (Passes < 17.13 cfs potential flow)
4=Grate#2 (Passes < 22.84 cfs potential flow)

Secondary OutFlow Max=0.00 cfs @ 5.00 hrs HW=990.00' (Free Discharge)

5=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Summary for Pond 4P: Wetland #2

Inflow Area =	1.000 ac,	8.00% Impervious,	Inflow Depth > 1.35"	for 100-yr event
Inflow =	1.87 cfs @	12.07 hrs,	Volume=	0.112 af
Outflow =	0.16 cfs @	13.36 hrs,	Volume=	0.089 af, Atten= 91%, Lag= 77.3 min
Primary =	0.16 cfs @	13.36 hrs,	Volume=	0.089 af
Secondary =	0.00 cfs @	5.00 hrs,	Volume=	0.000 af

Routing by Dyn-Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
Peak Elev= 991.33' @ 13.36 hrs Surf.Area= 4,406 sf Storage= 2,316 cf

Plug-Flow detention time= 179.6 min calculated for 0.089 af (79% of inflow)
Center-of-Mass det. time= 119.5 min (942.7 - 823.2)

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Type II 24-hr 100-yr Rainfall=5.73"

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n= 0.013 Corrugated PE, smooth interior, Flow Area= 1.23 sf
#2 Device 1 980.55' **3.0" Vert. Orifice** C= 0.600
#3 Device 1 982.95' **2.0' long Sharp-Crested Rectangular Weir** 2 End Contraction(s)

Primary OutFlow Max=0.30 cfs @ 12.13 hrs HW=982.33' TW=0.00' (Dynamic Tailwater)

↑ **1=Culvert** (Passes 0.30 cfs of 5.43 cfs potential flow)
↑ **2=Orifice** (Orifice Controls 0.30 cfs @ 6.20 fps)
↑ **3=Sharp-Crested Rectangular Weir** (Controls 0.00 cfs)

Summary for Pond 9P: DI #14

Inflow Area = 4.380 ac, 22.83% Impervious, Inflow Depth > 2.14" for 100-yr event
Inflow = 12.11 cfs @ 12.08 hrs, Volume= 0.779 af
Outflow = 12.11 cfs @ 12.08 hrs, Volume= 0.779 af, Atten= 0%, Lag= 0.0 min
Primary = 5.37 cfs @ 12.08 hrs, Volume= 0.663 af
Secondary = 6.74 cfs @ 12.08 hrs, Volume= 0.116 af

Routing by Dyn-Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
Peak Elev= 983.81' @ 12.08 hrs

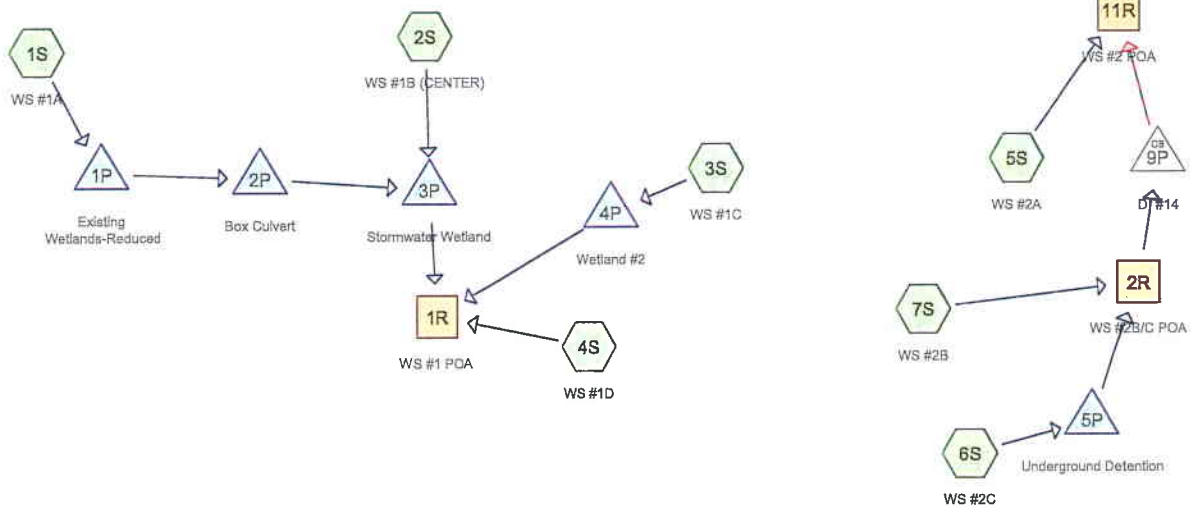
Device	Routing	Invert	Outlet Devices
#1	Primary	979.30'	18.0" Round Existing Culvert L= 308.0' CMP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 979.30' / 979.05' S= 0.0008 '/' Cc= 0.900 n= 0.025 Corrugated metal, Flow Area= 1.77 sf
#2	Secondary	983.30'	17.2" x 17.2" Horiz. Grate EJIW 5115M2 C= 0.600 Limited to weir flow at low heads

Primary OutFlow Max=5.36 cfs @ 12.08 hrs HW=983.80' TW=0.00' (Dynamic Tailwater)

↑ **1=Existing Culvert** (Barrel Controls 5.36 cfs @ 3.03 fps)

Secondary OutFlow Max=6.54 cfs @ 12.08 hrs HW=983.80' TW=0.00' (Dynamic Tailwater)

↑ **2=Grate EJIW 5115M2** (Weir Controls 6.54 cfs @ 2.30 fps)



Routing Diagram for Proposed
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Type II 24-hr 1-yr Rainfall=1.96"

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Summary for Subcatchment 1S: WS #1A

Runoff = 2.79 cfs @ 12.17 hrs, Volume= 0.235 af, Depth> 0.31"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Type II 24-hr 1-yr Rainfall=1.96"

Area (ac)	CN	Description
0.890	98	Paved parking, HSG D
0.260	30	Woods, Good, HSG A
1.580	77	Woods, Good, HSG D
1.100	39	>75% Grass cover, Good, HSG A
5.140	80	>75% Grass cover, Good, HSG D
8.970	75	Weighted Average
8.080		90.08% Pervious Area
0.890		9.92% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
0.5	18	0.0100	0.63		Sheet Flow, Smooth surfaces n= 0.011 P2= 2.31"
13.0	82	0.0100	0.11		Sheet Flow, Grass: Short n= 0.150 P2= 2.31"
1.9	171	0.0090	1.53		Shallow Concentrated Flow, Unpaved Kv= 16.1 fps
4.9	140	0.0090	0.47		Shallow Concentrated Flow, Woodland Kv= 5.0 fps
20.3	411	Total			

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Type II 24-hr 1-yr Rainfall=1.96"

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Summary for Subcatchment 2S: WS #1B (CENTER)

Runoff = 7.89 cfs @ 12.10 hrs, Volume= 0.525 af, Depth> 0.41"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Type II 24-hr 1-yr Rainfall=1.96"

Area (ac)	CN	Description
4.680	98	Paved parking, HSG D
2.190	39	>75% Grass cover, Good, HSG A
0.210	61	>75% Grass cover, Good, HSG B
7.610	80	>75% Grass cover, Good, HSG D
0.470	30	Woods, Good, HSG A
0.290	77	Woods, Good, HSG D
15.450	78	Weighted Average
10.770		69.71% Pervious Area
4.680		30.29% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
0.4	14	0.0100	0.60		Sheet Flow, Smooth surfaces n= 0.011 P2= 2.31"
9.3	86	0.0250	0.15		Sheet Flow, Grass: Short n= 0.150 P2= 2.31"
1.7	218	0.0180	2.16		Shallow Concentrated Flow, Unpaved Kv= 16.1 fps
1.5	62	0.0180	0.67		Shallow Concentrated Flow, Woodland Kv= 5.0 fps
0.3	60	0.0330	2.92		Shallow Concentrated Flow, Unpaved Kv= 16.1 fps
2.7	250	0.0025	1.56	15.55	Trap/Vee/Rect Channel Flow, Bot.W=0.00' D=1.00' Z= 10.0 ' Top.W=20.00' n= 0.030 Short grass
0.1	77	0.0480	9.94	7.81	Pipe Channel, 12.0" Round Area= 0.8 sf Perim= 3.1' r= 0.25' n= 0.013 Corrugated PE, smooth interior
16.0	767	Total			

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Type II 24-hr 1-yr Rainfall=1.96"

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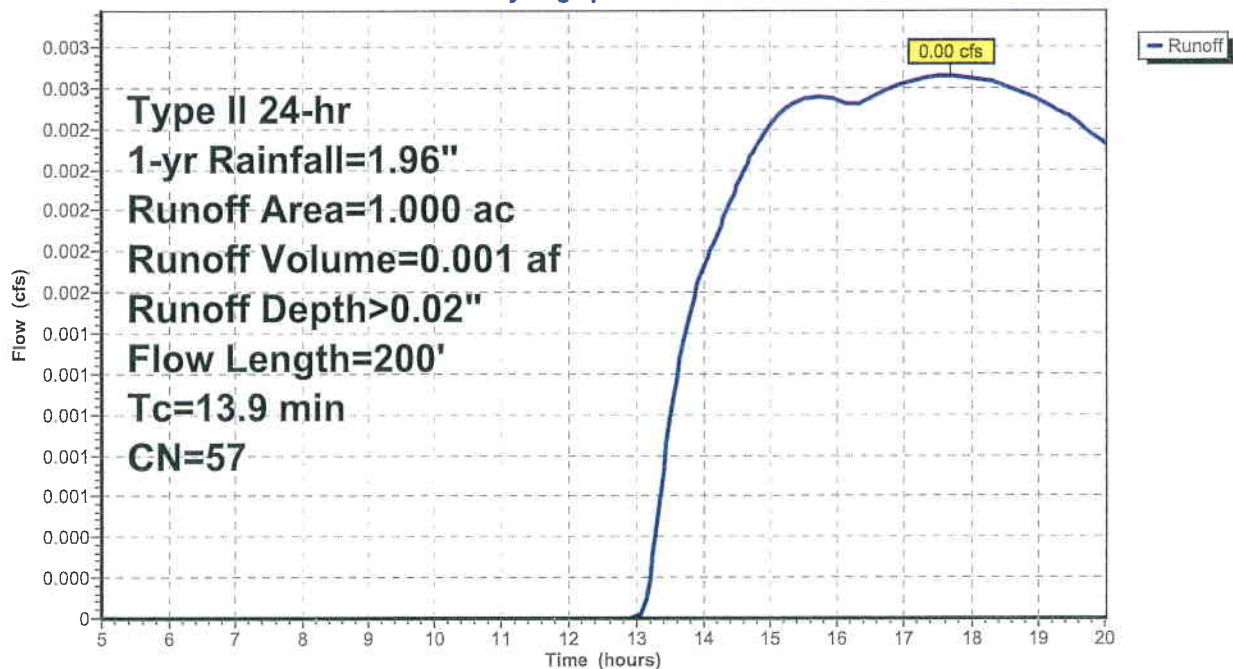
Summary for Subcatchment 3S: WS #1C

Runoff = 0.00 cfs @ 17.70 hrs, Volume= 0.001 af, Depth> 0.02"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
Type II 24-hr 1-yr Rainfall=1.96"

Area (ac)	CN	Description
0.080	98	Paved parking, HSG D
0.320	39	>75% Grass cover, Good, HSG A
0.600	61	>75% Grass cover, Good, HSG B
1.000	57	Weighted Average
0.920		92.00% Pervious Area
0.080		8.00% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
12.9	100	0.0150	0.13		Sheet Flow, Grass: Short n= 0.150 P2= 2.31"
1.0	100	0.0100	1.61		Shallow Concentrated Flow, Unpaved Kv= 16.1 fps
13.9	200	Total			

Subcatchment 3S: WS #1C**Hydrograph**

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Type II 24-hr 1-yr Rainfall=1.96"

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Summary for Subcatchment 5S: WS #2A

Runoff = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af, Depth= 0.00"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
Type II 24-hr 1-yr Rainfall=1.96"

Area (ac)	CN	Description
0.200	98	Paved parking, HSG D
0.940	30	Woods, Good, HSG A
1.120	39	>75% Grass cover, Good, HSG A
0.120	61	>75% Grass cover, Good, HSG B
2.380	42	Weighted Average
2.180		91.60% Pervious Area
0.200		8.40% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.1	40	0.0250	0.13		Sheet Flow, Grass: Short n= 0.150 P2= 2.31"
12.3	60	0.0440	0.08		Sheet Flow, Woods: Light underbrush n= 0.400 P2= 2.31"
0.8	60	0.0660	1.28		Shallow Concentrated Flow, Woodland Kv= 5.0 fps
0.4	95	0.0660	4.14		Shallow Concentrated Flow, Unpaved Kv= 16.1 fps
1.2	90	0.0660	1.28		Shallow Concentrated Flow, Woodland Kv= 5.0 fps
4.0	188	0.0240	0.77		Shallow Concentrated Flow, Woodland Kv= 5.0 fps
23.8	533	Total			

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Type II 24-hr 1-yr Rainfall=1.96"

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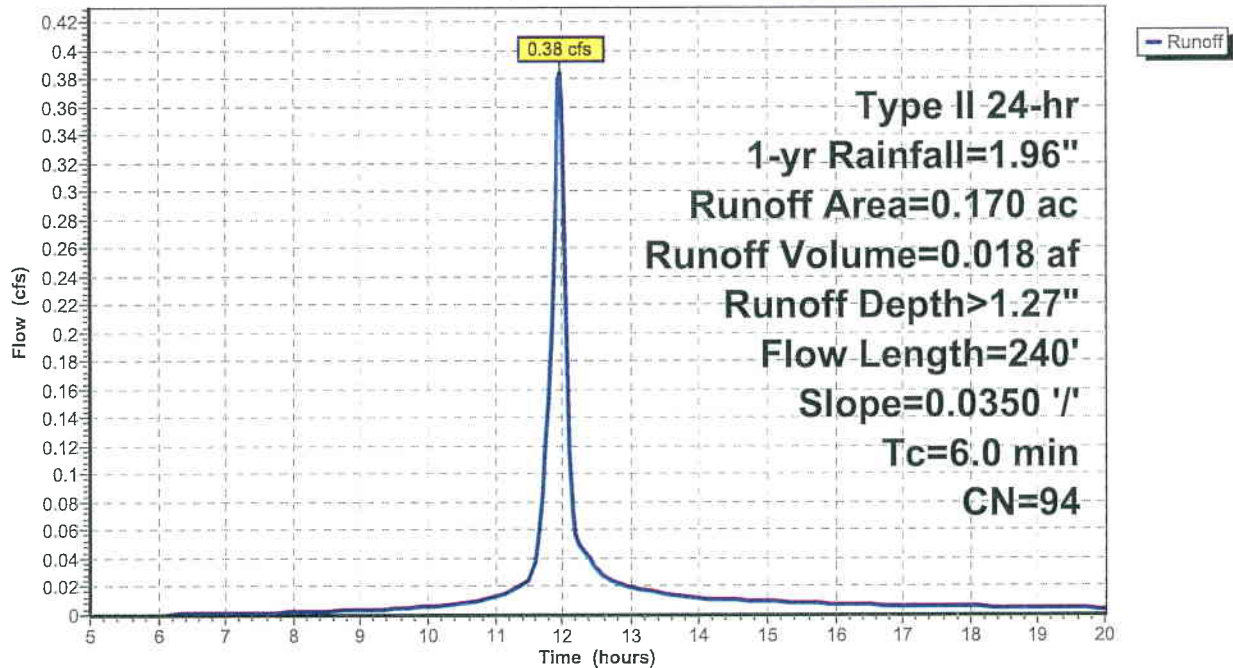
Summary for Subcatchment 6S: WS #2C

Runoff = 0.38 cfs @ 11.97 hrs, Volume= 0.018 af, Depth> 1.27"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
Type II 24-hr 1-yr Rainfall=1.96"

Area (ac)	CN	Description
0.150	98	Paved parking, HSG B
0.020	61	>75% Grass cover, Good, HSG B
0.170	94	Weighted Average
0.020		11.76% Pervious Area
0.150		88.24% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.1	100	0.0350	1.46		Sheet Flow, Smooth surfaces n= 0.011 P2= 2.31"
0.6	140	0.0350	3.80		Shallow Concentrated Flow, Paved Kv= 20.3 fps
4.3					Direct Entry,
6.0	240	Total			

Subcatchment 6S: WS #2C**Hydrograph**

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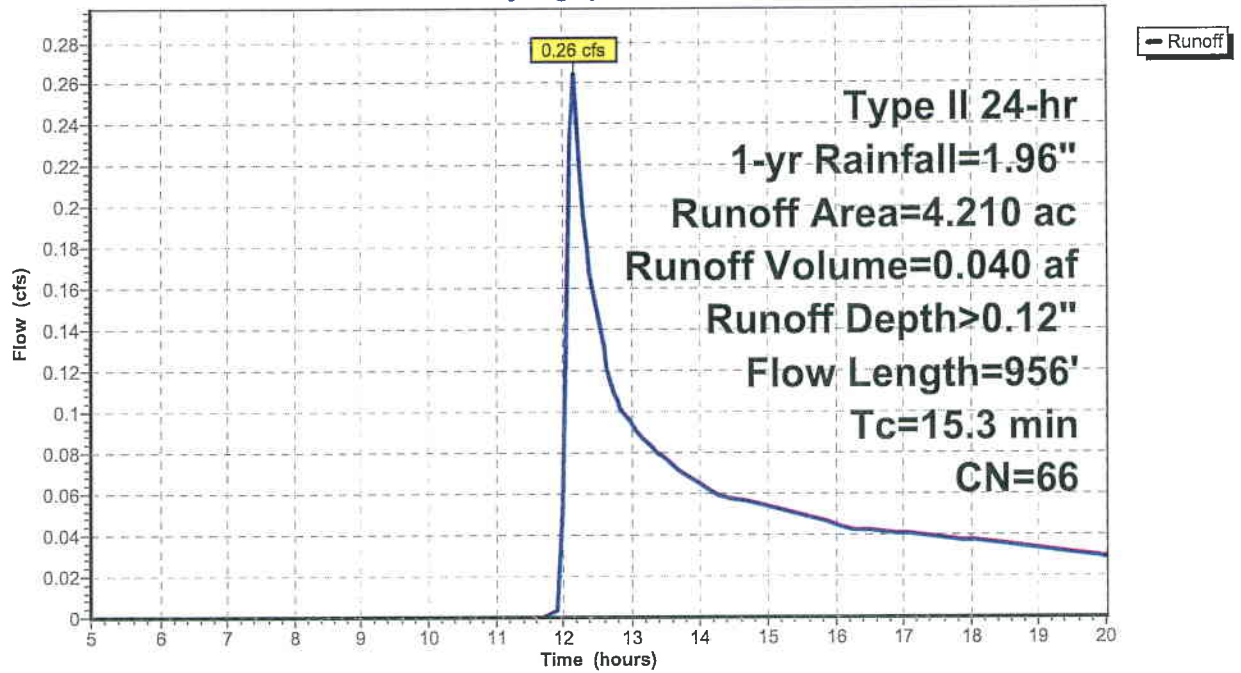
Type II 24-hr 1-yr Rainfall=1.96"

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Subcatchment 7S: WS #2B

Hydrograph



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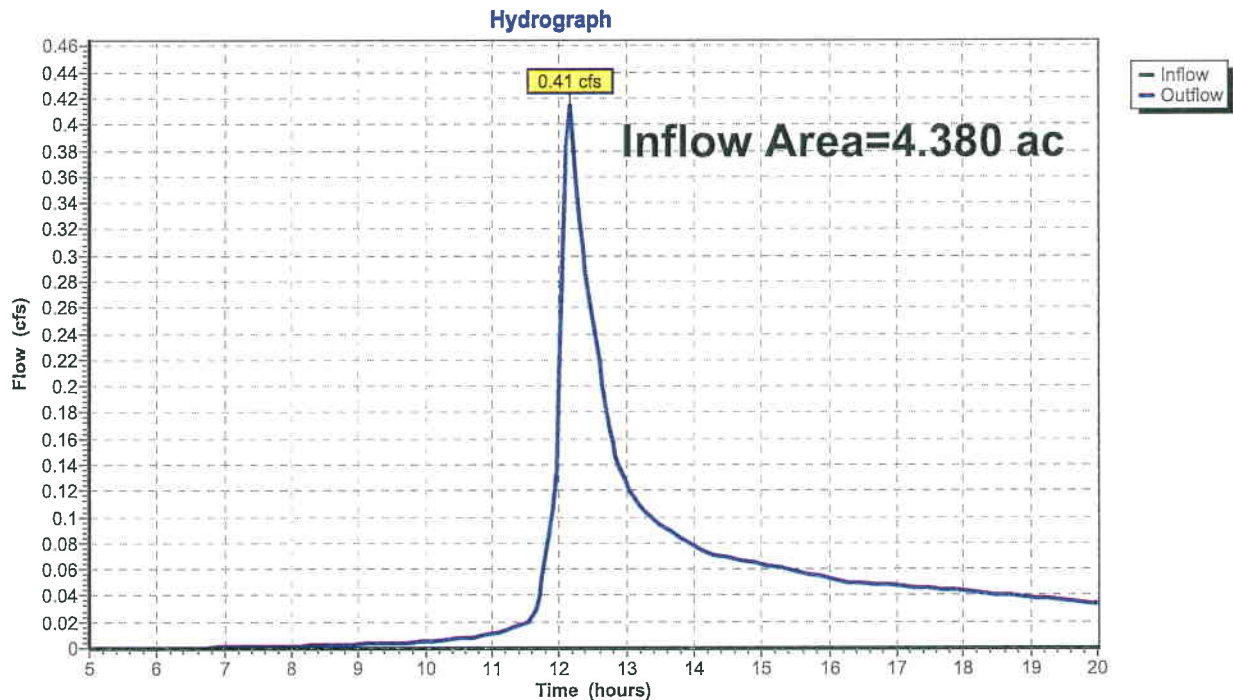
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Summary for Reach 2R: WS #2B/C POA

Inflow Area = 4.380 ac, 22.83% Impervious, Inflow Depth > 0.16" for 1-yr event
Inflow = 0.41 cfs @ 12.16 hrs, Volume= 0.058 af
Outflow = 0.41 cfs @ 12.16 hrs, Volume= 0.058 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Reach 2R: WS #2B/C POA



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Type II 24-hr 1-yr Rainfall=1.96"

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Summary for Pond 1P: Existing Wetlands-Reduced

Inflow Area = 8.970 ac, 9.92% Impervious, Inflow Depth > 0.31" for 1-yr event
 Inflow = 2.79 cfs @ 12.17 hrs, Volume= 0.235 af
 Outflow = 1.05 cfs @ 12.53 hrs, Volume= 0.173 af, Atten= 62%, Lag= 21.5 min
 Primary = 1.05 cfs @ 12.53 hrs, Volume= 0.173 af

Routing by Dyn-Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
 Peak Elev= 992.51' @ 12.53 hrs Surf.Area= 12,324 sf Storage= 3,267 cf

Plug-Flow detention time= 119.5 min calculated for 0.173 af (74% of inflow)
 Center-of-Mass det. time= 49.2 min (892.7 - 843.5)

Volume	Invert	Avail.Storage	Storage Description
#1	991.90'	21,366 cf	Custom Stage Data (Prismatic) Listed below (Recalc)

Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
991.90	0	0	0
992.00	539	27	27
992.50	12,019	3,140	3,166
993.00	30,390	10,602	13,769
993.25	30,390	7,598	21,366

Device	Routing	Invert	Outlet Devices
#1	Primary	992.42'	Asymmetrical Weir, C= 3.27 Offset (feet) -26.27 -25.00 0.00 20.00 26.27 Height (feet) 0.58 0.13 0.00 0.13 0.58

Primary OutFlow Max=1.04 cfs @ 12.53 hrs HW=992.51' TW=992.09' (Dynamic Tailwater)
 ↑1=Asymmetrical Weir (Weir Controls 1.04 cfs @ 0.39 fps)

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Type II 24-hr 1-yr Rainfall=1.96"

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Stage-Discharge for Pond 1P: Existing Wetlands-Reduced

Elevation (feet)	Primary (cfs)	Elevation (feet)	Primary (cfs)	Elevation (feet)	Primary (cfs)
991.90	0.00	992.43	0.00	992.96	50.64
991.91	0.00	992.44	0.03	992.97	52.32
991.92	0.00	992.45	0.07	992.98	54.01
991.93	0.00	992.46	0.14	992.99	55.73
991.94	0.00	992.47	0.25	993.00	57.47
991.95	0.00	992.48	0.40	993.01	59.06
991.96	0.00	992.49	0.59	993.02	60.52
991.97	0.00	992.50	0.82	993.03	61.91
991.98	0.00	992.51	1.10	993.04	63.25
991.99	0.00	992.52	1.43	993.05	64.54
992.00	0.00	992.53	1.82	993.06	65.79
992.01	0.00	992.54	2.26	993.07	67.01
992.02	0.00	992.55	2.76	993.08	68.19
992.03	0.00	992.56	3.32	993.09	69.35
992.04	0.00	992.57	3.92	993.10	70.48
992.05	0.00	992.58	4.57	993.11	71.59
992.06	0.00	992.59	5.26	993.12	72.68
992.07	0.00	992.60	5.98	993.13	73.75
992.08	0.00	992.61	6.74	993.14	74.80
992.09	0.00	992.62	7.54	993.15	75.83
992.10	0.00	992.63	8.37	993.16	76.85
992.11	0.00	992.64	9.23	993.17	77.85
992.12	0.00	992.65	10.12	993.18	78.83
992.13	0.00	992.66	11.05	993.19	79.81
992.14	0.00	992.67	12.00	993.20	80.76
992.15	0.00	992.68	12.98	993.21	81.71
992.16	0.00	992.69	13.99	993.22	82.64
992.17	0.00	992.70	15.03	993.23	83.56
992.18	0.00	992.71	16.09	993.24	84.47
992.19	0.00	992.72	17.19	993.25	85.37
992.20	0.00	992.73	18.30		
992.21	0.00	992.74	19.45		
992.22	0.00	992.75	20.62		
992.23	0.00	992.76	21.81		
992.24	0.00	992.77	23.03		
992.25	0.00	992.78	24.28		
992.26	0.00	992.79	25.55		
992.27	0.00	992.80	26.84		
992.28	0.00	992.81	28.16		
992.29	0.00	992.82	29.50		
992.30	0.00	992.83	30.86		
992.31	0.00	992.84	32.25		
992.32	0.00	992.85	33.66		
992.33	0.00	992.86	35.09		
992.34	0.00	992.87	36.55		
992.35	0.00	992.88	38.03		
992.36	0.00	992.89	39.53		
992.37	0.00	992.90	41.05		
992.38	0.00	992.91	42.59		
992.39	0.00	992.92	44.16		
992.40	0.00	992.93	45.75		
992.41	0.00	992.94	47.36		
992.42	0.00	992.95	48.99		

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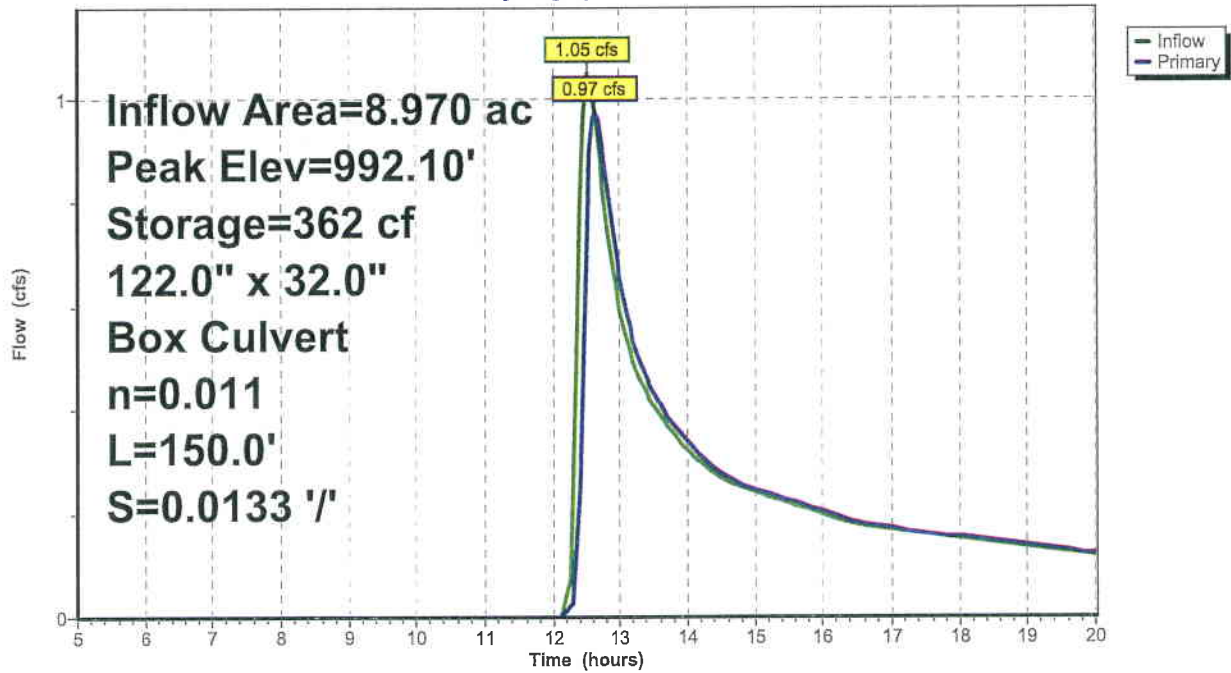
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Pond 2P: Box Culvert

Hydrograph



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Summary for Pond 3P: Stormwater Wetland

Inflow Area = 24.420 ac, 22.81% Impervious, Inflow Depth > 0.34" for 1-yr event
 Inflow = 7.89 cfs @ 12.10 hrs, Volume= 0.697 af
 Outflow = 0.31 cfs @ 20.00 hrs, Volume= 0.179 af, Atten= 96%, Lag= 473.8 min
 Primary = 0.31 cfs @ 20.00 hrs, Volume= 0.179 af
 Secondary = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af

Routing by Dyn-Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
 Peak Elev= 990.55' @ 20.00 hrs Surf.Area= 42,095 sf Storage= 22,531 cf

Plug-Flow detention time= 257.3 min calculated for 0.179 af (26% of inflow)
 Center-of-Mass det. time= 136.0 min (982.5 - 846.5)

Volume	Invert	Avail.Storage	Storage Description
#1	990.00'	169,355 cf	Custom Stage Data (Prismatic) Listed below (Recalc)
Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
990.00	39,300	0	0
993.00	54,445	140,618	140,618
993.50	60,505	28,738	169,355

Device	Routing	Invert	Outlet Devices
#1	Primary	990.00'	18.0" Round Culvert x3 X 3.00 L= 50.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 990.00' / 989.75' S= 0.0050 '/ Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 1.77 sf
#2	Device 1	990.00'	3.0" Vert. Orificex2 X 2.00 C= 0.600
#3	Device 1	992.00'	36.0" x 36.0" Horiz. Gate#1 C= 0.600 Limited to weir flow at low heads
#4	Device 1	992.00'	36.0" x 60.0" Horiz. Gate#2 C= 0.600 Limited to weir flow at low heads
#5	Secondary	993.00'	32.0' long x 10.0' breadth Broad-Crested Rectangular Weir Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 Coef. (English) 2.49 2.56 2.70 2.69 2.68 2.69 2.67 2.64

Primary OutFlow Max=0.31 cfs @ 20.00 hrs HW=990.55' TW=0.00' (Dynamic Tailwater)

1=Culvert x3 (Passes 0.31 cfs of 3.17 cfs potential flow)
 2=Orificex2 (Orifice Controls 0.31 cfs @ 3.15 fps)
 3=Gate#1 (Controls 0.00 cfs)
 4=Gate#2 (Controls 0.00 cfs)

Secondary OutFlow Max=0.00 cfs @ 5.00 hrs HW=990.00' (Free Discharge)

5=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

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Stage-Discharge for Pond 3P: Stormwater Wetland

Elevation (feet)	Discharge (cfs)	Primary (cfs)	Secondary (cfs)	Elevation (feet)	Discharge (cfs)	Primary (cfs)	Secondary (cfs)
990.00	0.00	0.00	0.00	992.65	27.78	27.78	0.00
990.05	0.01	0.01	0.00	992.70	28.14	28.14	0.00
990.10	0.04	0.04	0.00	992.75	28.50	28.50	0.00
990.15	0.08	0.08	0.00	992.80	28.85	28.85	0.00
990.20	0.13	0.13	0.00	992.85	29.20	29.20	0.00
990.25	0.17	0.17	0.00	992.90	29.55	29.55	0.00
990.30	0.20	0.20	0.00	992.95	29.89	29.89	0.00
990.35	0.22	0.22	0.00	993.00	30.23	30.23	0.00
990.40	0.25	0.25	0.00	993.05	31.45	30.56	0.89
990.45	0.27	0.27	0.00	993.10	33.41	30.89	2.52
990.50	0.29	0.29	0.00	993.15	35.85	31.22	4.63
990.55	0.31	0.31	0.00	993.20	38.67	31.54	7.13
990.60	0.33	0.33	0.00	993.25	41.89	31.86	10.03
990.65	0.34	0.34	0.00	993.30	45.46	32.18	13.28
990.70	0.36	0.36	0.00	993.35	49.34	32.49	16.85
990.75	0.37	0.37	0.00	993.40	53.53	32.81	20.72
990.80	0.39	0.39	0.00	993.45	58.18	33.11	25.07
990.85	0.40	0.40	0.00	993.50	63.17	33.42	29.76
990.90	0.42	0.42	0.00				
990.95	0.43	0.43	0.00				
991.00	0.44	0.44	0.00				
991.05	0.45	0.45	0.00				
991.10	0.47	0.47	0.00				
991.15	0.48	0.48	0.00				
991.20	0.49	0.49	0.00				
991.25	0.50	0.50	0.00				
991.30	0.51	0.51	0.00				
991.35	0.52	0.52	0.00				
991.40	0.53	0.53	0.00				
991.45	0.54	0.54	0.00				
991.50	0.55	0.55	0.00				
991.55	0.56	0.56	0.00				
991.60	0.57	0.57	0.00				
991.65	0.58	0.58	0.00				
991.70	0.59	0.59	0.00				
991.75	0.60	0.60	0.00				
991.80	0.61	0.61	0.00				
991.85	0.62	0.62	0.00				
991.90	0.63	0.63	0.00				
991.95	0.64	0.64	0.00				
992.00	0.65	0.65	0.00				
992.05	1.68	1.68	0.00				
992.10	3.56	3.56	0.00				
992.15	5.99	5.99	0.00				
992.20	8.87	8.87	0.00				
992.25	12.13	12.13	0.00				
992.30	15.74	15.74	0.00				
992.35	19.66	19.66	0.00				
992.40	23.88	23.88	0.00				
992.45	26.28	26.28	0.00				
992.50	26.66	26.66	0.00				
992.55	27.04	27.04	0.00				
992.60	27.41	27.41	0.00				

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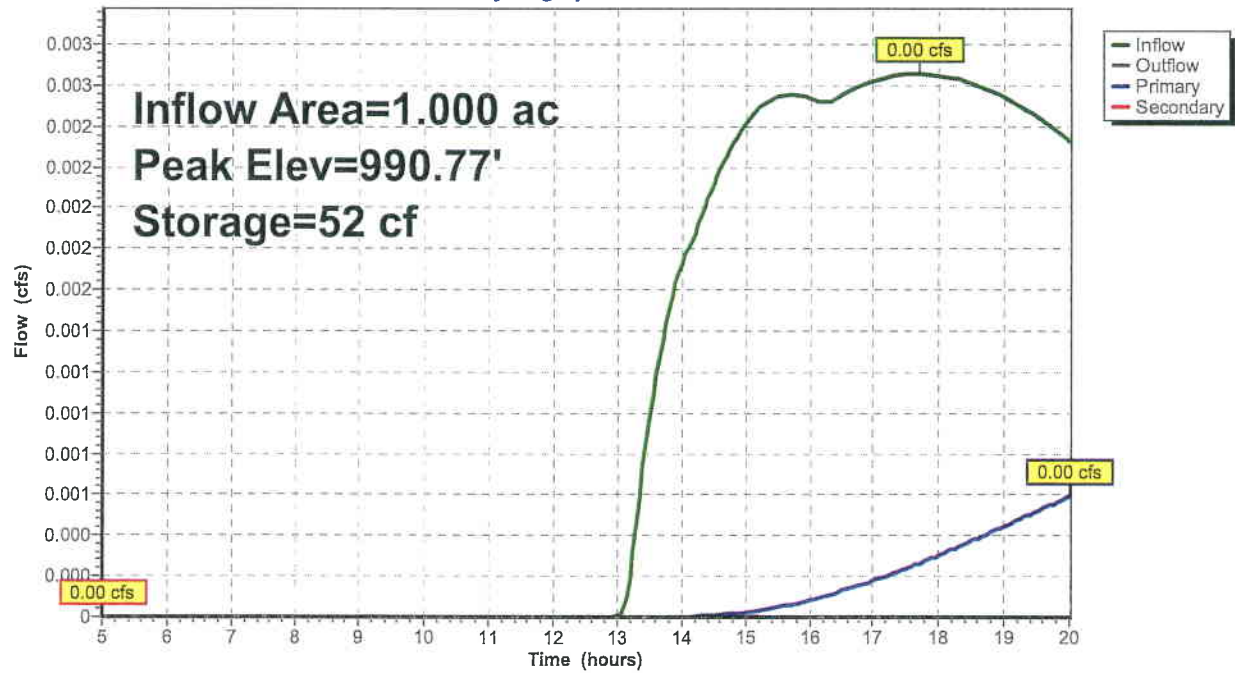
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Pond 4P: Wetland #2

Hydrograph



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Summary for Pond 5P: Underground Detention

Inflow Area = 0.170 ac, 88.24% Impervious, Inflow Depth > 1.27" for 1-yr event
 Inflow = 0.38 cfs @ 11.97 hrs, Volume= 0.018 af
 Outflow = 0.15 cfs @ 12.09 hrs, Volume= 0.018 af, Atten= 60%, Lag= 7.2 min
 Primary = 0.15 cfs @ 12.09 hrs, Volume= 0.018 af

Routing by Dyn-Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
 Peak Elev= 981.10' @ 12.09 hrs Surf.Area= 0.012 ac Storage= 0.005 af

Plug-Flow detention time= 17.1 min calculated for 0.018 af (99% of inflow)
 Center-of-Mass det. time= 14.4 min (779.3 - 764.9)

Volume	Invert	Avail.Storage	Storage Description
#1	980.55'	0.029 af	30.0" Round Pipe Storage x 2 L= 130.0'

Device	Routing	Invert	Outlet Devices
#1	Primary	980.35'	15.0" Round Culvert L= 95.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 980.35' / 979.30' S= 0.0111 ' /' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 1.23 sf
#2	Device 1	980.55'	3.0" Vert. Orifice C= 0.600
#3	Device 1	982.95'	2.0' long Sharp-Crested Rectangular Weir 2 End Contraction(s)

Primary OutFlow Max=0.15 cfs @ 12.09 hrs HW=981.10' TW=0.00' (Dynamic Tailwater)

- ↑ **1=Culvert** (Passes 0.15 cfs of 1.80 cfs potential flow)
- ↑ **2=Orifice** (Orifice Controls 0.15 cfs @ 3.14 fps)
- ↑ **3=Sharp-Crested Rectangular Weir** (Controls 0.00 cfs)

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Stage-Discharge for Pond 5P: Underground Detention

Elevation (feet)	Primary (cfs)	Elevation (feet)	Primary (cfs)	Elevation (feet)	Primary (cfs)
980.55	0.00	981.61	0.23	982.67	0.33
980.57	0.00	981.63	0.23	982.69	0.34
980.59	0.00	981.65	0.23	982.71	0.34
980.61	0.01	981.67	0.24	982.73	0.34
980.63	0.01	981.69	0.24	982.75	0.34
980.65	0.02	981.71	0.24	982.77	0.34
980.67	0.03	981.73	0.24	982.79	0.34
980.69	0.04	981.75	0.25	982.81	0.35
980.71	0.05	981.77	0.25	982.83	0.35
980.73	0.05	981.79	0.25	982.85	0.35
980.75	0.06	981.81	0.25	982.87	0.35
980.77	0.07	981.83	0.25	982.89	0.35
980.79	0.08	981.85	0.26	982.91	0.35
980.81	0.09	981.87	0.26	982.93	0.35
980.83	0.09	981.89	0.26	982.95	0.36
980.85	0.10	981.91	0.26	982.97	0.38
980.87	0.10	981.93	0.26	982.99	0.41
980.89	0.11	981.95	0.27	983.01	0.46
980.91	0.11	981.97	0.27	983.03	0.51
980.93	0.12	981.99	0.27	983.05	0.57
980.95	0.12	982.01	0.27		
980.97	0.13	982.03	0.28		
980.99	0.13	982.05	0.28		
981.01	0.14	982.07	0.28		
981.03	0.14	982.09	0.28		
981.05	0.14	982.11	0.28		
981.07	0.15	982.13	0.29		
981.09	0.15	982.15	0.29		
981.11	0.16	982.17	0.29		
981.13	0.16	982.19	0.29		
981.15	0.16	982.21	0.29		
981.17	0.17	982.23	0.29		
981.19	0.17	982.25	0.30		
981.21	0.17	982.27	0.30		
981.23	0.18	982.29	0.30		
981.25	0.18	982.31	0.30		
981.27	0.18	982.33	0.30		
981.29	0.19	982.35	0.31		
981.31	0.19	982.37	0.31		
981.33	0.19	982.39	0.31		
981.35	0.19	982.41	0.31		
981.37	0.20	982.43	0.31		
981.39	0.20	982.45	0.31		
981.41	0.20	982.47	0.32		
981.43	0.21	982.49	0.32		
981.45	0.21	982.51	0.32		
981.47	0.21	982.53	0.32		
981.49	0.21	982.55	0.32		
981.51	0.22	982.57	0.33		
981.53	0.22	982.59	0.33		
981.55	0.22	982.61	0.33		
981.57	0.22	982.63	0.33		
981.59	0.23	982.65	0.33		

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Stage-Discharge for Pond 9P: DI #14

Elevation (feet)	Discharge (cfs)	Primary (cfs)	Secondary (cfs)	Elevation (feet)	Discharge (cfs)	Primary (cfs)	Secondary (cfs)
979.30	0.00	0.00	0.00	981.95	3.52	3.52	0.00
979.35	0.00	0.00	0.00	982.00	3.58	3.58	0.00
979.40	0.01	0.01	0.00	982.05	3.64	3.64	0.00
979.45	0.02	0.02	0.00	982.10	3.70	3.70	0.00
979.50	0.04	0.04	0.00	982.15	3.76	3.76	0.00
979.55	0.06	0.06	0.00	982.20	3.82	3.82	0.00
979.60	0.09	0.09	0.00	982.25	3.88	3.88	0.00
979.65	0.12	0.12	0.00	982.30	3.93	3.93	0.00
979.70	0.16	0.16	0.00	982.35	3.99	3.99	0.00
979.75	0.20	0.20	0.00	982.40	4.05	4.05	0.00
979.80	0.26	0.26	0.00	982.45	4.10	4.10	0.00
979.85	0.31	0.31	0.00	982.50	4.15	4.15	0.00
979.90	0.37	0.37	0.00	982.55	4.21	4.21	0.00
979.95	0.44	0.44	0.00	982.60	4.26	4.26	0.00
980.00	0.52	0.52	0.00	982.65	4.31	4.31	0.00
980.05	0.59	0.59	0.00	982.70	4.36	4.36	0.00
980.10	0.68	0.68	0.00	982.75	4.41	4.41	0.00
980.15	0.77	0.77	0.00	982.80	4.46	4.46	0.00
980.20	0.86	0.86	0.00	982.85	4.51	4.51	0.00
980.25	0.95	0.95	0.00	982.90	4.56	4.56	0.00
980.30	1.05	1.05	0.00	982.95	4.61	4.61	0.00
980.35	1.15	1.15	0.00	983.00	4.66	4.66	0.00
980.40	1.26	1.26	0.00	983.05	4.70	4.70	0.00
980.45	1.36	1.36	0.00	983.10	4.75	4.75	0.00
980.50	1.47	1.47	0.00	983.15	4.80	4.80	0.00
980.55	1.58	1.58	0.00	983.20	4.84	4.84	0.00
980.60	1.69	1.69	0.00	983.25	4.89	4.89	0.00
980.65	1.80	1.80	0.00	983.30	4.93	4.93	0.00
980.70	1.91	1.91	0.00				
980.75	2.02	2.02	0.00				
980.80	2.12	2.12	0.00				
980.85	2.22	2.22	0.00				
980.90	2.32	2.32	0.00				
980.95	2.41	2.41	0.00				
981.00	2.49	2.49	0.00				
981.05	2.56	2.56	0.00				
981.10	2.62	2.62	0.00				
981.15	2.67	2.67	0.00				
981.20	2.70	2.70	0.00				
981.25	2.70	2.70	0.00				
981.30	2.58	2.58	0.00				
981.35	2.66	2.66	0.00				
981.40	2.74	2.74	0.00				
981.45	2.82	2.82	0.00				
981.50	2.90	2.90	0.00				
981.55	2.97	2.97	0.00				
981.60	3.05	3.05	0.00				
981.65	3.12	3.12	0.00				
981.70	3.19	3.19	0.00				
981.75	3.26	3.26	0.00				
981.80	3.33	3.33	0.00				
981.85	3.39	3.39	0.00				
981.90	3.46	3.46	0.00				

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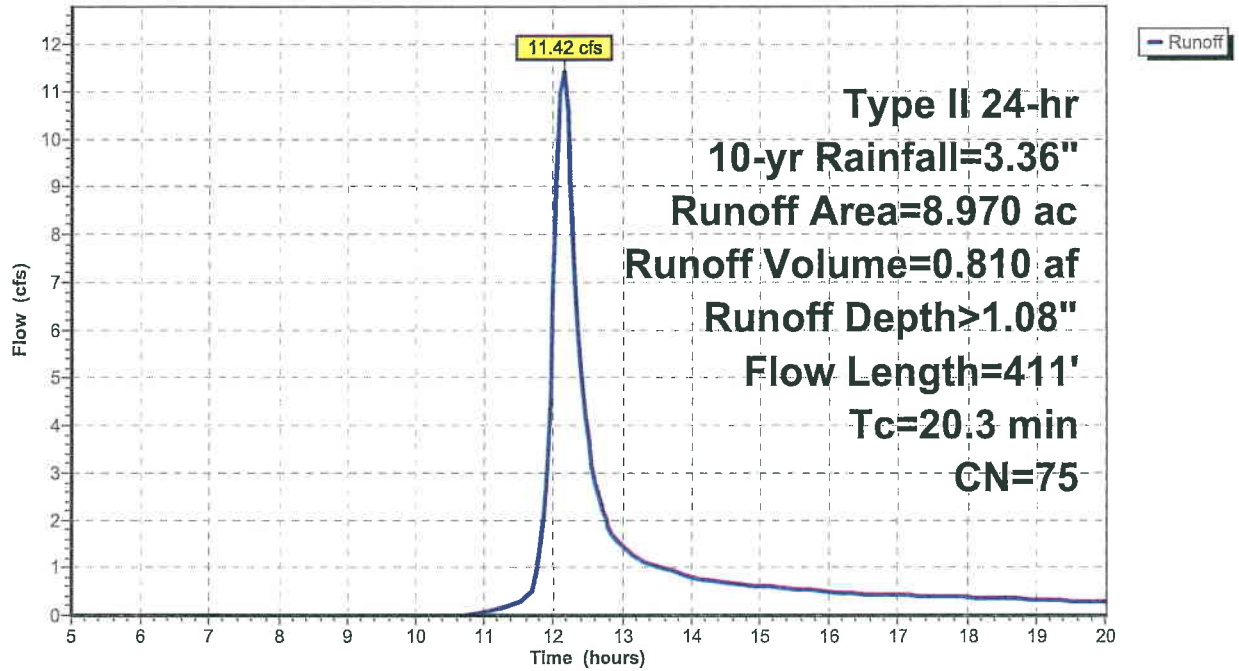
Type II 24-hr 10-yr Rainfall=3.36"

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Subcatchment 1S: WS #1A

Hydrograph



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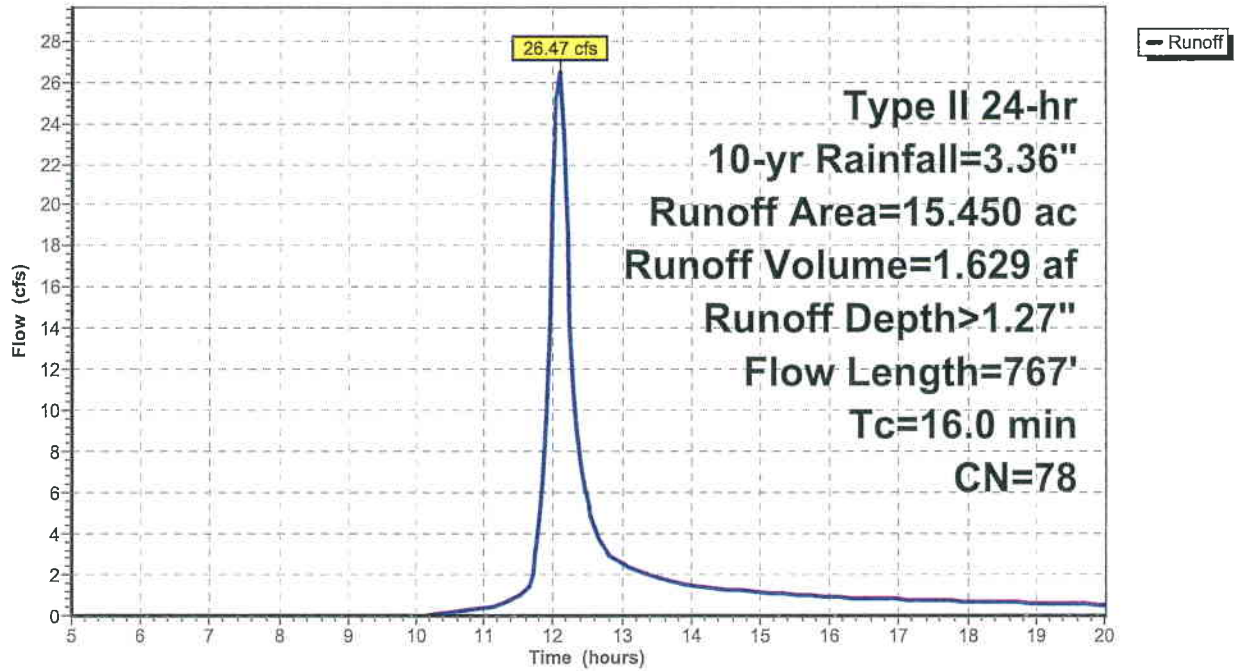
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Subcatchment 2S: WS #1B (CENTER)

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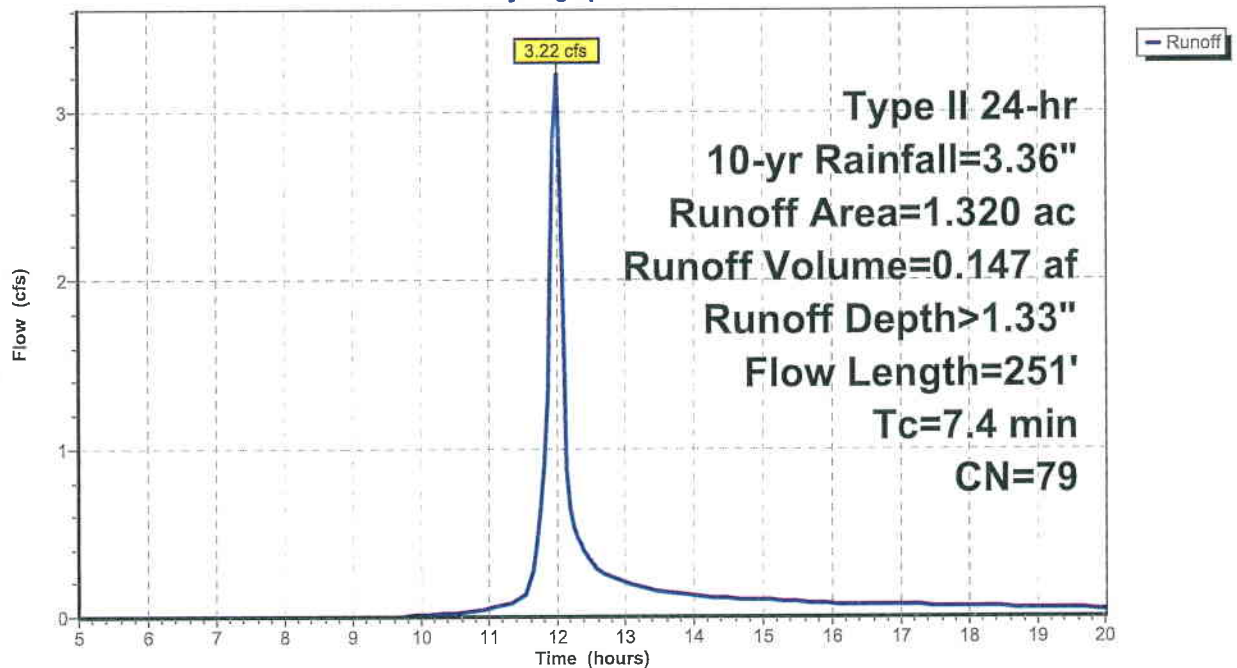
Summary for Subcatchment 4S: WS #1D

Runoff = 3.22 cfs @ 11.99 hrs, Volume= 0.147 af, Depth> 1.33"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
Type II 24-hr 10-yr Rainfall=3.36"

Area (ac)	CN	Description
0.680	78	Meadow, non-grazed, HSG D
0.640	80	>75% Grass cover, Good, HSG D
1.320	79	Weighted Average
1.320		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
4.5	65	0.0900	0.24		Sheet Flow, Grass: Short n= 0.150 P2= 2.31"
2.9	186	0.0044	1.07		Shallow Concentrated Flow, Unpaved Kv= 16.1 fps
7.4	251	Total			

Subcatchment 4S: WS #1D**Hydrograph**

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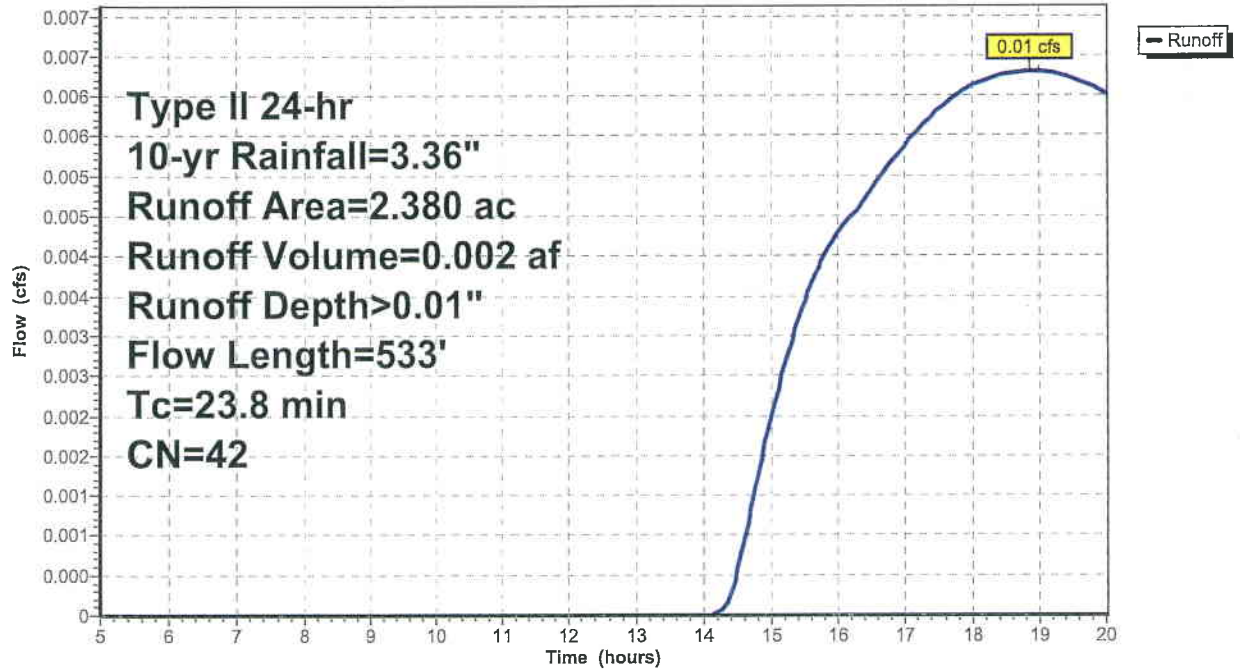
Type II 24-hr 10-yr Rainfall=3.36"

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Subcatchment 5S: WS #2A

Hydrograph



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Summary for Subcatchment 7S: WS #2B

Runoff = 3.36 cfs @ 12.10 hrs, Volume= 0.224 af, Depth> 0.64"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
Type II 24-hr 10-yr Rainfall=3.36"

Area (ac)	CN	Description
0.850	98	Paved parking, HSG D
0.100	30	Woods, Good, HSG A
0.350	39	>75% Grass cover, Good, HSG A
2.910	61	>75% Grass cover, Good, HSG B
4.210	66	Weighted Average
3.360		79.81% Pervious Area
0.850		20.19% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
9.8	100	0.0300	0.17		Sheet Flow, Grass: Short n= 0.150 P2= 2.31"
1.3	180	0.0210	2.33		Shallow Concentrated Flow, Unpaved Kv= 16.1 fps
1.7	206	0.0100	2.03		Shallow Concentrated Flow, Paved Kv= 20.3 fps
2.5	470	0.0100	3.09	5.46	Pipe Channel, 18.0" Round Area= 1.8 sf Perim= 4.7' r= 0.38' n= 0.025 Corrugated metal
15.3	956	Total			

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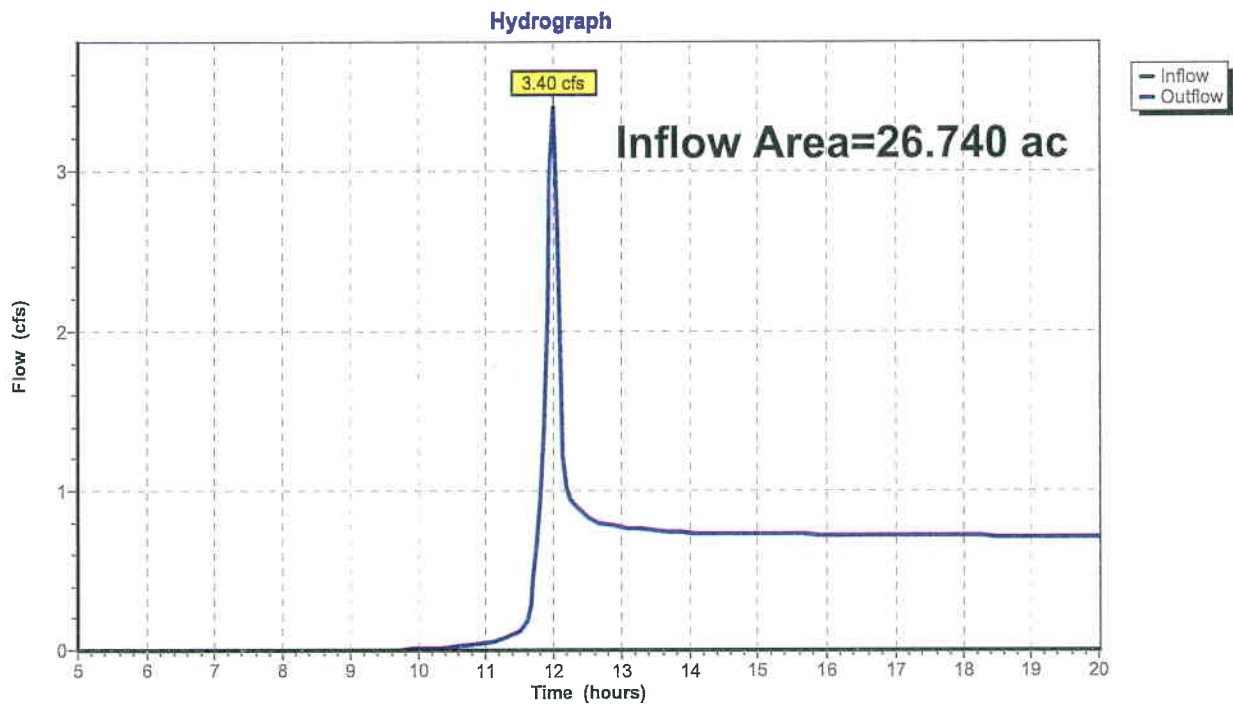
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Summary for Reach 1R: WS #1 POA

Inflow Area = 26.740 ac, 21.13% Impervious, Inflow Depth > 0.25" for 10-yr event
Inflow = 3.40 cfs @ 11.99 hrs, Volume= 0.558 af
Outflow = 3.40 cfs @ 11.99 hrs, Volume= 0.558 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Reach 1R: WS #1 POA



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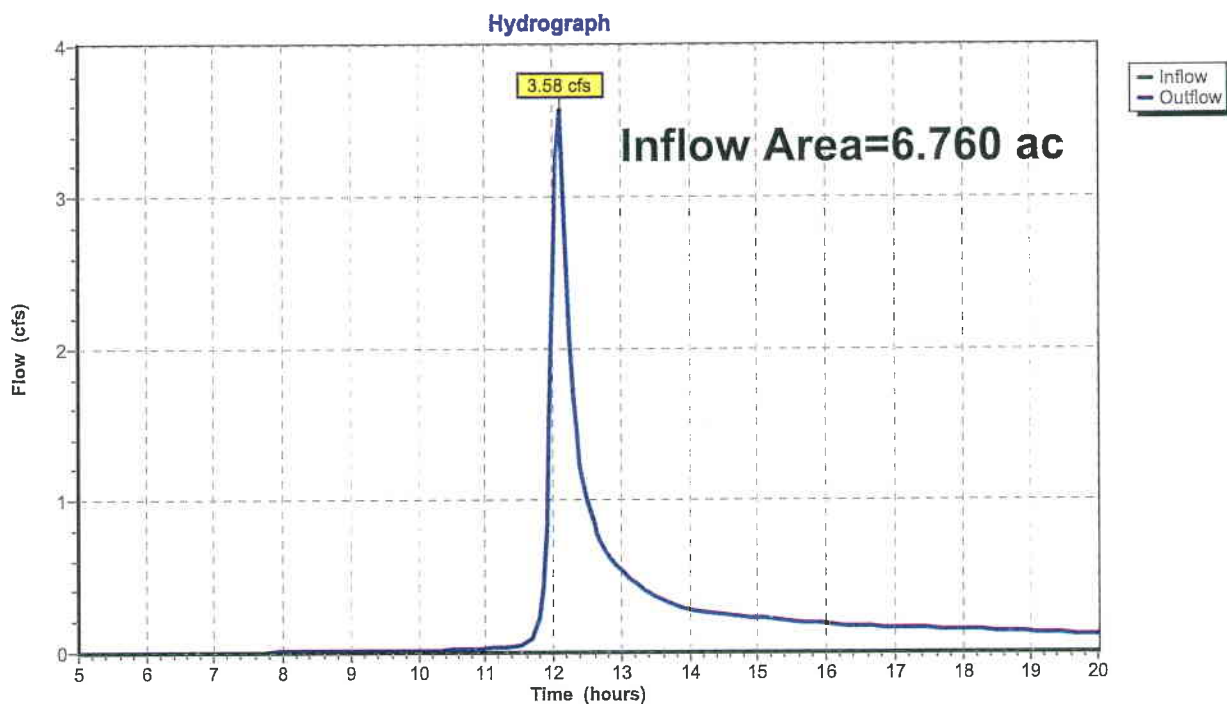
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Summary for Reach 11R: WS #2 POA

Inflow Area = 6.760 ac, 17.75% Impervious, Inflow Depth > 0.46" for 10-yr event
Inflow = 3.58 cfs @ 12.10 hrs, Volume= 0.262 af
Outflow = 3.58 cfs @ 12.10 hrs, Volume= 0.262 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Reach 11R: WS #2 POA



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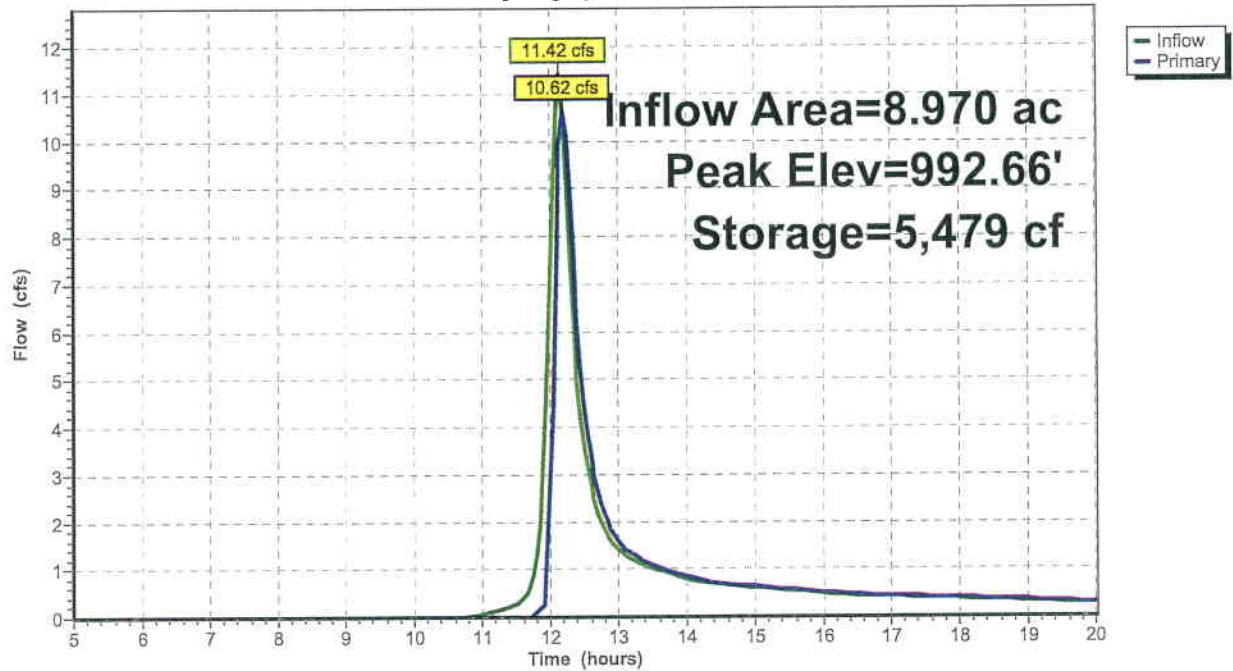
Type II 24-hr 10-yr Rainfall=3.36"

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Pond 1P: Existing Wetlands-Reduced

Hydrograph



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Summary for Pond 2P: Box Culvert

Inflow Area = 8.970 ac, 9.92% Impervious, Inflow Depth > 1.00" for 10-yr event
 Inflow = 10.62 cfs @ 12.20 hrs, Volume= 0.745 af
 Outflow = 10.29 cfs @ 12.25 hrs, Volume= 0.739 af, Atten= 3%, Lag= 2.5 min
 Primary = 10.29 cfs @ 12.25 hrs, Volume= 0.739 af

Routing by Dyn-Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
 Peak Elev= 992.46' @ 12.25 hrs Surf.Area= 4,119 sf Storage= 1,818 cf

Plug-Flow detention time= 5.9 min calculated for 0.736 af (99% of inflow)
 Center-of-Mass det. time= 2.9 min (832.2 - 829.3)

Volume	Invert	Avail.Storage	Storage Description
#1	992.00'	4,045 cf	Custom Stage Data (Prismatic) Listed below (Recalc)

Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
992.00	3,730	0	0
992.50	4,150	1,970	1,970
993.00	4,150	2,075	4,045

Device	Routing	Invert	Outlet Devices
#1	Primary	992.00'	122.0" W x 32.0" H Box Culvert L= 150.0' Box, headwall w/3 square edges, Ke= 0.500 Inlet / Outlet Invert= 992.00' / 990.00' S= 0.0133 ' S= 0.0133 ' Cc= 0.900 n= 0.011 Concrete pipe, straight & clean, Flow Area= 27.11 sf

Primary OutFlow Max=10.24 cfs @ 12.25 hrs HW=992.46' TW=990.86' (Dynamic Tailwater)

↑ **1=Culvert** (Inlet Controls 10.24 cfs @ 2.18 fps)

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Type II 24-hr 10-yr Rainfall=3.36"

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Stage-Discharge for Pond 2P: Box Culvert

Elevation (feet)	Primary (cfs)	Elevation (feet)	Primary (cfs)	Elevation (feet)	Primary (cfs)
992.00	0.00	993.06	35.62	994.12	100.74
992.02	0.09	993.08	36.63	994.14	102.17
992.04	0.26	993.10	37.65	994.16	103.60
992.06	0.48	993.12	38.68	994.18	105.04
992.08	0.74	993.14	39.72	994.20	106.49
992.10	1.03	993.16	40.77	994.22	107.95
992.12	1.36	993.18	41.83	994.24	109.41
992.14	1.71	993.20	42.90	994.26	110.88
992.16	2.09	993.22	43.98	994.28	112.35
992.18	2.49	993.24	45.06	994.30	113.83
992.20	2.92	993.26	46.16	994.32	115.32
992.22	3.37	993.28	47.26	994.34	116.82
992.24	3.84	993.30	48.37	994.36	118.32
992.26	4.33	993.32	49.49	994.38	119.82
992.28	4.84	993.34	50.62	994.40	121.34
992.30	5.36	993.36	51.76	994.42	122.86
992.32	5.91	993.38	52.91	994.44	124.38
992.34	6.47	993.40	54.06	994.46	125.92
992.36	7.05	993.42	55.22	994.48	127.46
992.38	7.64	993.44	56.39	994.50	129.00
992.40	8.26	993.46	57.57	994.52	130.55
992.42	8.88	993.48	58.76	994.54	132.11
992.44	9.52	993.50	59.95	994.56	133.67
992.46	10.18	993.52	61.16	994.58	135.24
992.48	10.85	993.54	62.37	994.60	136.82
992.50	11.54	993.56	63.59	994.62	138.40
992.52	12.24	993.58	64.81	994.64	139.99
992.54	12.95	993.60	66.05	994.66	141.58
992.56	13.68	993.62	67.29		
992.58	14.42	993.64	68.54		
992.60	15.17	993.66	69.80		
992.62	15.93	993.68	71.06		
992.64	16.71	993.70	72.34		
992.66	17.50	993.72	73.62		
992.68	18.30	993.74	74.90		
992.70	19.11	993.76	76.20		
992.72	19.94	993.78	77.50		
992.74	20.77	993.80	78.81		
992.76	21.62	993.82	80.13		
992.78	22.48	993.84	81.45		
992.80	23.35	993.86	82.78		
992.82	24.23	993.88	84.12		
992.84	25.12	993.90	85.47		
992.86	26.03	993.92	86.82		
992.88	26.94	993.94	88.18		
992.90	27.86	993.96	89.55		
992.92	28.80	993.98	90.92		
992.94	29.74	994.00	92.31		
992.96	30.70	994.02	93.69		
992.98	31.66	994.04	95.09		
993.00	32.63	994.06	96.49		
993.02	33.62	994.08	97.90		
993.04	34.61	994.10	99.31		

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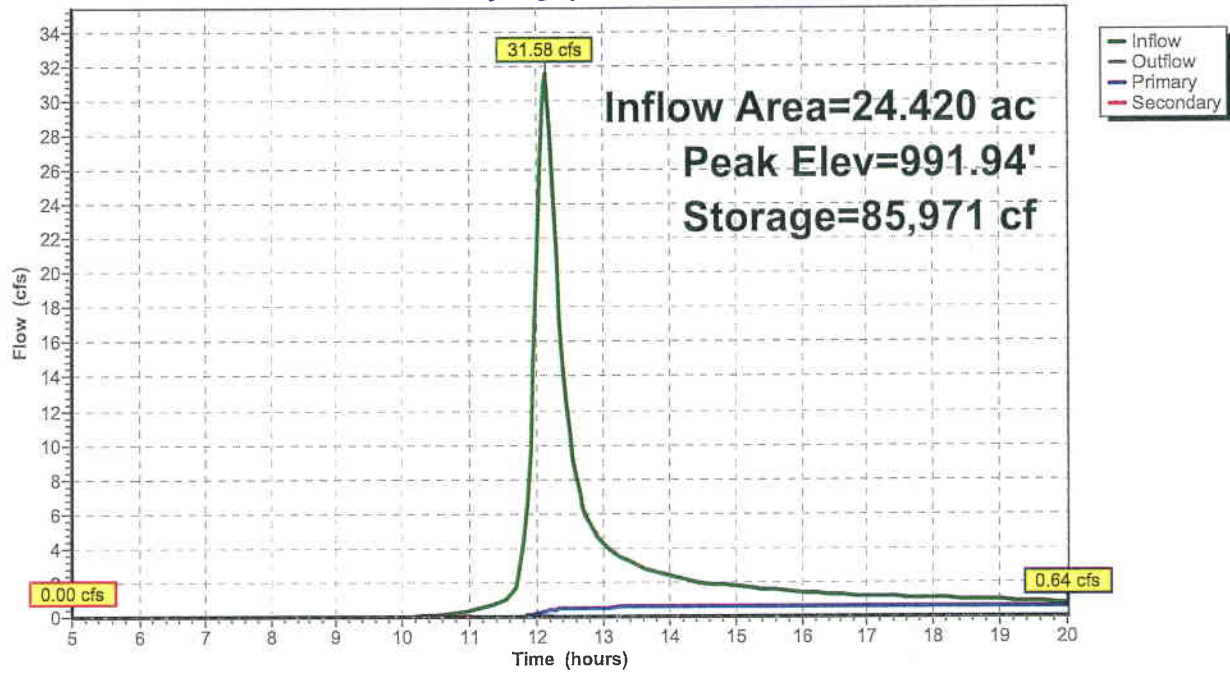
Type II 24-hr 10-yr Rainfall=3.36"

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Pond 3P: Stormwater Wetland

Hydrograph



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Summary for Pond 4P: Wetland #2

Inflow Area = 1.000 ac, 8.00% Impervious, Inflow Depth > 0.31" for 10-yr event
 Inflow = 0.28 cfs @ 12.11 hrs, Volume= 0.026 af
 Outflow = 0.03 cfs @ 14.35 hrs, Volume= 0.018 af, Atten= 88%, Lag= 134.3 min
 Primary = 0.03 cfs @ 14.35 hrs, Volume= 0.018 af
 Secondary = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af

Routing by Dyn-Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
 Peak Elev= 990.88' @ 14.35 hrs Surf.Area= 3,657 sf Storage= 451 cf

Plug-Flow detention time= 178.6 min calculated for 0.018 af (69% of inflow)
 Center-of-Mass det. time= 95.5 min (960.4 - 864.9)

Volume	Invert	Avail.Storage	Storage Description
#1	990.75'	10,990 cf	Custom Stage Data (Prismatic) Listed below (Recalc)
Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
990.75	3,160	0	0
991.00	4,100	908	908
992.00	5,025	4,563	5,470
993.00	6,015	5,520	10,990

Device	Routing	Invert	Outlet Devices
#1	Primary	990.75'	8.0" Round Culvert L= 25.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 990.75' / 990.50' S= 0.0100 ' / ' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.35 sf
#2	Device 1	990.75'	3.0" Vert. Orifice C= 0.600
#3	Device 1	992.50'	36.0" x 36.0" Horiz. Grate C= 0.600 Limited to weir flow at low heads
#4	Secondary	993.00'	32.0' long x 10.0' breadth Broad-Crested Rectangular Weir Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 Coef. (English) 2.49 2.56 2.70 2.69 2.68 2.69 2.67 2.64

Primary OutFlow Max=0.03 cfs @ 14.35 hrs HW=990.88' TW=0.00' (Dynamic Tailwater)

1=Culvert (Passes 0.03 cfs of 0.05 cfs potential flow)
 2=Orifice (Orifice Controls 0.03 cfs @ 1.24 fps)
 3=Grate (Controls 0.00 cfs)

Secondary OutFlow Max=0.00 cfs @ 5.00 hrs HW=990.75' (Free Discharge)

4=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

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Type II 24-hr 10-yr Rainfall=3.36"

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Stage-Discharge for Pond 4P: Wetland #2

Elevation (feet)	Discharge (cfs)	Primary (cfs)	Secondary (cfs)
990.75	0.00	0.00	0.00
990.80	0.01	0.01	0.00
990.85	0.02	0.02	0.00
990.90	0.04	0.04	0.00
990.95	0.06	0.06	0.00
991.00	0.08	0.08	0.00
991.05	0.10	0.10	0.00
991.10	0.11	0.11	0.00
991.15	0.12	0.12	0.00
991.20	0.13	0.13	0.00
991.25	0.14	0.14	0.00
991.30	0.15	0.15	0.00
991.35	0.16	0.16	0.00
991.40	0.17	0.17	0.00
991.45	0.18	0.18	0.00
991.50	0.19	0.19	0.00
991.55	0.19	0.19	0.00
991.60	0.20	0.20	0.00
991.65	0.21	0.21	0.00
991.70	0.21	0.21	0.00
991.75	0.22	0.22	0.00
991.80	0.23	0.23	0.00
991.85	0.23	0.23	0.00
991.90	0.24	0.24	0.00
991.95	0.25	0.25	0.00
992.00	0.25	0.25	0.00
992.05	0.26	0.26	0.00
992.10	0.26	0.26	0.00
992.15	0.27	0.27	0.00
992.20	0.27	0.27	0.00
992.25	0.28	0.28	0.00
992.30	0.28	0.28	0.00
992.35	0.29	0.29	0.00
992.40	0.29	0.29	0.00
992.45	0.30	0.30	0.00
992.50	0.30	0.30	0.00
992.55	0.74	0.74	0.00
992.60	1.55	1.55	0.00
992.65	1.66	1.66	0.00
992.70	1.69	1.69	0.00
992.75	1.71	1.71	0.00
992.80	1.74	1.74	0.00
992.85	1.76	1.76	0.00
992.90	1.79	1.79	0.00
992.95	1.81	1.81	0.00
993.00	1.84	1.84	0.00

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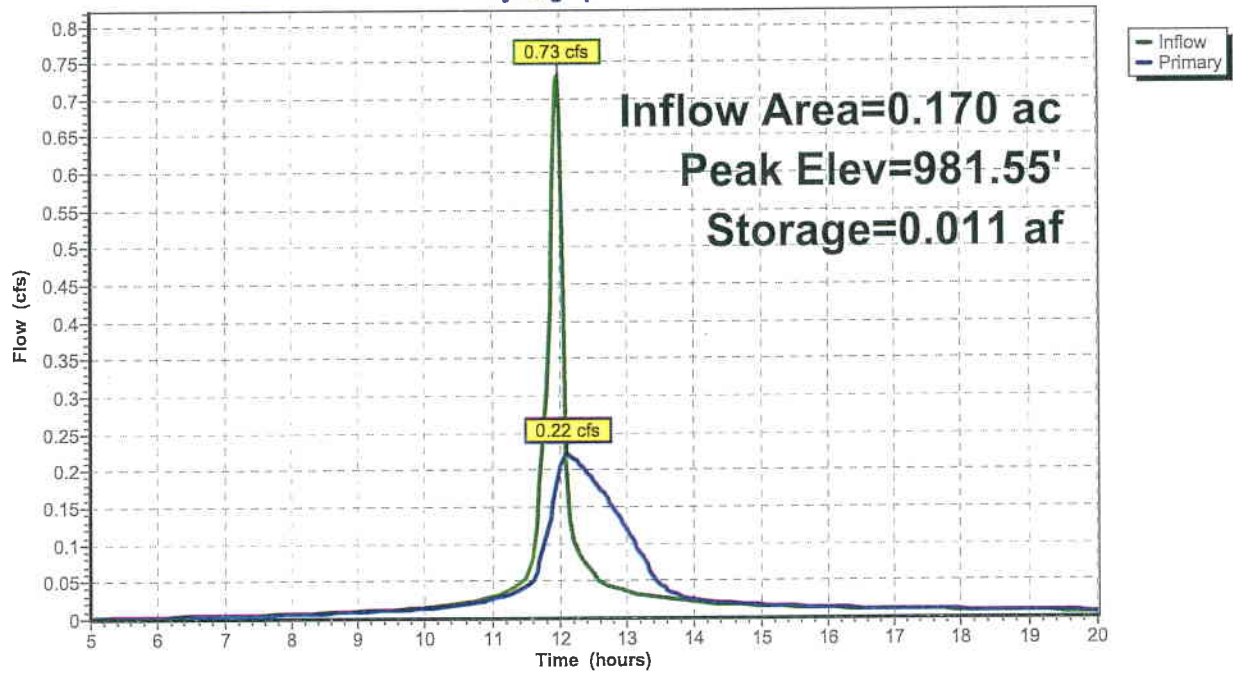
Type II 24-hr 10-yr Rainfall=3.36"

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Pond 5P: Underground Detention

Hydrograph



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Summary for Pond 9P: DI #14

Inflow Area = 4.380 ac, 22.83% Impervious, Inflow Depth > 0.71" for 10-yr event
Inflow = 3.58 cfs @ 12.10 hrs, Volume= 0.259 af
Outflow = 3.58 cfs @ 12.10 hrs, Volume= 0.259 af, Atten= 0%, Lag= 0.0 min
Primary = 3.58 cfs @ 12.10 hrs, Volume= 0.259 af
Secondary = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af

Routing by Dyn-Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Peak Elev= 982.00' @ 12.10 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	979.30'	18.0" Round Existing Culvert L= 308.0' CMP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 979.30' / 979.05' S= 0.0008 '/' Cc= 0.900 n= 0.025 Corrugated metal, Flow Area= 1.77 sf
#2	Secondary	983.30'	17.2" x 17.2" Horiz. Grate EJIW 5115M2 C= 0.600 Limited to weir flow at low heads

Primary OutFlow Max=3.58 cfs @ 12.10 hrs HW=981.99' TW=0.00' (Dynamic Tailwater)

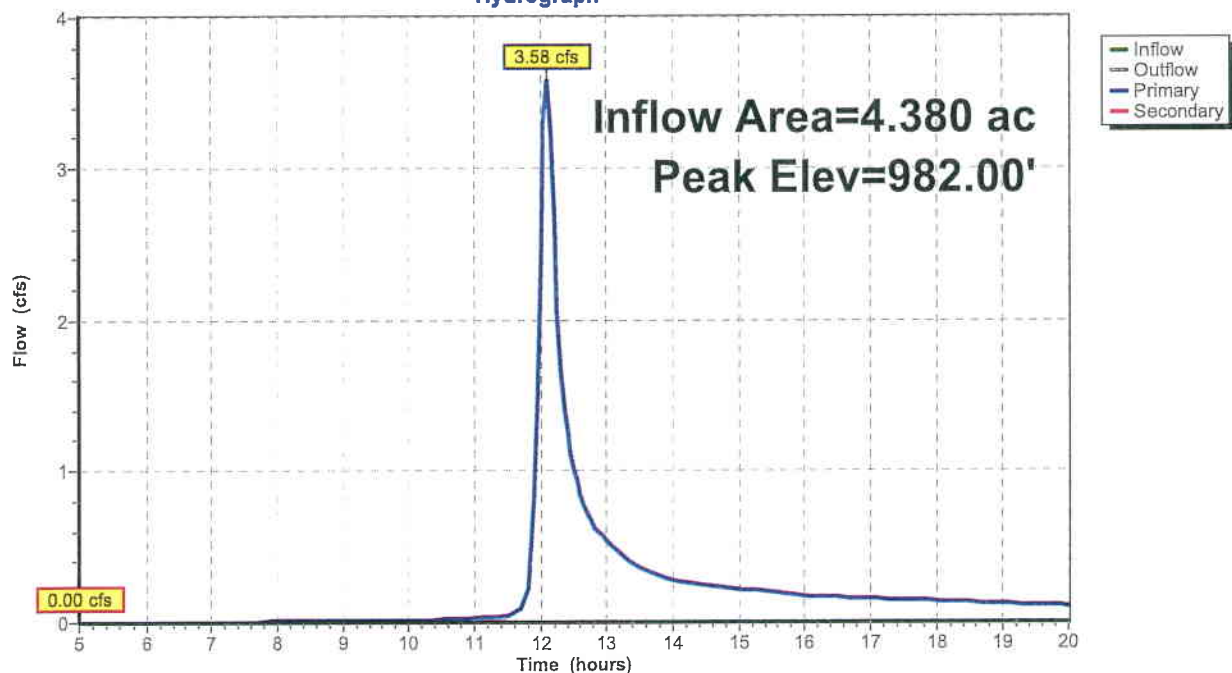
↑ **1=Existing Culvert** (Barrel Controls 3.58 cfs @ 2.02 fps)

Secondary OutFlow Max=0.00 cfs @ 5.00 hrs HW=979.31' TW=0.00' (Dynamic Tailwater)

↑ **2=Grate EJIW 5115M2** (Controls 0.00 cfs)

Pond 9P: DI #14

Hydrograph



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Type II 24-hr 100-yr Rainfall=5.73"

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Summary for Subcatchment 1S: WS #1A

Runoff = 30.02 cfs @ 12.13 hrs, Volume= 2.096 af, Depth> 2.80"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
Type II 24-hr 100-yr Rainfall=5.73"

Area (ac)	CN	Description
0.890	98	Paved parking, HSG D
0.260	30	Woods, Good, HSG A
1.580	77	Woods, Good, HSG D
1.100	39	>75% Grass cover, Good, HSG A
5.140	80	>75% Grass cover, Good, HSG D
8.970	75	Weighted Average
8.080		90.08% Pervious Area
0.890		9.92% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
0.5	18	0.0100	0.63		Sheet Flow, Smooth surfaces n= 0.011 P2= 2.31"
13.0	82	0.0100	0.11		Sheet Flow, Grass: Short n= 0.150 P2= 2.31"
1.9	171	0.0090	1.53		Shallow Concentrated Flow, Unpaved Kv= 16.1 fps
4.9	140	0.0090	0.47		Shallow Concentrated Flow, Woodland Kv= 5.0 fps
20.3	411	Total			

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Type II 24-hr 100-yr Rainfall=5.73"

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Summary for Subcatchment 2S: WS #1B (CENTER)

Runoff = 64.12 cfs @ 12.08 hrs, Volume= 3.975 af, Depth> 3.09"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
Type II 24-hr 100-yr Rainfall=5.73"

Area (ac)	CN	Description
4.680	98	Paved parking, HSG D
2.190	39	>75% Grass cover, Good, HSG A
0.210	61	>75% Grass cover, Good, HSG B
7.610	80	>75% Grass cover, Good, HSG D
0.470	30	Woods, Good, HSG A
0.290	77	Woods, Good, HSG D
15.450	78	Weighted Average
10.770		69.71% Pervious Area
4.680		30.29% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
0.4	14	0.0100	0.60		Sheet Flow, Smooth surfaces n= 0.011 P2= 2.31"
9.3	86	0.0250	0.15		Sheet Flow, Grass: Short n= 0.150 P2= 2.31"
1.7	218	0.0180	2.16		Shallow Concentrated Flow, Unpaved Kv= 16.1 fps
1.5	62	0.0180	0.67		Shallow Concentrated Flow, Woodland Kv= 5.0 fps
0.3	60	0.0330	2.92		Shallow Concentrated Flow, Unpaved Kv= 16.1 fps
2.7	250	0.0025	1.56	15.55	Trap/Vee/Rect Channel Flow, Bot.W=0.00' D=1.00' Z= 10.0 '/' Top.W=20.00' n= 0.030 Short grass
0.1	77	0.0480	9.94	7.81	Pipe Channel, 12.0" Round Area= 0.8 sf Perim= 3.1' r= 0.25' n= 0.013 Corrugated PE, smooth interior
16.0	767	Total			

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Type II 24-hr 100-yr Rainfall=5.73"

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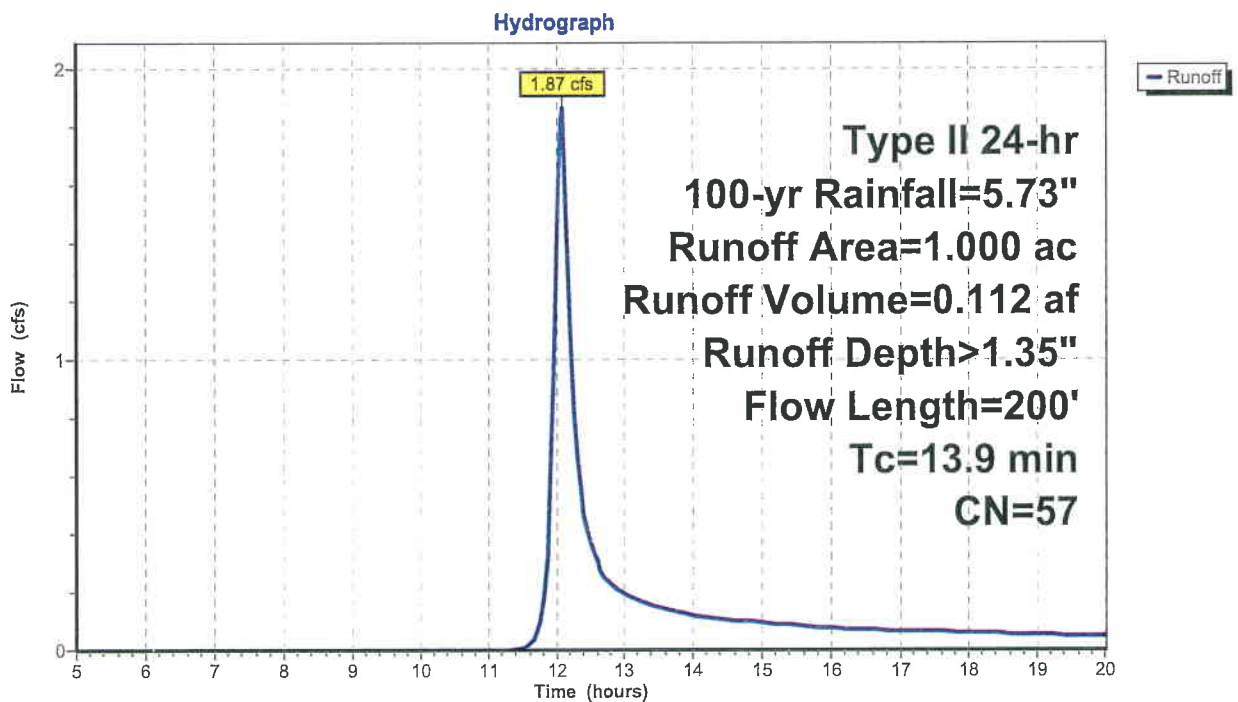
Summary for Subcatchment 3S: WS #1C

Runoff = 1.87 cfs @ 12.07 hrs, Volume= 0.112 af, Depth> 1.35"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
Type II 24-hr 100-yr Rainfall=5.73"

Area (ac)	CN	Description
0.080	98	Paved parking, HSG D
0.320	39	>75% Grass cover, Good, HSG A
0.600	61	>75% Grass cover, Good, HSG B
1.000	57	Weighted Average
0.920		92.00% Pervious Area
0.080		8.00% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
12.9	100	0.0150	0.13		Sheet Flow, Grass: Short n= 0.150 P2= 2.31"
1.0	100	0.0100	1.61		Shallow Concentrated Flow, Unpaved Kv= 16.1 fps
13.9	200	Total			

Subcatchment 3S: WS #1C

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Type II 24-hr 100-yr Rainfall=5.73"

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Summary for Subcatchment 5S: WS #2A

Runoff = 0.56 cfs @ 12.27 hrs, Volume= 0.086 af, Depth> 0.43"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
Type II 24-hr 100-yr Rainfall=5.73"

Area (ac)	CN	Description
0.200	98	Paved parking, HSG D
0.940	30	Woods, Good, HSG A
1.120	39	>75% Grass cover, Good, HSG A
0.120	61	>75% Grass cover, Good, HSG B
2.380	42	Weighted Average
2.180		91.60% Pervious Area
0.200		8.40% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.1	40	0.0250	0.13		Sheet Flow, Grass: Short n= 0.150 P2= 2.31"
12.3	60	0.0440	0.08		Sheet Flow, Woods: Light underbrush n= 0.400 P2= 2.31"
0.8	60	0.0660	1.28		Shallow Concentrated Flow, Woodland Kv= 5.0 fps
0.4	95	0.0660	4.14		Shallow Concentrated Flow, Unpaved Kv= 16.1 fps
1.2	90	0.0660	1.28		Shallow Concentrated Flow, Woodland Kv= 5.0 fps
4.0	188	0.0240	0.77		Shallow Concentrated Flow, Woodland Kv= 5.0 fps
23.8	533	Total			

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Type II 24-hr 100-yr Rainfall=5.73"

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Summary for Subcatchment 6S: WS #2C

Runoff = 1.31 cfs @ 11.96 hrs, Volume= 0.067 af, Depth> 4.69"

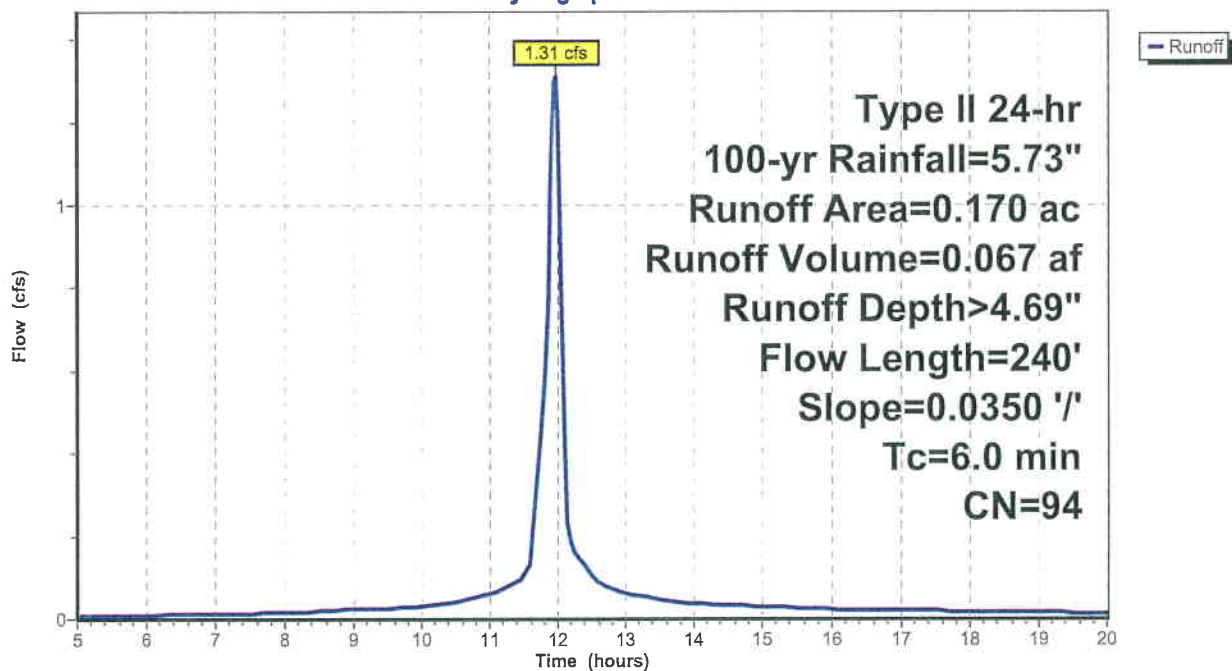
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
Type II 24-hr 100-yr Rainfall=5.73"

Area (ac)	CN	Description
0.150	98	Paved parking, HSG B
0.020	61	>75% Grass cover, Good, HSG B
0.170	94	Weighted Average
0.020		11.76% Pervious Area
0.150		88.24% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.1	100	0.0350	1.46		Sheet Flow, Smooth surfaces n= 0.011 P2= 2.31"
0.6	140	0.0350	3.80		Shallow Concentrated Flow, Paved Kv= 20.3 fps
4.3					Direct Entry,
6.0	240	Total			

Subcatchment 6S: WS #2C

Hydrograph



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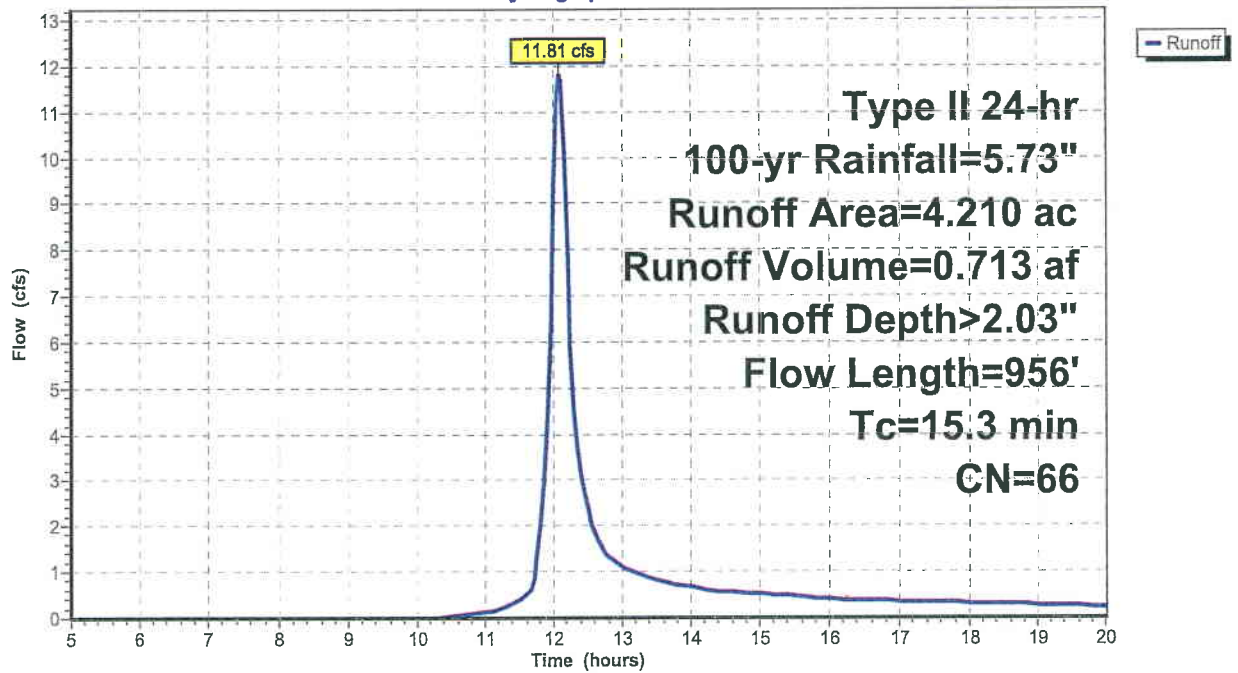
Type II 24-hr 100-yr Rainfall=5.73"

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Subcatchment 7S: WS #2B

Hydrograph



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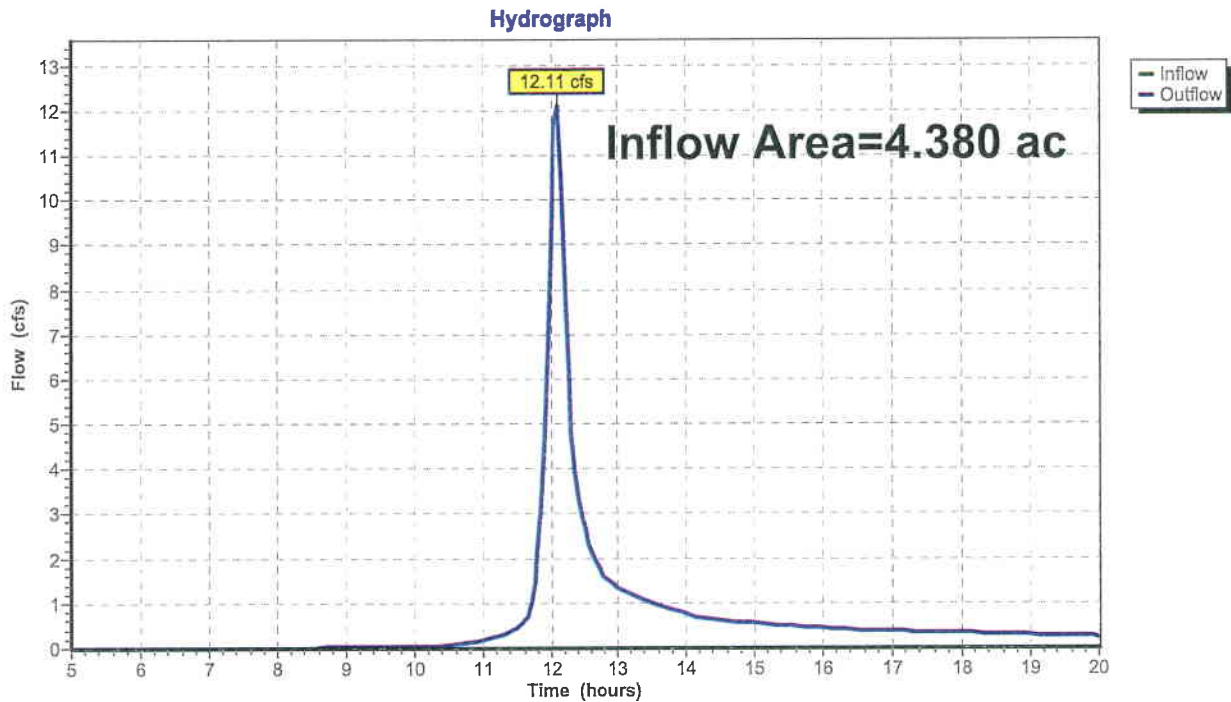
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Summary for Reach 2R: WS #2B/C POA

Inflow Area = 4.380 ac, 22.83% Impervious, Inflow Depth > 2.14" for 100-yr event
Inflow = 12.11 cfs @ 12.08 hrs, Volume= 0.779 af
Outflow = 12.11 cfs @ 12.08 hrs, Volume= 0.779 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Reach 2R: WS #2B/C POA



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Type II 24-hr 100-yr Rainfall=5.73"

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Summary for Pond 1P: Existing Wetlands-Reduced

Inflow Area = 8.970 ac, 9.92% Impervious, Inflow Depth > 2.80" for 100-yr event
 Inflow = 30.02 cfs @ 12.13 hrs, Volume= 2.096 af
 Outflow = 24.60 cfs @ 12.20 hrs, Volume= 2.026 af, Atten= 18%, Lag= 4.3 min
 Primary = 24.60 cfs @ 12.20 hrs, Volume= 2.026 af

Routing by Dyn-Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
 Peak Elev= 992.88' @ 12.25 hrs Surf.Area= 26,162 sf Storage= 10,515 cf

Plug-Flow detention time= 23.1 min calculated for 2.019 af (96% of inflow)
 Center-of-Mass det. time= 10.8 min (806.2 - 795.3)

Volume	Invert	Avail.Storage	Storage Description
#1	991.90'	21,366 cf	Custom Stage Data (Prismatic) Listed below (Recalc)

Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
991.90	0	0	0
992.00	539	27	27
992.50	12,019	3,140	3,166
993.00	30,390	10,602	13,769
993.25	30,390	7,598	21,366

Device	Routing	Invert	Outlet Devices
#1	Primary	992.42'	Asymmetrical Weir, C= 3.27 Offset (feet) -26.27 -25.00 0.00 20.00 26.27 Height (feet) 0.58 0.13 0.00 0.13 0.58

Primary OutFlow Max=22.02 cfs @ 12.20 hrs HW=992.88' TW=992.81' (Dynamic Tailwater)
 ↑1=Asymmetrical Weir (Weir Controls 22.02 cfs @ 0.98 fps)

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Type II 24-hr 100-yr Rainfall=5.73"

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Stage-Discharge for Pond 1P: Existing Wetlands-Reduced

Elevation (feet)	Primary (cfs)	Elevation (feet)	Primary (cfs)	Elevation (feet)	Primary (cfs)
991.90	0.00	992.43	0.00	992.96	50.64
991.91	0.00	992.44	0.03	992.97	52.32
991.92	0.00	992.45	0.07	992.98	54.01
991.93	0.00	992.46	0.14	992.99	55.73
991.94	0.00	992.47	0.25	993.00	57.47
991.95	0.00	992.48	0.40	993.01	59.06
991.96	0.00	992.49	0.59	993.02	60.52
991.97	0.00	992.50	0.82	993.03	61.91
991.98	0.00	992.51	1.10	993.04	63.25
991.99	0.00	992.52	1.43	993.05	64.54
992.00	0.00	992.53	1.82	993.06	65.79
992.01	0.00	992.54	2.26	993.07	67.01
992.02	0.00	992.55	2.76	993.08	68.19
992.03	0.00	992.56	3.32	993.09	69.35
992.04	0.00	992.57	3.92	993.10	70.48
992.05	0.00	992.58	4.57	993.11	71.59
992.06	0.00	992.59	5.26	993.12	72.68
992.07	0.00	992.60	5.98	993.13	73.75
992.08	0.00	992.61	6.74	993.14	74.80
992.09	0.00	992.62	7.54	993.15	75.83
992.10	0.00	992.63	8.37	993.16	76.85
992.11	0.00	992.64	9.23	993.17	77.85
992.12	0.00	992.65	10.12	993.18	78.83
992.13	0.00	992.66	11.05	993.19	79.81
992.14	0.00	992.67	12.00	993.20	80.76
992.15	0.00	992.68	12.98	993.21	81.71
992.16	0.00	992.69	13.99	993.22	82.64
992.17	0.00	992.70	15.03	993.23	83.56
992.18	0.00	992.71	16.09	993.24	84.47
992.19	0.00	992.72	17.19	993.25	85.37
992.20	0.00	992.73	18.30		
992.21	0.00	992.74	19.45		
992.22	0.00	992.75	20.62		
992.23	0.00	992.76	21.81		
992.24	0.00	992.77	23.03		
992.25	0.00	992.78	24.28		
992.26	0.00	992.79	25.55		
992.27	0.00	992.80	26.84		
992.28	0.00	992.81	28.16		
992.29	0.00	992.82	29.50		
992.30	0.00	992.83	30.86		
992.31	0.00	992.84	32.25		
992.32	0.00	992.85	33.66		
992.33	0.00	992.86	35.09		
992.34	0.00	992.87	36.55		
992.35	0.00	992.88	38.03		
992.36	0.00	992.89	39.53		
992.37	0.00	992.90	41.05		
992.38	0.00	992.91	42.59		
992.39	0.00	992.92	44.16		
992.40	0.00	992.93	45.75		
992.41	0.00	992.94	47.36		
992.42	0.00	992.95	48.99		

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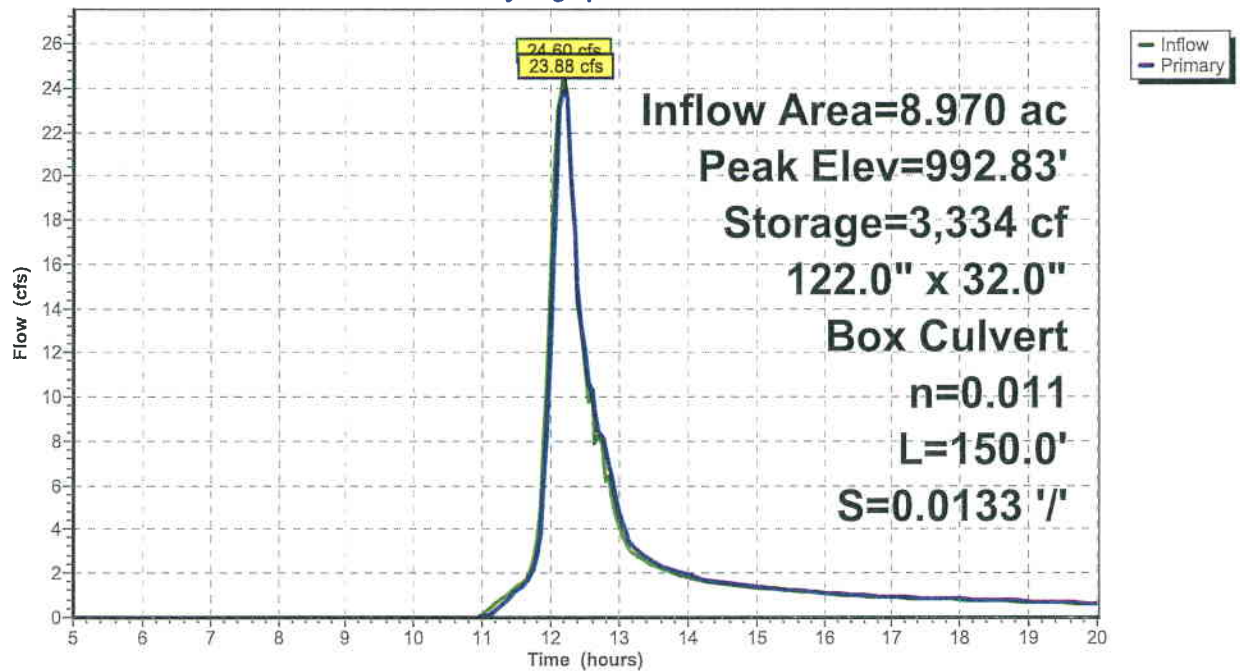
Type II 24-hr 100-yr Rainfall=5.73"

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Pond 2P: Box Culvert

Hydrograph



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Summary for Pond 3P: Stormwater Wetland

Inflow Area = 24.420 ac, 22.81% Impervious, Inflow Depth > 2.94" for 100-yr event
 Inflow = 84.73 cfs @ 12.10 hrs, Volume= 5.990 af
 Outflow = 27.23 cfs @ 12.46 hrs, Volume= 3.893 af, Atten= 68%, Lag= 21.4 min
 Primary = 27.23 cfs @ 12.46 hrs, Volume= 3.893 af
 Secondary = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af

Routing by Dyn-Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
 Peak Elev= 992.58' @ 12.46 hrs Surf.Area= 52,305 sf Storage= 117,990 cf

Plug-Flow detention time= 129.3 min calculated for 3.893 af (65% of inflow)
 Center-of-Mass det. time= 58.8 min (853.1 - 794.2)

Volume	Invert	Avail.Storage	Storage Description
#1	990.00'	169,355 cf	Custom Stage Data (Prismatic) Listed below (Recalc)

Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
990.00	39,300	0	0
993.00	54,445	140,618	140,618
993.50	60,505	28,738	169,355

Device	Routing	Invert	Outlet Devices
#1	Primary	990.00'	18.0" Round Culvert x3 X 3.00 L= 50.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 990.00' / 989.75' S= 0.0050 ' ' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 1.77 sf
#2	Device 1	990.00'	3.0" Vert. Orificex2 X 2.00 C= 0.600
#3	Device 1	992.00'	36.0" x 36.0" Horiz. Grate#1 C= 0.600 Limited to weir flow at low heads
#4	Device 1	992.00'	36.0" x 60.0" Horiz. Grate#2 C= 0.600 Limited to weir flow at low heads
#5	Secondary	993.00'	32.0' long x 10.0' breadth Broad-Crested Rectangular Weir Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 Coef. (English) 2.49 2.56 2.70 2.69 2.68 2.69 2.67 2.64

Primary OutFlow Max=27.23 cfs @ 12.46 hrs HW=992.58' TW=0.00' (Dynamic Tailwater)

↑ **1=Culvert x3** (Inlet Controls 27.23 cfs @ 5.14 fps)
 ↑ **2=Orificex2** (Passes < 0.74 cfs potential flow)
 ↑ **3=Grate#1** (Passes < 17.13 cfs potential flow)
 ↑ **4=Grate#2** (Passes < 22.84 cfs potential flow)

Secondary OutFlow Max=0.00 cfs @ 5.00 hrs HW=990.00' (Free Discharge)

↑ **5=Broad-Crested Rectangular Weir** (Controls 0.00 cfs)

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Type II 24-hr 100-yr Rainfall=5.73"

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Stage-Discharge for Pond 3P: Stormwater Wetland

Elevation (feet)	Discharge (cfs)	Primary (cfs)	Secondary (cfs)	Elevation (feet)	Discharge (cfs)	Primary (cfs)	Secondary (cfs)
990.00	0.00	0.00	0.00	992.65	27.78	27.78	0.00
990.05	0.01	0.01	0.00	992.70	28.14	28.14	0.00
990.10	0.04	0.04	0.00	992.75	28.50	28.50	0.00
990.15	0.08	0.08	0.00	992.80	28.85	28.85	0.00
990.20	0.13	0.13	0.00	992.85	29.20	29.20	0.00
990.25	0.17	0.17	0.00	992.90	29.55	29.55	0.00
990.30	0.20	0.20	0.00	992.95	29.89	29.89	0.00
990.35	0.22	0.22	0.00	993.00	30.23	30.23	0.00
990.40	0.25	0.25	0.00	993.05	31.45	30.56	0.89
990.45	0.27	0.27	0.00	993.10	33.41	30.89	2.52
990.50	0.29	0.29	0.00	993.15	35.85	31.22	4.63
990.55	0.31	0.31	0.00	993.20	38.67	31.54	7.13
990.60	0.33	0.33	0.00	993.25	41.89	31.86	10.03
990.65	0.34	0.34	0.00	993.30	45.46	32.18	13.28
990.70	0.36	0.36	0.00	993.35	49.34	32.49	16.85
990.75	0.37	0.37	0.00	993.40	53.53	32.81	20.72
990.80	0.39	0.39	0.00	993.45	58.18	33.11	25.07
990.85	0.40	0.40	0.00	993.50	63.17	33.42	29.76
990.90	0.42	0.42	0.00				
990.95	0.43	0.43	0.00				
991.00	0.44	0.44	0.00				
991.05	0.45	0.45	0.00				
991.10	0.47	0.47	0.00				
991.15	0.48	0.48	0.00				
991.20	0.49	0.49	0.00				
991.25	0.50	0.50	0.00				
991.30	0.51	0.51	0.00				
991.35	0.52	0.52	0.00				
991.40	0.53	0.53	0.00				
991.45	0.54	0.54	0.00				
991.50	0.55	0.55	0.00				
991.55	0.56	0.56	0.00				
991.60	0.57	0.57	0.00				
991.65	0.58	0.58	0.00				
991.70	0.59	0.59	0.00				
991.75	0.60	0.60	0.00				
991.80	0.61	0.61	0.00				
991.85	0.62	0.62	0.00				
991.90	0.63	0.63	0.00				
991.95	0.64	0.64	0.00				
992.00	0.65	0.65	0.00				
992.05	1.68	1.68	0.00				
992.10	3.56	3.56	0.00				
992.15	5.99	5.99	0.00				
992.20	8.87	8.87	0.00				
992.25	12.13	12.13	0.00				
992.30	15.74	15.74	0.00				
992.35	19.66	19.66	0.00				
992.40	23.88	23.88	0.00				
992.45	26.28	26.28	0.00				
992.50	26.66	26.66	0.00				
992.55	27.04	27.04	0.00				
992.60	27.41	27.41	0.00				

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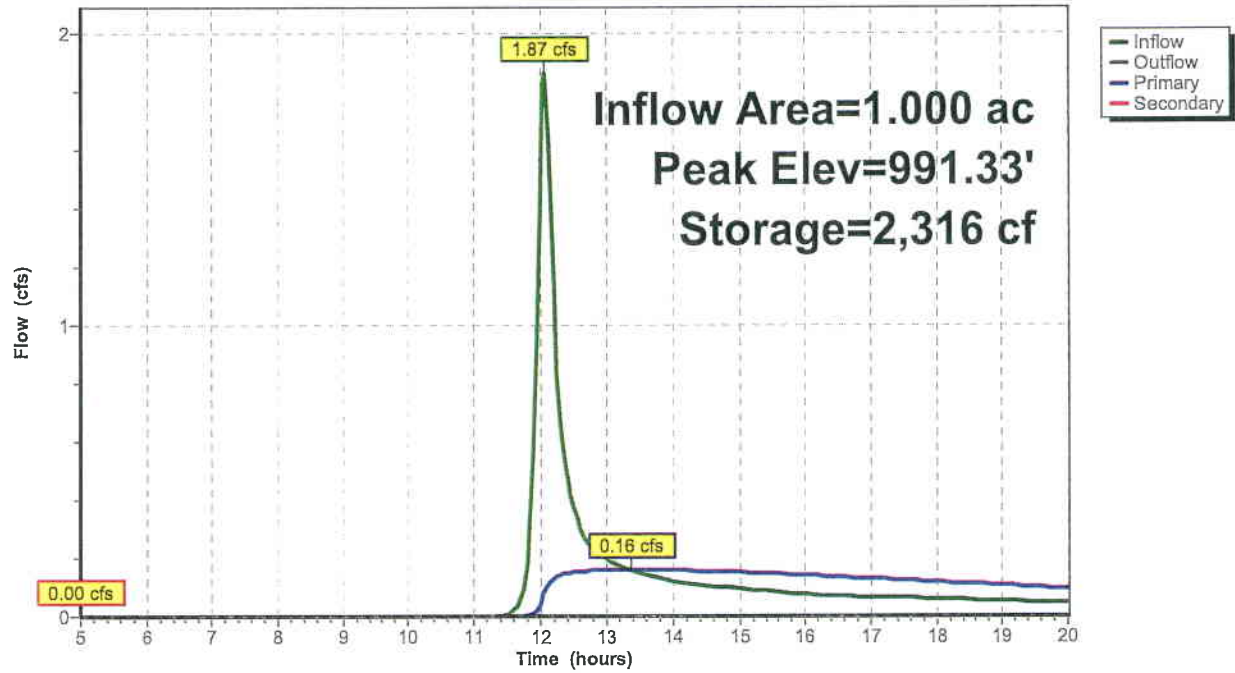
Type II 24-hr 100-yr Rainfall=5.73"

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Pond 4P: Wetland #2

Hydrograph



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Summary for Pond 5P: Underground Detention

Inflow Area = 0.170 ac, 88.24% Impervious, Inflow Depth > 4.69" for 100-yr event
 Inflow = 1.31 cfs @ 11.96 hrs, Volume= 0.067 af
 Outflow = 0.30 cfs @ 12.13 hrs, Volume= 0.066 af, Atten= 77%, Lag= 9.8 min
 Primary = 0.30 cfs @ 12.13 hrs, Volume= 0.066 af

Routing by Dyn-Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
 Peak Elev= 982.34' @ 12.13 hrs Surf.Area= 0.013 ac Storage= 0.022 af

Plug-Flow detention time= 29.1 min calculated for 0.066 af (100% of inflow)
 Center-of-Mass det. time= 27.0 min (766.9 - 739.9)

Volume	Invert	Avail.Storage	Storage Description
#1	980.55'	0.029 af	30.0" Round Pipe Storage x 2 L= 130.0'

Device	Routing	Invert	Outlet Devices
#1	Primary	980.35'	15.0" Round Culvert L= 95.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 980.35' / 979.30' S= 0.0111 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 1.23 sf
#2	Device 1	980.55'	3.0" Vert. Orifice C= 0.600
#3	Device 1	982.95'	2.0' long Sharp-Crested Rectangular Weir 2 End Contraction(s)

Primary OutFlow Max=0.30 cfs @ 12.13 hrs HW=982.33' TW=0.00' (Dynamic Tailwater)

1=Culvert (Passes 0.30 cfs of 5.43 cfs potential flow)
 2=Orifice (Orifice Controls 0.30 cfs @ 6.20 fps)
 3=Sharp-Crested Rectangular Weir (Controls 0.00 cfs)

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Type II 24-hr 100-yr Rainfall=5.73"

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Stage-Discharge for Pond 5P: Underground Detention

Elevation (feet)	Primary (cfs)	Elevation (feet)	Primary (cfs)	Elevation (feet)	Primary (cfs)
980.55	0.00	981.61	0.23	982.67	0.33
980.57	0.00	981.63	0.23	982.69	0.34
980.59	0.00	981.65	0.23	982.71	0.34
980.61	0.01	981.67	0.24	982.73	0.34
980.63	0.01	981.69	0.24	982.75	0.34
980.65	0.02	981.71	0.24	982.77	0.34
980.67	0.03	981.73	0.24	982.79	0.34
980.69	0.04	981.75	0.25	982.81	0.35
980.71	0.05	981.77	0.25	982.83	0.35
980.73	0.05	981.79	0.25	982.85	0.35
980.75	0.06	981.81	0.25	982.87	0.35
980.77	0.07	981.83	0.25	982.89	0.35
980.79	0.08	981.85	0.26	982.91	0.35
980.81	0.09	981.87	0.26	982.93	0.35
980.83	0.09	981.89	0.26	982.95	0.36
980.85	0.10	981.91	0.26	982.97	0.38
980.87	0.10	981.93	0.26	982.99	0.41
980.89	0.11	981.95	0.27	983.01	0.46
980.91	0.11	981.97	0.27	983.03	0.51
980.93	0.12	981.99	0.27	983.05	0.57
980.95	0.12	982.01	0.27		
980.97	0.13	982.03	0.28		
980.99	0.13	982.05	0.28		
981.01	0.14	982.07	0.28		
981.03	0.14	982.09	0.28		
981.05	0.14	982.11	0.28		
981.07	0.15	982.13	0.29		
981.09	0.15	982.15	0.29		
981.11	0.16	982.17	0.29		
981.13	0.16	982.19	0.29		
981.15	0.16	982.21	0.29		
981.17	0.17	982.23	0.29		
981.19	0.17	982.25	0.30		
981.21	0.17	982.27	0.30		
981.23	0.18	982.29	0.30		
981.25	0.18	982.31	0.30		
981.27	0.18	982.33	0.30		
981.29	0.19	982.35	0.31		
981.31	0.19	982.37	0.31		
981.33	0.19	982.39	0.31		
981.35	0.19	982.41	0.31		
981.37	0.20	982.43	0.31		
981.39	0.20	982.45	0.31		
981.41	0.20	982.47	0.32		
981.43	0.21	982.49	0.32		
981.45	0.21	982.51	0.32		
981.47	0.21	982.53	0.32		
981.49	0.21	982.55	0.32		
981.51	0.22	982.57	0.33		
981.53	0.22	982.59	0.33		
981.55	0.22	982.61	0.33		
981.57	0.22	982.63	0.33		
981.59	0.23	982.65	0.33		

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Type II 24-hr 100-yr Rainfall=5.73"

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Stage-Discharge for Pond 9P: DI #14

Elevation (feet)	Discharge (cfs)	Primary (cfs)	Secondary (cfs)	Elevation (feet)	Discharge (cfs)	Primary (cfs)	Secondary (cfs)
979.30	0.00	0.00	0.00	981.95	3.52	3.52	0.00
979.35	0.00	0.00	0.00	982.00	3.58	3.58	0.00
979.40	0.01	0.01	0.00	982.05	3.64	3.64	0.00
979.45	0.02	0.02	0.00	982.10	3.70	3.70	0.00
979.50	0.04	0.04	0.00	982.15	3.76	3.76	0.00
979.55	0.06	0.06	0.00	982.20	3.82	3.82	0.00
979.60	0.09	0.09	0.00	982.25	3.88	3.88	0.00
979.65	0.12	0.12	0.00	982.30	3.93	3.93	0.00
979.70	0.16	0.16	0.00	982.35	3.99	3.99	0.00
979.75	0.20	0.20	0.00	982.40	4.05	4.05	0.00
979.80	0.26	0.26	0.00	982.45	4.10	4.10	0.00
979.85	0.31	0.31	0.00	982.50	4.15	4.15	0.00
979.90	0.37	0.37	0.00	982.55	4.21	4.21	0.00
979.95	0.44	0.44	0.00	982.60	4.26	4.26	0.00
980.00	0.52	0.52	0.00	982.65	4.31	4.31	0.00
980.05	0.59	0.59	0.00	982.70	4.36	4.36	0.00
980.10	0.68	0.68	0.00	982.75	4.41	4.41	0.00
980.15	0.77	0.77	0.00	982.80	4.46	4.46	0.00
980.20	0.86	0.86	0.00	982.85	4.51	4.51	0.00
980.25	0.95	0.95	0.00	982.90	4.56	4.56	0.00
980.30	1.05	1.05	0.00	982.95	4.61	4.61	0.00
980.35	1.15	1.15	0.00	983.00	4.66	4.66	0.00
980.40	1.26	1.26	0.00	983.05	4.70	4.70	0.00
980.45	1.36	1.36	0.00	983.10	4.75	4.75	0.00
980.50	1.47	1.47	0.00	983.15	4.80	4.80	0.00
980.55	1.58	1.58	0.00	983.20	4.84	4.84	0.00
980.60	1.69	1.69	0.00	983.25	4.89	4.89	0.00
980.65	1.80	1.80	0.00	983.30	4.93	4.93	0.00
980.70	1.91	1.91	0.00	983.35	5.19	4.98	0.21
980.75	2.02	2.02	0.00	983.40	5.61	5.02	0.59
980.80	2.12	2.12	0.00	983.45	6.15	5.07	1.09
980.85	2.22	2.22	0.00	983.50	6.79	5.11	1.68
980.90	2.32	2.32	0.00	983.55	7.50	5.15	2.34
980.95	2.41	2.41	0.00	983.60	8.28	5.19	3.08
981.00	2.49	2.49	0.00	983.65	9.12	5.24	3.88
981.05	2.56	2.56	0.00	983.70	10.02	5.28	4.74
981.10	2.62	2.62	0.00	983.75	10.98	5.32	5.66
981.15	2.67	2.67	0.00	983.80	11.99	5.36	6.63
981.20	2.70	2.70	0.00				
981.25	2.70	2.70	0.00				
981.30	2.58	2.58	0.00				
981.35	2.66	2.66	0.00				
981.40	2.74	2.74	0.00				
981.45	2.82	2.82	0.00				
981.50	2.90	2.90	0.00				
981.55	2.97	2.97	0.00				
981.60	3.05	3.05	0.00				
981.65	3.12	3.12	0.00				
981.70	3.19	3.19	0.00				
981.75	3.26	3.26	0.00				
981.80	3.33	3.33	0.00				
981.85	3.39	3.39	0.00				
981.90	3.46	3.46	0.00				

PROJECT: 46 South St
LOCATION: Trumansburg, NY
JOB NUMBER: E17-19

Notes:
Tc = Time of Concentration (min) - MIN COVER(ft) 1.00
i = 25 year storm intensity (in/hr) - All Piping is (HDPE) High Density Polyethylene (n =0.010)
c = Coefficient of Runoff

SUBAREA DI #4 (START RUN)	REFERENCE POINTS				LOCAL			PREVIOUS cA's			TOTAL	Cont.	Q	PIPE	LENGTH/ SLOPE			CAP	VEL	TIME			
	FROM	TO	Ic	ε	A(ac)	cA	from sa	Ic	cA	cA	Ic	cA	Ic	I	cfs	dia	mat'l	n	ft	%	cfs	fps	min
	DS	DI #4	DI #3		0.35	0.01	0.00																
	TG				0.90	0.04	0.04																
INV				6.00	TOTAL	0.04	NONE			0.04	6.00	6.26	0.2	8	HDPE	0.010	164	0.50	1.1	3.2	0.86		
SUBAREA DI #3	REFERENCE POINTS				LOCAL			PREVIOUS cA's			TOTAL	Cont.	Q	PIPE	LENGTH/ SLOPE			CAP	VEL	TIME			
	FROM	TO	Ic	ε	A(ac)	cA	from sa	Ic	cA	cA	Ic	cA	Ic	I	cfs	dia	mat'l	n	ft	%	cfs	fps	min
	DS	DI #3	SIMH #1		0.35	0.12	0.04	DI #4	6.86	0.04													
	TG				0.90	0.15	0.14																
INV				6.00	TOTAL	0.18	6.86			0.04	6.86	6.26	1.4	10	HDPE	0.010	154	0.50	2.0	3.7	0.70		
SUBAREA DI #2	REFERENCE POINTS				LOCAL			PREVIOUS cA's			TOTAL	Cont.	Q	PIPE	LENGTH/ SLOPE			CAP	VEL	TIME			
	FROM	TO	Ic	ε	A(ac)	cA	from sa	Ic	cA	cA	Ic	cA	Ic	I	cfs	dia	mat'l	n	ft	%	cfs	fps	min
	DS	DI #2	DI #1		0.35	0.20	0.07	DI #3	7.55	0.22													
	TG				0.90	0.38	0.34																
INV				6.00	TOTAL	0.41	7.55			0.22	6.83	7.55	6.26	3.9	12	HDPE	0.010	97	1.00	4.6	5.9	0.27	
SUBAREA DI #1 (START RUN)	REFERENCE POINTS				LOCAL			PREVIOUS cA's			TOTAL	Cont.	Q	PIPE	LENGTH/ SLOPE			CAP	VEL	TIME			
	FROM	TO	Ic	ε	A(ac)	cA	from sa	Ic	cA	cA	Ic	cA	Ic	I	cfs	dia	mat'l	n	ft	%	cfs	fps	min
	DS	DI #1	SIMH #1		0.35	0.20	0.07																
	TG				0.90	0.48	0.43																
INV				6.00	TOTAL	0.50	6.00			0.00	0.50	6.00	6.26	3.1	12	HDPE	0.010	97	1.20	5.1	6.5	0.25	
SUBAREA SIMH #1	REFERENCE POINTS				LOCAL			PREVIOUS cA's			TOTAL	Cont.	Q	PIPE	LENGTH/ SLOPE			CAP	VEL	TIME			
	FROM	TO	Ic	ε	A(ac)	cA	from sa	Ic	cA	cA	Ic	cA	Ic	I	cfs	dia	mat'l	n	ft	%	cfs	fps	min
	DS	SIMH #1	Wetland		0.35	0.00	0.00	DI #1	6.25	0.50													
	TG				0.90	0.00	0.00	DI #2	7.83	0.63													
INV				6.00	TOTAL	0.00	7.83			1.13	1.13	7.83	6.26	7.1	12	HDPE	0.010	73	2.96	8.0	10.1	0.12	

SUBAREA Lot 4/5 Culvert (START RUN)	REFERENCE POINTS		LOCAL		PREVIOUS cA's		TOTAL	Cont.	Q	PIPE	LENGTH SLOPE		CAP	VEL	TIME
	FROM	TO	Ic	S	A(ac)	cA	Ic	cA	I	dia	ft	%	cfs	fps	min
	DS	Lot 4/5 Culvert				0.08									
	TG	DI #11				0.35									
	INV					0.90									
			6.00	TOTAL	0.11		6.00	0.11	6.26	8 HDPE	0.010	47	1.00	1.6	4.5
SUBAREA Lot 3/4 Culvert (START RUN)	REFERENCE POINTS		LOCAL		PREVIOUS cA's		TOTAL	Cont.	Q	PIPE	LENGTH SLOPE		CAP	VEL	TIME
	FROM	TO	Ic	S	A(ac)	cA	Ic	cA	I	dia	ft	%	cfs	fps	min
	DS	Lot 3/4 Culvert				0.08									
	TG	DI #10				0.35									
	INV					0.90									
			6.00	TOTAL	0.11		6.00	0.00	6.26	8 HDPE	0.010	46	7.00	4.2	11.9
SUBAREA Lot 2/3 Culvert (START RUN)	REFERENCE POINTS		LOCAL		PREVIOUS cA's		TOTAL	Cont.	Q	PIPE	LENGTH SLOPE		CAP	VEL	TIME
	FROM	TO	Ic	S	A(ac)	cA	Ic	cA	I	dia	ft	%	cfs	fps	min
	DS	Lot 2/3 Culvert				0.22									
	TG	DI #9				0.35									
	INV					0.90									
			6.00	TOTAL	0.29		6.00	0.00	6.26	8 HDPE	0.010	45	11.30	5.3	15.1
SUBAREA DI #11	REFERENCE POINTS		LOCAL		PREVIOUS cA's		TOTAL	Cont.	Q	PIPE	LENGTH SLOPE		CAP	VEL	TIME
	FROM	TO	Ic	S	A(ac)	cA	Ic	cA	I	dia	ft	%	cfs	fps	min
	DS	DI #11				0.02									
	TG	DI #10				0.35									
	INV					0.90									
			6.00	TOTAL	0.11		6.17	0.11	6.26	10 HDPE	0.010	134	1.10	3.0	5.5
SUBAREA DI #10	REFERENCE POINTS		LOCAL		PREVIOUS cA's		TOTAL	Cont.	Q	PIPE	LENGTH SLOPE		CAP	VEL	TIME
	FROM	TO	Ic	S	A(ac)	cA	Ic	cA	I	dia	ft	%	cfs	fps	min
	DS	DI #10				0.02									
	TG	DI #9				0.35									
	INV					0.90									
			6.00	TOTAL	0.09		6.58	0.33	6.26	10 HDPE	0.010	104	0.88	2.7	4.9
SUBAREA DI #9	REFERENCE POINTS		LOCAL		PREVIOUS cA's		TOTAL	Cont.	Q	PIPE	LENGTH SLOPE		CAP	VEL	TIME
	FROM	TO	Ic	S	A(ac)	cA	Ic	cA	I	dia	ft	%	cfs	fps	min
	DS	DI #9				0.01									
	TG	DI #8				0.35									
	INV					0.90									
			6.00	TOTAL	0.10		6.94	0.71	6.26	12 HDPE	0.010	82	1.70	6.0	7.7
							0.80		5.0						0.18

SUBAREA	REFERENCE POINTS		LOCAL		PREVIOUS c/s		TOTAL		Cont.		Q		PIPE		LENGTH		SLOPE		CAP		VEL		TIME	
	FROM	TO	Tg	s	A(sec)	cA	from ss	Tg	cA	Tg	I	cfs	dia	mat	n	ft	%	sf	sf	fps	hrs	min		
(START RUN)	DS	DI #13		0.35	0.26	0.08																		
	TG	Wetland		0.90	0.35	0.32																		
	INV		6.00	TOTAL	0.41		6.00	0.00	0.41	6.00	6.26	2.5	12	HDPE	0.010	237	0.50	3.3	4.2	0.95				

Prepared by Josh Stackhouse on March 14, 2018

Stormwater Treatment System Design Summary

46 South Street

Village of Trumansburg, NY

Information provided by Steven Rowe, PE (T.G. Miller, P.C.)

Site information:

Structure ID	Area (ac)	Percent Impervious	Tc (min)	WQF- 90% Average Runoff Flow (cfs)	Peak Flow (100-Yr) (cfs)
CDS	0.17	88.2%	6	0.22	1.31

Assumptions:

- NYSDEC has adopted the NJCAT/NJDEP verified flow rates for the CDS system. NYSDEC has effectively created three categories of treatment, new development (standalone), redevelopment and pretreatment. Specific approval and sizing criteria are applied to each category. Per the specifying engineer, this project falls under **Redevelopment**.

CDS System Sizing:

The CDS Stormwater Treatment System is a high-performance hydrodynamic separator. Using patented continuous deflective separation technology, the CDS system screens, separates and traps debris, sediment, and oil and grease from stormwater runoff. The indirect screening capability of the system allows for 100% removal of floatables and neutrally buoyant material without blinding. Flow and screening controls physically separate captured solids, preventing re-suspension and release of previously trapped pollutants.

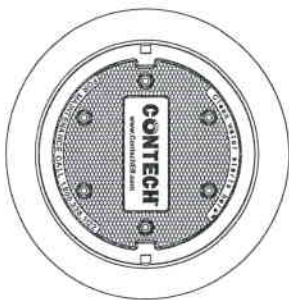
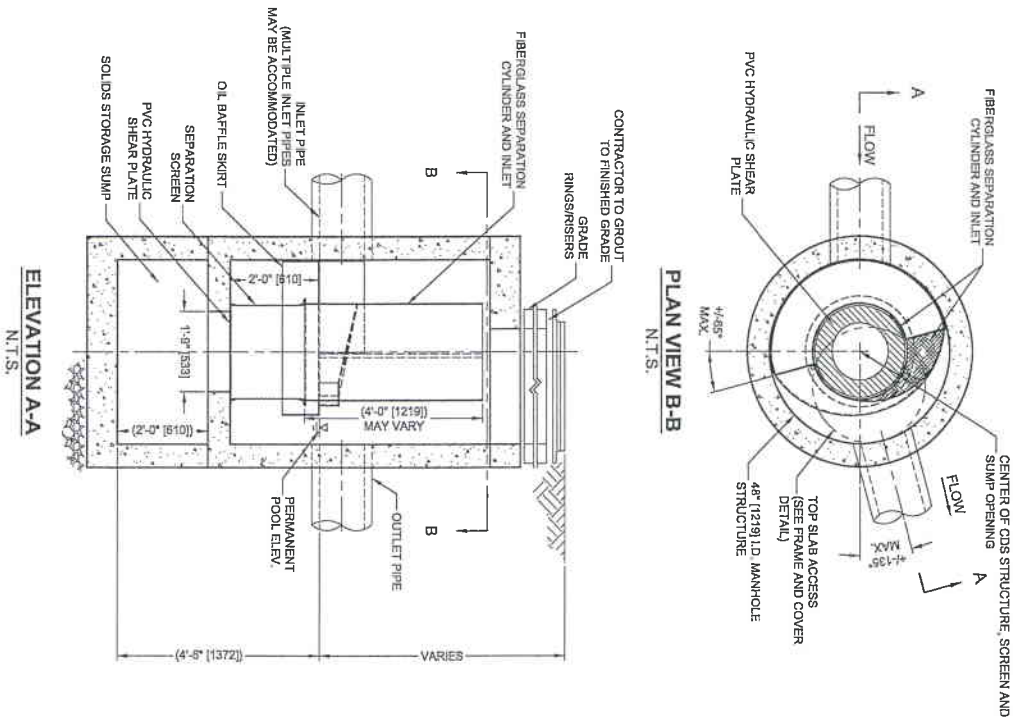
Contech typically selects the CDS model that based on the NJCAT/NJDEP verified flow rates meets or exceeds the Water Quality Flow generated by the Water Quality Volume. The NJCAT/NJDEP verification uses the TARP protocol and as such meets the requirement laid out by NYSDEC on page 9-8 of the New York State Stormwater Management Design Manual for redevelopment projects. No such specification exists for pretreatment projects, but in the best interest of the environment Contech holds to those flows for pretreatment projects as well. Based on the flows above, Contech recommends:

Structure ID	Treatment Device	NYSDEC Approved Treatment Flow (cfs)
CDS	CDS2015-4 (CDS-4)	0.93

Maintenance:

Like any stormwater best management practice, the CDS system requires regular inspection and maintenance to ensure optimal performance. Maintenance frequency will be driven by site conditions. Quarterly visual inspections are recommended, at which time the accumulation of pollutants can be determined. On average, the CDS system requires annual removal of accumulated pollutants.

Please contact us if you have any questions or need any additional information. Again, thank you for your interest in the CDS system. We look forward to receiving your feedback and working with you.



FRAME AND COVER
(DIAMETER VARIES)
N.T.S.

CDS-4-C (CDS2015-4) DESIGN NOTES

CDS-4-C (CDS2015-4) RATED TREATMENT CAPACITY IS 0.25 GPM. IF THE SITE CONDITIONS EXCEED MAXIMUM HYDRAULIC INTERNAL BYPASS CAPACITY, AN UPSTREAM BYPASS STRUCTURE IS REQUIRED.

SITE SPECIFIC DATA REQUIREMENTS

STRUCTURE ID			
WATER QUALITY FLOW RATE (GPM OR L/s)			*
PEAK FLOW RATE (GPM OR L/s)			*
RETURN PERIOD OF PEAK FLOW (YRS)			*
SCREEN APERTURE (2400)			*
PIPE DATA:			
INLET PIPE 1	I.E.	MATERIAL	DIAMETER
INLET PIPE 2	*	*	*
OUTLET PIPE	*	*	*
RIM ELEVATION			*
ANTI-FLOTATION BALLAST		WIDTH	HEIGHT

* PER ENGINEER OF RECORD

- GENERAL NOTES:
- CONTECH TO PROVIDE ALL MATERIALS UNLESS NOTED OTHERWISE.
 - DIMENSIONS MARKED WITH () ARE REFERENCE DIMENSIONS. ACTUAL DIMENSIONS MAY VARY.
 - FOR FABRICATION DRAWINGS WITH DETAILED STRUCTURE DIMENSIONS AND WEIGHTS, PLEASE CONTACT YOUR CONTECH ENGINEERED SOLUTIONS LLC REPRESENTATIVE. www.contech.com
 - CDS WATER QUALITY STRUCTURE SHALL BE IN ACCORDANCE WITH ALL DESIGN DATA AND INFORMATION CONTAINED IN THIS DRAWING.
 - STRUCTURE SHALL MEET ASHTO HS20 LOAD RATING, ASSUMING GROUNDWATER ELEVATION AT OR BELOW THE OUTLET PIPE INVERT ELEVATION. ENGINEER OF RECORD TO CONFIRM ACTUAL GROUNDWATER ELEVATION. CASTINGS SHALL MEET HS20 (ASHTO M 290) AND BE AS WITH THE CONTECH FOUNDATION.
 - IF REQUIRED BY CONTRACT, THE CONTECH FOUNDATION SHALL BE PLACED ON SHEET AT BOTTOM OF SCREEN CYLINDER. REMOVE AND REPLACE AS NECESSARY DURING MAINTENANCE CLEANING.

- INSTALLATION NOTES:
- ANY SUB-BASE, BACKFILL DEPTH, AND/OR ANTI-FLOTATION PROVISIONS ARE SITE-SPECIFIC DESIGN CONSIDERATIONS AND SHALL BE SPECIFIED BY ENGINEER OF RECORD.
 - CONTRACTOR TO PROVIDE EQUIPMENT WITH SUFFICIENT LIFTING AND REACH CAPACITY TO LIFT AND SET THE CDS MANHOLE STRUCTURE (LIFTING CLUTCHES PROVIDED).
 - CONTRACTOR TO PROVIDE AND MAINTAIN SUFFICIENT SLAB BETWEEN ALL STRUCTURE SECTIONS, AND ASSEMBLY STRUCTURE.
 - CONTRACTOR TO PROVIDE, INSTALL, AND GROUT PIPES. MATCH PIPE INVERTS WITH ELEVATIONS SHOWN.
 - CONTRACTOR TO TAKE APPROPRIATE MEASURES TO ASSURE UNIT IS WATER TIGHT. HOLDING WATER TO FLOWLINE INVERT MINIMUM. IT IS SUGGESTED THAT ALL JOINTS BELOW PIPE INVERTS ARE GROUTED.

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ENGINEERED SOLUTIONS LLC
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800-530-1122 816-945-7000 816-945-7993 FAX

CDS-4-C (CDS2015-4)
ONLINE CDS
STANDARD DETAIL



DI #14



South Street Culvert Analysis

Routing Diagram for Proposed

Prepared by Microsoft, Printed 3/15/2018

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Proposed

Prepared by Microsoft

Printed 3/15/2018

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Page 2

Pipe Listing (selected nodes)

Line#	Node Number	In-Invert (feet)	Out-Invert (feet)	Length (feet)	Slope (ft/ft)	n	Diam/Width (inches)	Height (inches)	Inside-Fill (inches)
1	9P	979.30	979.05	308.0	0.0008	0.025	18.0	0.0	0.0

Proposed

Prepared by Microsoft

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Type II 24-hr 100-yr Rainfall=5.73"

Printed 3/15/2018

Page 4

Summary for Pond 9P: DI #14

[57] Hint: Peaked at 983.81' (Flood elevation advised)

Inflow Area = 4.380 ac, 22.83% Impervious, Inflow Depth > 2.14" for 100-yr event
Inflow = 12.11 cfs @ 12.08 hrs, Volume= 0.779 af
Outflow = 12.11 cfs @ 12.08 hrs, Volume= 0.779 af, Atten= 0%, Lag= 0.0 min
Primary = 5.37 cfs @ 12.08 hrs, Volume= 0.663 af
Secondary = 6.74 cfs @ 12.08 hrs, Volume= 0.116 af **Pipe system overflows through grate during 100-year event**

Routing by Dyn-Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Peak Elev= 983.81' @ 12.08 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	979.30'	18.0" Round Existing Culvert L= 308.0' CMP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 979.30' / 979.05' S= 0.0008 '/' Cc= 0.900 n= 0.025 Corrugated metal, Flow Area= 1.77 sf
#2	Secondary	983.30'	17.2" x 17.2" Horiz. Grate EJIW 5115M2 C= 0.600 Limited to weir flow at low heads

Primary OutFlow Max=5.36 cfs @ 12.08 hrs HW=983.80' TW=0.00' (Dynamic Tailwater)

←**1=Existing Culvert** (Barrel Controls 5.36 cfs @ 3.03 fps)

Secondary OutFlow Max=6.54 cfs @ 12.08 hrs HW=983.80' TW=0.00' (Dynamic Tailwater)

←**2=Grate EJIW 5115M2** (Weir Controls 6.54 cfs @ 2.30 fps)

Pond 9P: DI #14

Hydrograph

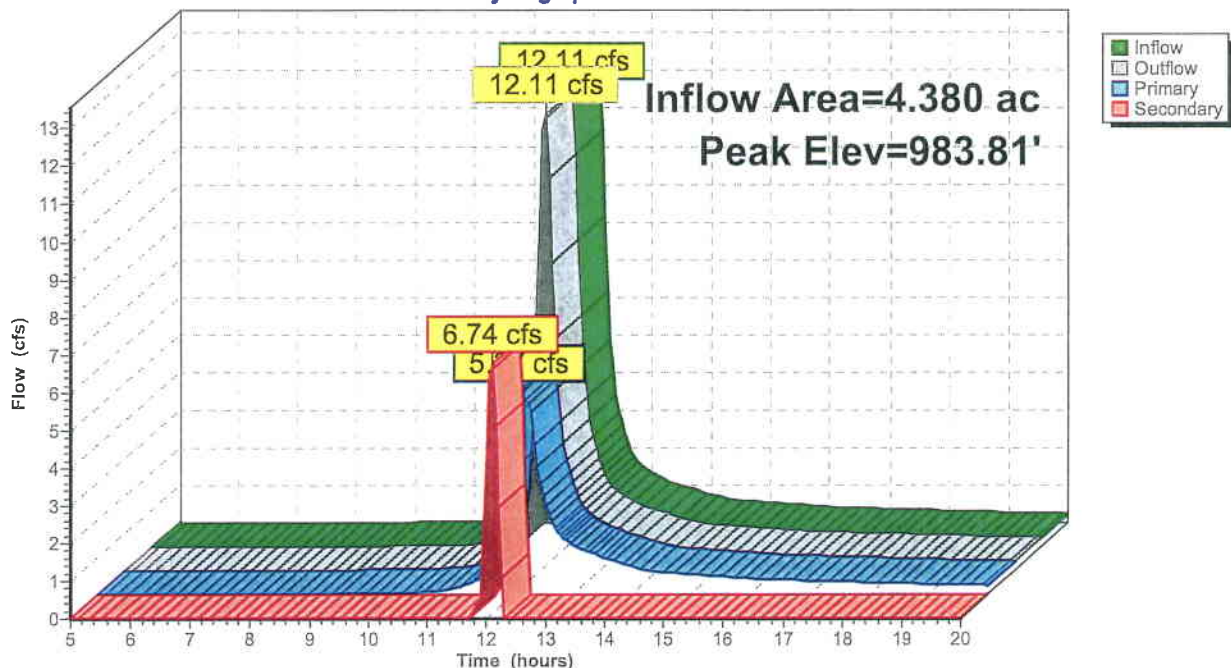


Exhibit H





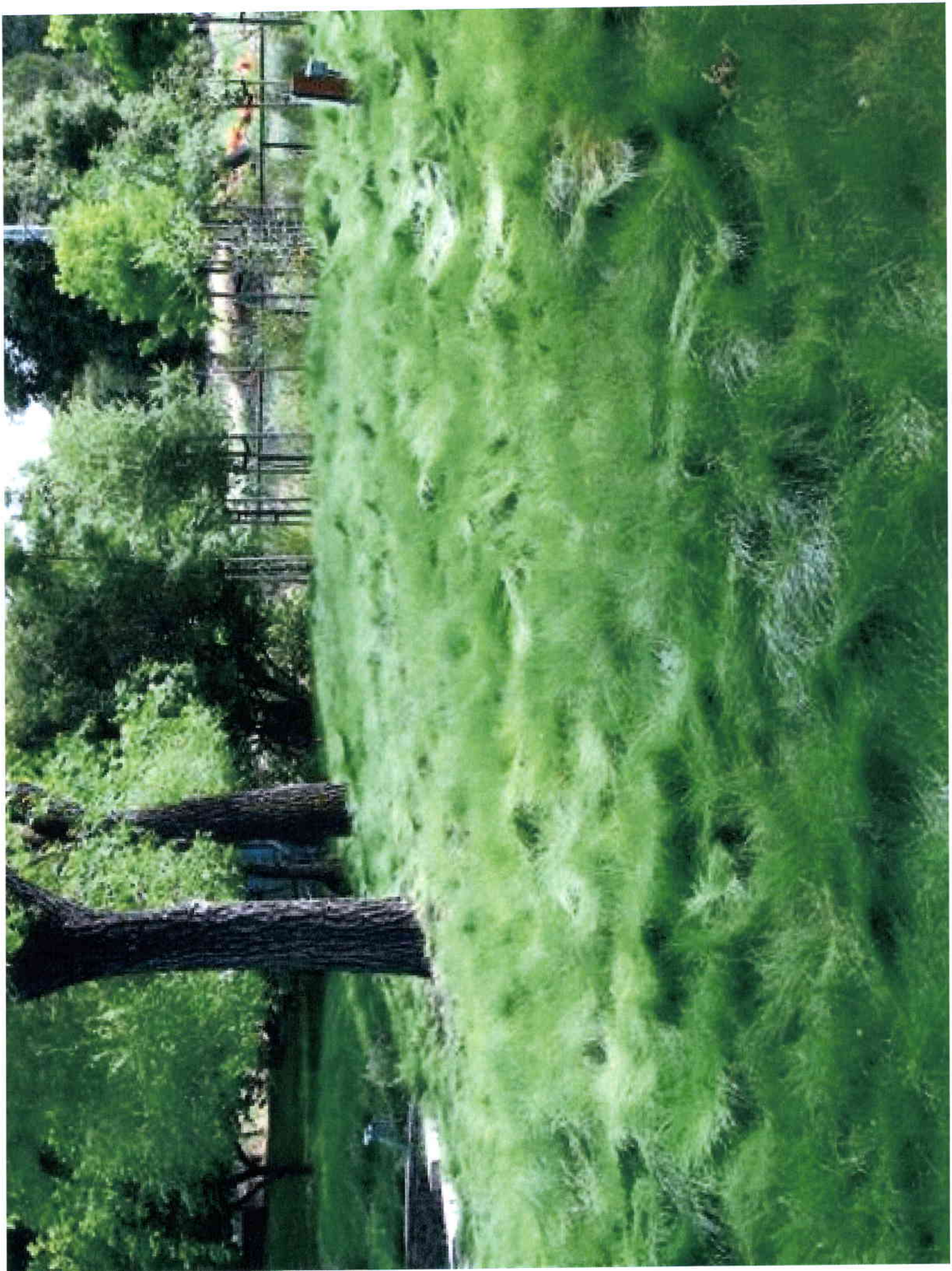
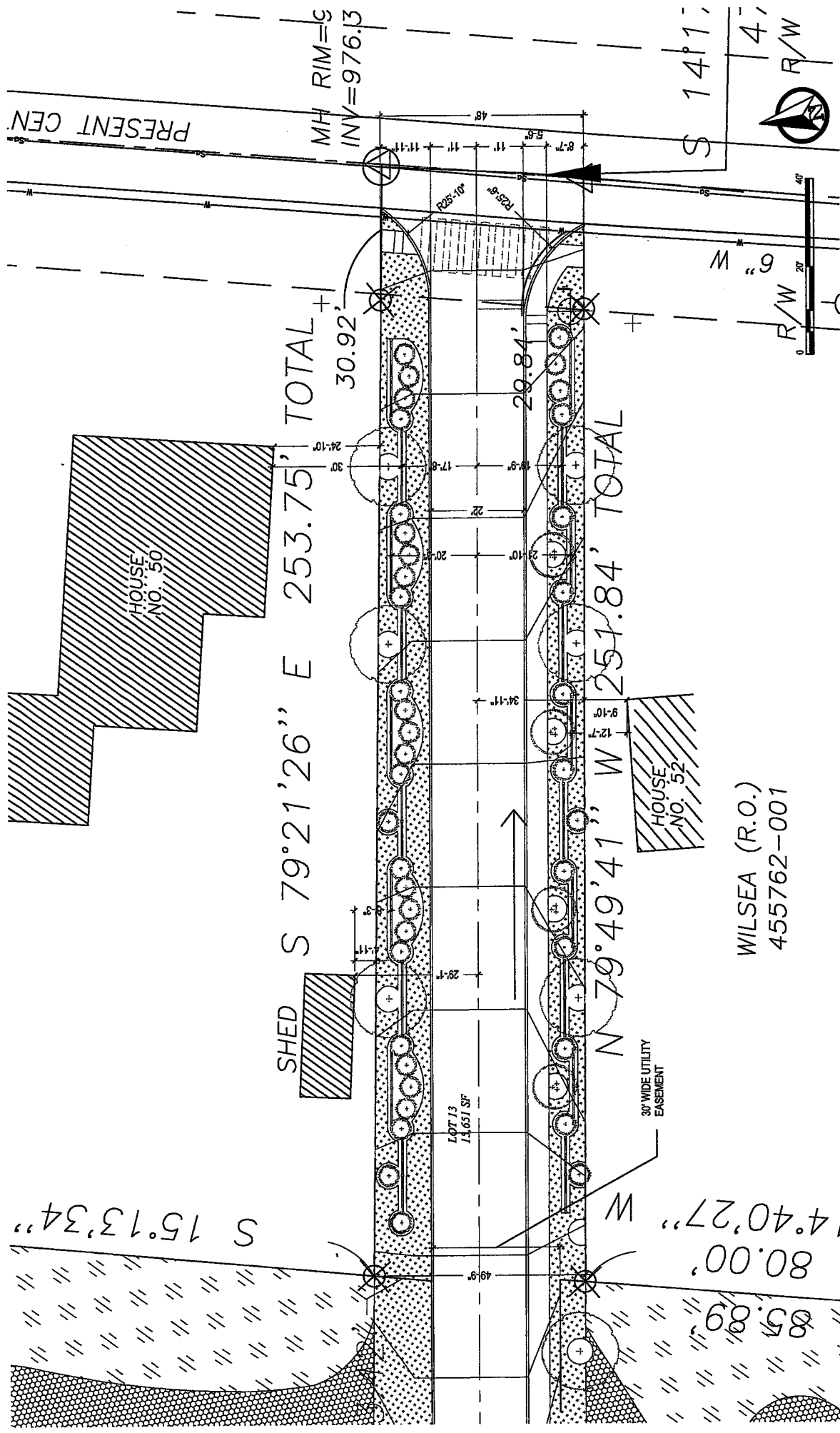
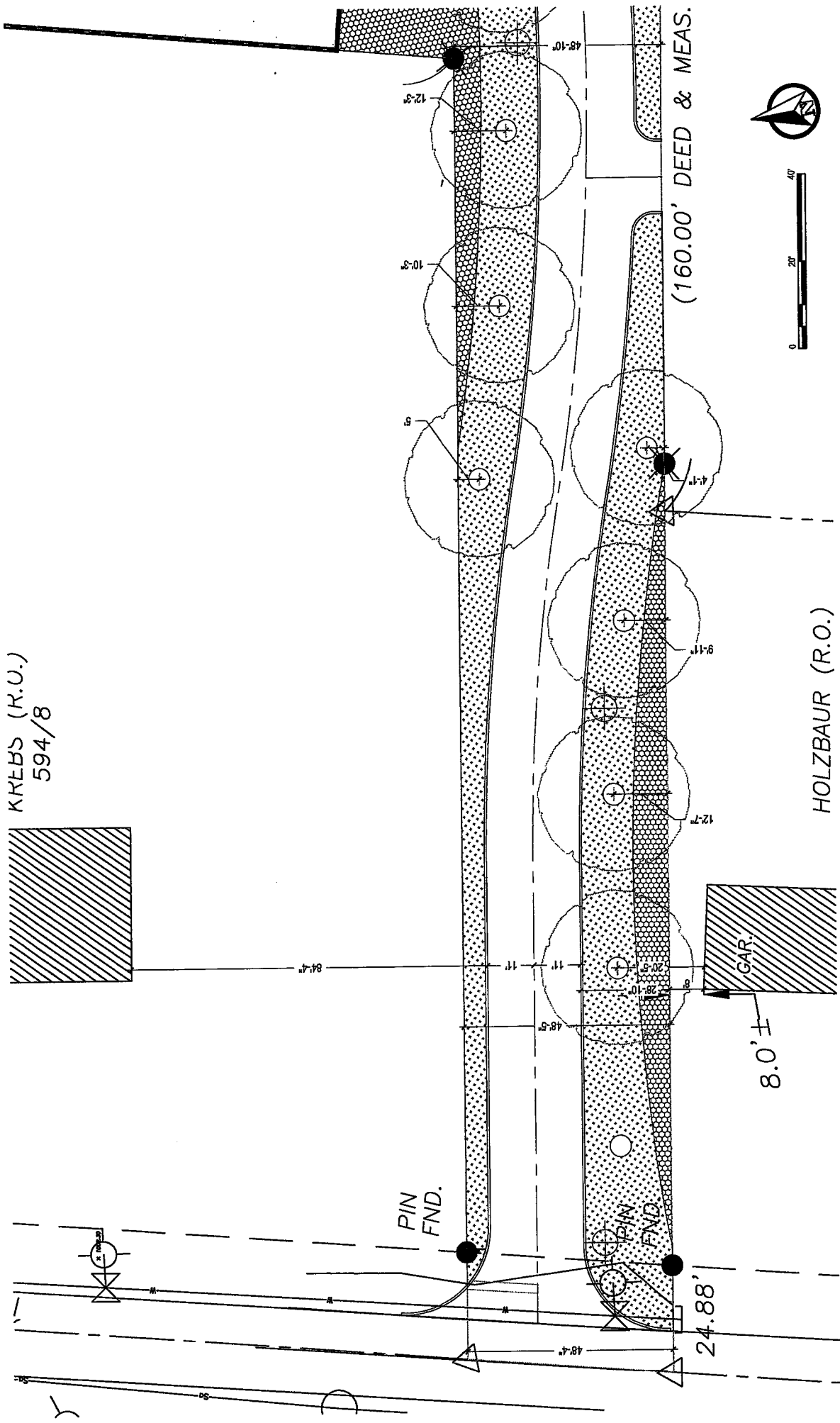


Exhibit I



WILSEA (R.O.)
455762-001



KREBS (K.U.)
594/8

HOLZBAUR (R.O.)